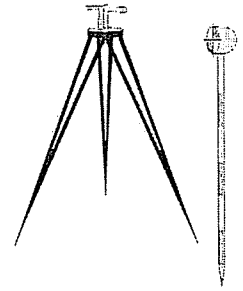




*SPARACO & YOUNGBLOOD, PLLC*  
*CIVIL ENGINEERING \* LAND SURVEYING \* SITE PLANNING*  
*P.O. Box #818; 18 N. Main Street Harriman, N.Y. 10926*  
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*[sparaco.steve@selsny.com](mailto:sparaco.steve@selsny.com)*  
*[wdyls1@gmail.com](mailto:wdyls1@gmail.com)*



## **DRAINAGE REPORT**

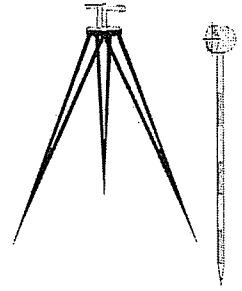
**PROJECT: OAK TREE**

**JOB #: SY #1385**

**REV. DATE: 2-6-20**



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[\*wdyls1@gmail.com\*](mailto:wdyls1@gmail.com)



February 6, 2020

Planning Board  
Town of Haverstraw  
1 Rosman Road  
Garnerville NY 10923

Att: Annette Hendrie, Chief Clerk to Planning Board

Re: Drainage Narrative (SY#1385)  
1-72 Oak Tree Lane and 22 Rosman Road, Haverstraw, NY 10962  
Tax Lots # 26.05-1-42 & 26.09-2-8

Dear Ms. Hendrie:

We have prepared a hydrologic analysis of the 14.3-acre Oak Tree project located as described above in the Town of Haverstraw, NY.

The scope of the Oak Tree project includes the demolition of the existing structures and pavement on site and redeveloped with a site plan for a 228 unit apartment complex containing a boulevard entrance and loop road with connector access and provision of 470 parking spaces at the subject site.

This project proposes a development disturbance area greater than an acre of disturbance, and therefore must meet state mandated requirements for water quality and "green" infrastructure best management practices.

We have reviewed the Rockland County Soil Survey conditions for this area and also performed deep hole and percolation testing and it appears that the soils where the Easterly drainage systems will be located will be amenable to underground infiltration/detention system designs. Our staff witnessed deep hole and percolation testing throughout the two sites on 10-30-18, 11-29-18 and 11-31-17. Areas throughout the site comprised of Fine and Gravelly Sandy Loams throughout the site. Areas tested in the Easterly half of the site were tested and witnessed by our staff indicated adequate permeability rates. Some areas tested in the Westerly portion of the site were not suitable for infiltration.

We have determined that drainage on this site generally drains in three different directions offsite and are indicated on the drainage area plans enclosed in the appendix.

Drainage discharges toward Study Points #1 & #2 consist of areas that drain to the North and West and eventually toward an apartment complex in an RG zone in the Town of Haverstraw and also lands owned by Suez Water to the West and North of the site.

Drainage discharges toward Study Points #3 & #4 consist of areas that drain to the North and East to a 36-inch RCP (Pt. 3) and eventually to a catchbasin located at the Northeasterly corner of Barnes Avenue (Pt. 4) in the Town of West Haverstraw.

Two separate stormwater attenuation systems have been proposed on site to mitigate against increases in discharge offsite in addition to providing water quality benefits in accordance with NYSDEC Stormwater regulations for all the new development on site.

Discharges to the Northwesterly end of the site (Sub-area "Site-1A") will be mitigated via a reduction in total area in this direction, thus yielding reduced flows in developed conditions. However this area will still require that water quality compliance be provided. This will be achieved through a combination of vegetated swales and also a water quality filter (to be designed under separate cover) that will be proposed in conjunction with an underground storage system in this area. The system will consist of fourteen (14) Stormtech MC-4500 units with an outlet control structure for routing purposes and will be controlled by a 3-inch diameter control orifice and 3.93-foot (15-inch diameter pipe overflow) wide service spillway weir. This system eventually will discharge to a 50-foot long level spreader and then overflow toward the existing apartment complex property to the West and Suez Water parcel to the North.

Discharges to the Southwesterly area on site (Sub-area "Site-2") will be mitigated by a reduction in total area in this direction, thus yielding reduced flows in developed conditions. Envirohood in line oil water separators will be provided for all catchbasins in this area as well as the rest of the site. Details to be provided in the site plan set prior to final approval.

Discharges to the Northeasterly end of the site (Sub-area "Site-5A") will be mitigated via a proposed underground retention/detention system in this area for water quality purposes and will require one hundred forty (140) Stormtech MC-4500 units with an outlet control structure for routing purposes. A 14-minute percolation rate for this area was determined during field testing performed on 11-29-18 and incorporated in our design along with a 4.5-inch diameter control orifice and a 4.71-foot (18-inch diameter overflow) wide service spillway weir. This system overflows toward the larger above ground infiltration/detention basin just to the South and East of this system.

Discharges to the Southeasterly end of the site (Sub-areas "Site-3A" & "Site-4") will be mitigated via a proposed above ground retention/detention system in this area and will be controlled by a proposed outlet structure prior to release of storm flows offsite. The pond will include water quality elements including a forebay for pre-treatment purposes and a sand filter for water quality purposes and will also function as a detention basin for discharges greater than the 1-year design storm. A 28-minute percolation rate for this area was determined during field testing performed on 11-29-18 and incorporated in our design along with 3.5-inch and 8-inch diameter control orifii and a 3.0-foot wide service spillway weir.

A full Storm Water Pollution Prevention Plan (SWPPP) will be required for this project. We will submit a full SWPPP at a later date prior to final approval. Our preliminary calculations enclosed herein indicate that compliance can readily be achieved with the current design.

Our analysis includes storms ranging from the 1-year to the 100-year design. Refer to the Summary Table below for a comparison of Existing and Developed Conditions Discharges from the site.

**Summary Table # 1 – Oak Tree drainage to the Northwest (Pt. #1) for Existing and Developed Conditions:**

Conditions	Storm Frequency (in years)					
	1	2	5	10	25	100
Pre-Dev. Discharges (cfs)	2.28	4.27	7.30	9.18	12.14	22.48
Post-Dev. Discharges (cfs)	0.91	1.76	3.04	4.12	6.68	11.92
Net Change:	-1.37	-2.51	-4.26	-5.06	-5.46	-10.56

**Summary Table # 2 – Oak Tree drainage to the Southwest (Pt. #2) for Existing and Developed Conditions:**

Conditions	Storm Frequency (in years)					
	1	2	5	10	25	100
Pre-Dev. Discharges (cfs)	0.25	0.47	0.78	0.96	1.23	2.11
Post-Dev. Discharges (cfs)	0.22	0.37	0.57	0.68	0.84	1.36
Net Change:	-0.03	-0.10	-0.21	-0.28	-0.39	-0.75

**Summary Table # 3 – Oak Tree and offsite drainage to the East (Pt. #3) to a field inlet conveying discharges through an existing 36-inch RCP toward Barnes Avenue for Existing and Developed Conditions:**

**Storm Frequency (in years)**

Conditions	1	2	5	10	25	100
Pre-Dev. Discharges (cfs)	11.95	19.43	29.95	36.30	45.62	75.83
Post-Dev. Discharges (cfs)	9.69	15.19	22.90	27.30	33.70	73.67
Net Change:	- 2.26	- 4.24	- 7.05	- 9.00	- 11.92	- 2.16

**Summary Table # 4 – Oak Tree and offsite drainage toward the Northeast (Pt. #4) to a common municipal drainage point (Curb Inlet) at the NE corner of Barnes Avenue for Existing and Developed Conditions:**

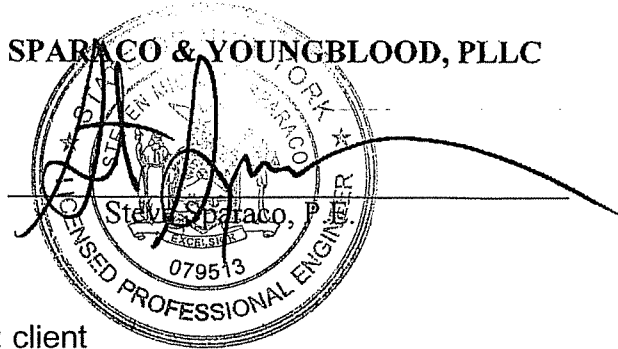
**Storm Frequency (in years)**

Conditions	1	2	5	10	25	100
Pre-Dev. Discharges (cfs)	16.12	27.58	44.98	55.27	70.59	121.08
Post-Dev. Discharges (cfs)	12.85	21.67	34.43	41.90	53.01	102.91
Net Change:	-3.27	- 5.91	- 10.55	- 13.37	- 17.58	- 18.17

Attached are drainage area maps, drainage calculations and backup Hec-1 output data in support of our analysis.

Very truly yours,

**SPARACO & YOUNGBLOOD, PLLC**



cc.: client

# **TABLE OF CONTENTS:**

## Appendix:

- 1.) Methodology
- 2.) Figure #A: Existing Offsite Conditions Drainage Area Map at 1"=50' scale
- 3.) Figure #B: Existing Conditions Drainage Area Map at 1"=50' scale
- 4.) Figure #C: Developed Conditions Drainage Area Map at 1"=50' scale
- 5.) Site Deep Hole and Percolation Results (Refer to Figure "C" for locations)
- 6.) Rockland County Soils Information
- 7.) Curve Number Calculations

## Water Quality Analysis Backup Calculations:

- Reference: Exhibit 4-III: Unit Peak Discharge (qu) for SCS type III rainfall distribution (from TR-55 manual)
- Reference: Figure 8.5 Detention Time vs. Discharge Ratios (from NYSDEC Water Quality Manual)

The following Data provided for Subareas "Site-1A", "Site-5A" & "Site-3A"):

- 1.) Title Sheet
- 2.) Plan Views and Details for each Detention System
- 3.) Peak Discharge Calculations
- 4.) Volume Calculations
- 5.) Summary Table WQ-1: Water Quality Calculations
- 6.) Summary Table WQ-2: Runoff Reduction Volume Calculations
- 7.) Channel Protection Calculations
- 8.) Elevation vs. Discharge Summary Chart

## Hec-1 Analyses:

- 1.) Existing Conditions Hec-1 Model
- 2.) Developed Conditions Hec-1 Model

## **ENGINEERING METHODOLOGY:**

### Area Hydrology:

We have prepared a hydrologic analysis of the 14.3-acre Oak Tree project located as described above in the Town of Haverstraw, NY.

### Methodology:

Four study points where discharges exit the site were analyzed (Study Point 1 through 4 -see attached drainage area maps) to evaluate site runoff under pre- and post- development conditions.

All drainage area delineations and any changes from existing to proposed conditions are indicated graphically on Drainage Area Maps provided in the Appendix.

A hydrologic analysis was performed utilizing procedures outlined in the Soil Conservation Service (SCS) publication Technical Report 55 (TR-55). SCS hydrographs were developed utilizing hydrographs consisting of a 24-hour rainfall event using an SCS Type-III rainfall distribution and unit hydrograph parameters, including drainage area, curve number (CN), time of concentration, and percent impervious.

Time of concentration travel paths on site were insignificant and diminimus as they pertain to this project upon review of the area hydrology thru this site. A 10-minute minimum was used for existing conditions and a 5-minute minimum time of concentration was used for proposed conditions for all developed subareas on site. A 6-minute lag time from the site and discharges collected at the 36-inch RCP at (Study Point #3) to the NE catchbasin at Barnes Avenue (Study Point #4) was utilized for existing and developed conditions in this model.

Curve number calculations were based on hydrologic soil data obtained from available Rockland County Soils Maps. Refer to the Appendix for supporting soils data.

The Army Corps of Engineers hydrologic analysis computer program HEC-1 was utilized to generate runoff hydrographs for the 1, 2, 5, 10, 25 and 100-year frequency storms for pre and post-development conditions. This program was also utilized to perform hydrograph routings and additions to design the required mitigative facilities for developed conditions.

### Stormwater Analysis and proposed mitigation:

The scope of the Oak Tree project includes the demolition of the existing structures and pavement on site and redeveloped with a site plan for a 228 unit apartment complex containing a boulevard entrance and loop road with connector access and provision of 470 parking spaces at the subject site.

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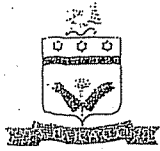
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*Soils Information:*

- 1.) Deep hole and Percolation Testing*
  - 2.) Rockland County Soils Information*
-



### Test Hole Log

Site: Oak Tree  
 Job # SY-1385  
 Date: 11/29/18  
 Name: Sean Kinsley / Bill Johnson

Weather Cond.: Partly Cloudy

Sheet No: 1 | 2  
~~#4~~ | ~~#5~~ | ~~#7~~

DEPTH		TEST HOLE #1	TEST HOLE #2	TEST HOLE #3	TEST HOLE #4	TEST HOLE #5	TEST HOLE #7
FEET	INCHES						
1	3	Humus	HUMUS	HUMUS	BLACKTOP	HUMUS	HUMUS
	6		↑	↑	↑	↑	↑
	9		SANDY LOAM	↑	LOAM	LOAM	LOAM
2	12	Dark Loam	SANDY LOAM	SANDY LOAM	↓	Loam	Some Boulders
	15						
	18						
	21						
3	24	↓	↓	↓	↓	↓	↓
	27						
	30						
4	33	40" Separe	GREY CLAY LOAM W/BOULDS	↓	↓	↓	↓
	36						
	39						
5	42	Sandy Clay	↓	↓	↓	↓	↓
	45						
	48						
6	51	↓	↓	HUMUS	↓	SILTY LOAM HARD	↓
	54						
	57						
7	60	85" Boulders Some	↓	↓	↓	↓	↓
	63						
	66						
	69			GRAVELLY LOAM	↓		
	72						
	75						
PERC. RATE							
DEPTH TO G. W.							

Notes: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_



Sparaco Engineering and Land Surveying PC  
 26 Fireman Memorial Drive - Suite 210  
 Pomona, NY 10970

Phone: (845) 362-1966  
 Fax: (845) 362-1987  
 Email: info@selsny.com

## Test Hole Log

Site: Oak Tree  
 Job # SY-1385  
 Date: 10/29/18  
 Name: WMD #5R

Weather Cond.: CLOUDY 50°

Sheet No: 2 | 2  
#4 | #5 | #7

DEPTH FEET	INCHES	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE																											
									1	2	3	#4	#5	#7																					
8	87	Sandy Clay * Gravelly loam w/ boulders * Bot. No Rock No Water	↓	↑	↓	↓	↓	↓																											
	90								PERC.	RO. B	PERC.	PERC.	PERC.	PERC.																					
	93																																		
	96																																		
9	99								Sandy Clay * Gravelly loam w/ boulders * Bot. No Rock No Water	↓	↑	↓	↓	↓	↓																				
	102																																		
	105																																		
	108																																		
10	111															Sandy Clay * Gravelly loam w/ boulders * Bot. No Rock No Water	↓	↑	↓	↓	↓	↓													
	114																																		
	117																																		
	120																																		
11	123																						Sandy Clay * Gravelly loam w/ boulders * Bot. No Rock No Water	↓	↑	↓	↓	↓	↓						
	126																																		
	129																																		
	132																																		
12	135	Sandy Clay * Gravelly loam w/ boulders * Bot. No Rock No Water	↓	↑	↓	↓	↓	↓																											
	138																																		
	141																																		
	144																																		
13	147								Sandy Clay * Gravelly loam w/ boulders * Bot. No Rock No Water	↓	↑	↓	↓	↓	↓																				
	150																													BOT. NO	BOT. NO	BOT. NO	BOT. NO	BOT. NO	
	153																													WATER	NO ROCK	ROCK NO	Rock No	ROCK NO	
	156																													OR ROCK	OR WATER	WATER	Water	WATER	
14	159															Sandy Clay * Gravelly loam w/ boulders * Bot. No Rock No Water	↓	↑	↓	↓	↓	↓													
	162																																		
	165																																		
	168																																		
PERC. RATE																																			
DEPTH TO G. W.																																			

Notes: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

NEW YORK STATE DEPARTMENT OF HEALTH

Bureau of Community Sanitation and Food Protection

Percolation Test Data

See instructions on reverse side  
Development/Site: Oak Tree

(TN/C)

County: Rockland

Date: 11/29/18 Test Conducted By: Sean Kinsky

Test Hole No.	Test Hole Depth (Inches)	Lot No.	Soil Profile	Presoaking Date & Time	Time	Percolation Test Runs									
						1	2	3	4	5	6				
#1	114"		See Soil log	3" above Top Nail 10:15	END										
#2	96"	"	"	2" above Top Nail 10:45	RESULT	N.G.									
#3	96"	"	"	2" above Top Nail 11:15	END	11:34	11:57	12:27:40	12:57:45						
#4	96"		See Soil log	1" above Top Nail 11:40	BEGIN	11:07	11:35	12:00:00	12:30:35						
#5	96"	"	"	2" above Top Nail 13:55	RESULT	27 min	27 min	:27:40	:27:10						
#7	96"	"	Timed by Stopwatch	2" above Top Nail 15:27:05	END	11:20	11:26	11:32	11:39	11:46:30	11:41:15				

1. Begin time, end time and result in minutes for a water elevation change from 6" to 5" above the bottom of the test hole.



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 26 Fireman Memorial Drive - Suite 210  
 Pomona, NY 10970

Phone: (845) 362-1966  
 Fax: (845) 362-1987  
 Email: info@selsny.com

## Test Hole Log

Site: OAK TREES  
 Job #: SY-1385  
 Date: 10/30/18  
 Name: WMU #6 SK #8

Weather Cond.: CLEAR 40°

Sheet No.: 1 | 2  
#10 | #17 | #19

DEPTH FEET	INCHES	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE
		#6	#8	#9	#10	#17	#19
1	3	HUMUS	HUMUS	HUMUS	HUMUS	HUMUS	HUMUS
	6	↑	↑	↑	↑	↑	↑
	9	↑	↑	↑	↑	↑	↑
	12	↑	↑	↑	↑	↑	↑
2	15	↑	FILL	BROWN LOAM	↑	SANDY LOAM	SANDY LOAM
	18	↑	↓	↓	↑	↓	↓
	21	FILL TOPSOIL	↑	↓	↓	↓	↓
3	24	↑	↑	↑	↑	↑	↑
	27	↑	↑	↑	↑	↑	↑
	30	↑	GREY SILT LOAM	↑	↑	↑	↑
	33	↑	HARD	↑	↑	↑	↑
4	36	↑	↑	↑	↑	↑	↑
	39	↑	SOME BOULDERS	SILT LOAM	↑	SILT LOAM	SILT LOAM
	42	↑	↑	HARD	↑	SOME BOULDERS	SOME BOULDERS
5	45	↑	↑	↑	↑	↑	↑
	48	↑	↑	↑	↑	↑	↑
	51	↑	↑	↑	↑	↑	↑
	54	CLAY LOAM	↑	↑	↑	↑	↑
6	57	↑	↑	↑	↑	↑	↑
	60	↑	↑	↑	↑	↑	↑
	63	↑	↑	↑	SILT LOAM	↑	↑
	66	↑	↑	↑	HARD	↑	↑
7	69	↑	↑	↑	↑	↑	↑
	72	↑	↑	↑	↑	↑	↑
	75	↑	↑	↑	↑	↑	↑
	78	↑	↑	↑	↑	↑	↑
	81	↑	↑	↑	↑	↑	↑
84	↑	↑	↑	↑	↑	↑	
PERC. RATE							
DEPTH TO G. W.							

Notes: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_



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Phone: (845) 362-1966  
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## Test Hole Log

Site: OAK TREE  
 Job # SY-1385  
 Date: 10/30/18  
 Name: WMO #3, K #6 #8 #9 #10 #17

Weather Cond.: CLEAR 40°

Sheet No: 2 | 2

DEPTH FEET	DEPTH INCHES	TEST HOLE					
		#6	#8	#9	#10	#17	
8	87	SILT LOAM	PERC	PERC			
	90						
	93						
	96						
9	99						
	102						
	105						
	108						
10	111						SEEP
	114						
	117						
	120						
11	123						
	126						
	129						
	132						
12	135						WET
	138						
	141						
	144						
13	147	NO ROCK NO WATER		NO ROCK NO WATER	NO ROCK NO WATER	NO ROCK NO WATER	NO ROCK
	150						
	153						
	156						
14	159		NO ROCK NO WATER				
	162						
	165						
	168						
PERC. RATE							
DEPTH TO G. W.							

Notes: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

NEW YORK STATE DEPARTMENT OF HEALTH

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See instructions on reverse side.

Development/Site: Oak Tree

(T/M/C)

County: Rockland

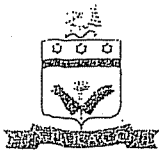
Date: 11/30/18

Test Conducted By: Sean Kinsley

Test Hole No.	Test Hole Depth (Inches)	Lot No.	Soil Profile	Presoaking Date & Time	Time	Percolation Test Runs										
						1	2	3	4	5	6					
#6	96"		See Soil Log	2" above 10:21	END BEGIN RESULT END BEGIN RESULT											
#8	96"		" "	2" above 11:21	END BEGIN RESULT											
#9	96"		" "	2" above 11:40	END BEGIN RESULT	13:08:45	13:47:00	14:29:50								
#10	96"		" "	1 1/2" Above 12:01	END BEGIN RESULT	12:37:00	13:11:55	13:53:30								
#17	<del>96"</del> 72"		" "	2" Above 13:16	END BEGIN RESULT	13:145	13:05	13:20								
#19	36"		" "	2" Above 13:48	END BEGIN RESULT	12:59:00	13:08:46	13:26:55	14:26:40	15:30:25						
					END BEGIN RESULT	12:22:50	12:57:55	13:39:10	14:31:20							
					END BEGIN RESULT	13:11:10	13:50	13:50	13:50	13:50	13:50	13:50	13:50	13:50	13:50	13:50
					END BEGIN RESULT											
					END BEGIN RESULT											
					END BEGIN RESULT											

1. Begin time, end time and result in minutes for a water elevation change from 6" to 5" above the bottom of the test hole.





# Test Hole Log

Site: Oak Tree  
 Job # SY-1385  
 Date: 11/31/18  
 Name: Sean Kinsley / Bill Johnson

Weather Cond.: \_\_\_\_\_

Sheet No: 1 | 2  
 #12 #11 #15 #20

DEPTH FEET	DEPTH INCHES	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE
		#14	#13	#12	#11	#15	#20
1	3	Humus	HUMUS	↑	HUMUS	HUMUS	HUMUS
	6	Fill w/ Cobbles Loamy	↑	CLAY LOAM FILL	↑	LOAM FILL	↑
	9		CLAY LOAM	↓	LOAM FILL	↑	
	12		↑	HUMUS	↓	↑	
15	↓		↑	↓	↑		
2	18	Humus	↑	PERC.	↑	CLAY LOAM W/BOULDERS	↑
	21		↑	↑	↑	CLAY LOAM	
	24		↑	↑	↑	↑	
	27		↑	↑	↑	↑	
3	30	Clay Loam	↑	↑	↑	↑	↑
	33		↑	↑	↑	↑	
	36		↑	↑	↑	↑	
	39		↑	↑	↑	↑	
4	42	Loam	↑	↑	↑	↑	↑
	45		↑	↑	↑	↑	
	48		↑	↑	↑	↑	
	51		↑	↑	↑	↑	
5	54	Loam	↑	↑	↑	↑	↑
	57		↑	↑	↑	↑	
	60		↑	↑	↑	↑	
	63		↑	↑	↑	↑	
6	66	Loam	↑	↑	↑	↑	↑
	69		↑	↑	↑	↑	
	72		↑	↑	↑	↑	
	75		↑	↑	↑	↑	
7	78	Loam	↑	↑	↑	↑	↑
	81		↑	↑	↑	↑	
	84		↑	↑	↑	↑	
	87		↑	↑	↑	↑	
PERC. RATE							
DEPTH TO G. W.							

Notes: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_



Sparaco Engineering and Land Surveying PC Phone: (845) 362-1966  
 26 Fireman Memorial Drive - Suite 210 Fax: (845) 362-1987  
 Pomona, NY 10970 Email: info@selsny.com

### Test Hole Log

Site: Oak Tree Weather Cond.: \_\_\_\_\_  
 Job # S4-1385  
 Date: 11/31/18  
 Name: Sean Kinsky / Bill Johnson Sheet No: 2 | 2  
   #14    #13    #12    #11    #15    #20

DEPTH		TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE			
FEET	INCHES									
8	87	↓	↑ Some BOULDER	SANDY LOAM	↑	PERC.	↓			
	90									
	93									
	96									
9	99				SANDY LOAM	↓		PERC.		
	102									
	105									
	108									
10	111					PERC.		↓	PERC.	
	114									
	117									
	120									
11	123							NO ROCK NO WATER	↓	PERC.
	126									
	129									
	132									
12	135	NO ROCK NO WATER	↓	PERC.						
	138									
	141									
	144									
13	147		NO ROCK NO WATER	↓	PERC.					
	150									
	153									
	156									
14	159			NO ROCK NO WATER	↓	PERC.				
	162									
	165									
	168									
PERC. RATE										
DEPTH TO G. W.										

Notes: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

15' NO ROCK  
NO WATER

SW ① ② ③ ④  
 PERC. 20 37:20

NEW YORK STATE DEPARTMENT OF HEALTH

Bureau of Community Sanitation and Food Protection

Percolation Test Data

See instructions on reverse side.

Development/Site: Oak Tree

(T/M/C)

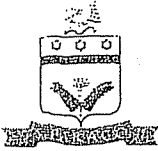
County: Rockland

Date: 10/31/18

Test Conducted By: Sear Kinsky

Test Hole No.	Test Hole Depth (Inches)	Lot No.	Soil Profile	Presoaking Date & Time	Time	Percolation Test Runs										
						1	2	3	4	5	6					
#14	84"		See Soil Log	2" Above 10:02	END BEGIN RESULT											
#13	132"		" "	2" Above 11:00	END BEGIN RESULT											
#12	30"		" "	2" Above 11:23	END BEGIN RESULT	12:13:40	12:55:40	13:27:34								
#11	72"		" "	2" Above 12:08	END BEGIN RESULT	11:57:20	12:26:15	12:57:25								
#15	96"		" "	2" Above 12:35	END BEGIN RESULT	12:16:40	12:49:15	13:00:09								
#20	96"		" " Step control	2" Above 13:20	END BEGIN RESULT	13:30:15										
						N.G.										
						14:02:07										
						N.G.										
						14:01:20										
						37:20	40:00	N.G.								

1. Begin time, end time and result in minutes for a water elevation change from 6" to 5" above the bottom of the test hole.



Sparaco Engineering and Land Surveying PC  
 26 Fireman Memorial Drive - Suite 210  
 Pomona, NY 10970

Phone: (845) 362-1966  
 Fax: (845) 362-1987  
 Email: info@selsny.com

## Test Hole Log

Site: OAK TREE  
 Job # SY-1385  
 Date: 10/31/18  
 Name: W. M. JOHNSON

Weather Cond.: CLEAR 50°

Sheet No: 1 | 2

#21

DEPTH FEET	DEPTH INCHES	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE
1	3	↑ HUMUS ↓					
	6						
	9						
2	12	↑ BROWN CLAY LOAM ↓					
	15						
	18						
	21						
3	24	↑ GREY CLAY LOAM HARD ↓					
	27						
	30						
	33						
4	36	↑					
	39						
	42						
5	45						
	48						
	51						
6	54						
	57						
	60						
	63						
7	66						
	69						
	72						
	75						
	78						
	81						
	84						
PERC. RATE							
DEPTH TO G. W.							

Notes: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_



Sparaco Engineering and Land Surveying PC  
 26 Fireman Memorial Drive - Suite 210  
 Pomona, NY 10970

Phone: (845) 362-1966  
 Fax: (845) 362-1987  
 Email: info@selsny.com

# Test Hole Log

Site: OAK TREE  
 Job # SY-1385  
 Date: 10/31/18  
 Name: W.M.J.

Weather Cond.: CLEAR 50°

Sheet No: 2 | 2

#21

DEPTH		TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE	TEST HOLE
FEET	INCHES						
8	87	PERC.  Some SAND STONE SOFT  					
	90						
	93						
	96						
9	99						
	102						
	105						
	108						
10	111						
	114						
	117						
	120						
11	123						
	126						
	129						
	132						
12	135						
	138						
	141						
	144						
13	147						
	150						
	153						
	156						
14	159						
	162						
	165						
	168						
PERC. RATE							
DEPTH TO G. W.							

Notes: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

NEW YORK STATE DEPARTMENT OF HEALTH

Bureau of Community Sanitation and Food Protection

Percolation Test Data

See instructions on reverse side

Development/Site: Oak Tree

(T/V/C)

County: Rockland

Date: 10/31/18

Test Conducted By: Sean Kinsley

Test Hole No.	Test Hole Depth (Inches)	Lot No.	Soil Profile	Presoaking Date & Time	Time	Percolation Test Runs									
						1	2	3	4	5	6				
#21			See Soil Log <u>steps 6-13:29</u>	<u>2" Above</u>	END										
					BEGIN										
					RESULT	<u>N.G.</u>									
					END										
					BEGIN										
					RESULT										
					END										
					BEGIN										
					RESULT										
					END										
					BEGIN										
					RESULT										
					END										
					BEGIN										
					RESULT										
					END										
					BEGIN										
					RESULT										

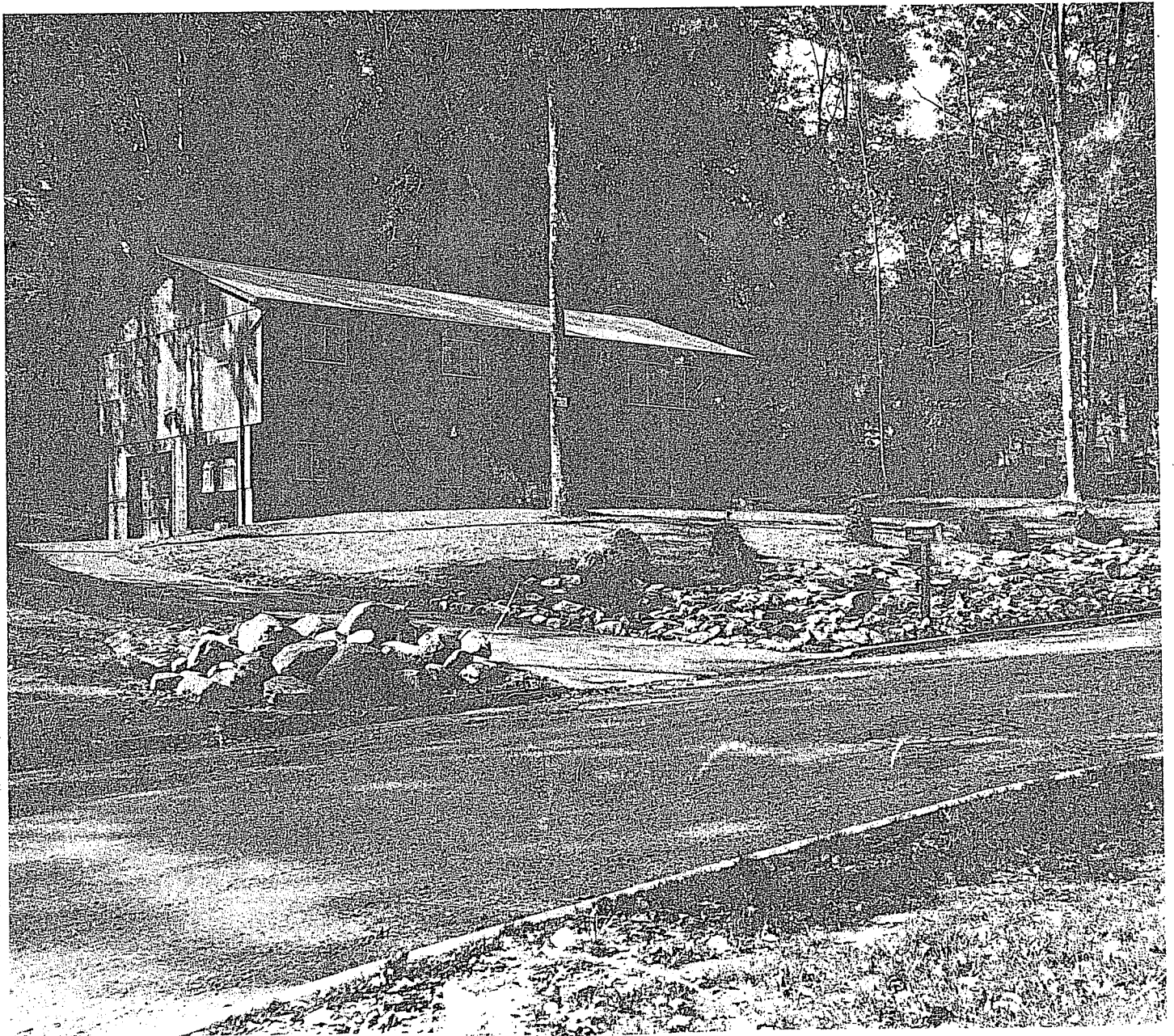
1. Begin time, end time and result in minutes for a water elevation change from 6" to 5" above the bottom of the test hole.

United States  
Department of  
Agriculture

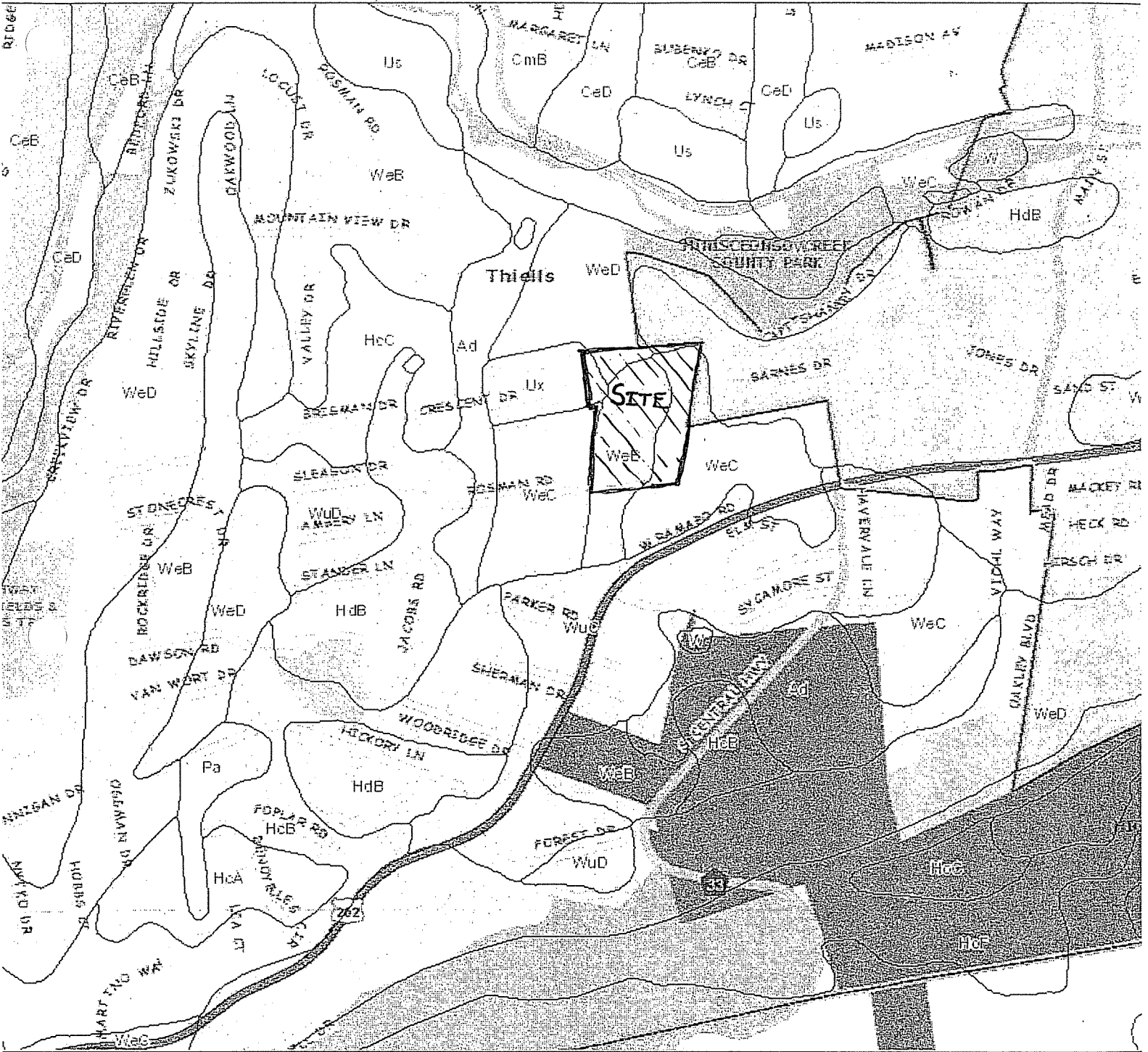
Soil  
Conservation  
Service

In cooperation with  
Cornell University  
Agricultural Experiment  
Station

# Soil Survey of Rockland County, New York



# ArcGIS Web Map





Soil name and map symbol	Hydro-logic group	Flooding			High water table			Bedrock		Risk of corrosion		
		Frequency	Duration	Months	Depth	Kind	Months	Depth	Hardness	Potential frost action	Uncoated steel	Concrete
Pt*, Pv* Pits					<u>Ft</u>			<u>In</u>				
Ra Rippowam	C	Frequent	Brief	Oct-May	0-1.5	Apparent	Sep-Jun	>60	---	High	High	High
ReA, ReB, ReC, ReD Riverhead	B	None	---	---	>6.0	---	---	>60	---	Moderate	Low	High
RuB*, RuC*, RuD* Riverhead	B	None	---	---	>6.0	---	---	>60	---	Moderate	Low	High
Sa Sloan	B/D	Occasional	Brief	Nov-Jun	0-1.0	Apparent	Nov-Jun	>60	---	High	High	Low
Ur*, Us, Uw Udorthents												
Ux* Urban land												
Wa Wallington	C	None	---	---	0.5-1.5	Perched	Jan-Apr	>60	---	High	High	Moderate
Wc Watchaug	B	None	---	---	1.5-2.5	Apparent	Nov-Apr	>60	---	High	Low	High
WeA, WeB, WeC, WeD Wethersfield	C	None	---	---	1.5-2.5	Perched	Feb-Apr	>60	---	Moderate	Low	Moderate
WuB*, WuC*, WuD* Wethersfield	C	None	---	---	1.5-2.5	Perched	Feb-Apr	>60	---	Moderate	Low	Moderate
YaB, YaC, YaD Yalesville	C	None	---	---	>6.0	---	---	20-40	Hard	Low	Low	Moderate
YuB*, YuC*, YuD* Yalesville	C	None	---	---	>6.0	---	---	20-40	Hard	Low	Low	Moderate

\* See description of the map unit for composition and behavior characteristics of the map unit.

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one:  Existing  Developed

CN for Sub-basin: Site-1

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			1	70
C	Lawn / Open Space - Good Condition	74			2.2	162.8
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.94	92.12
Totals =					4.14	324.92

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{324.92}{4.14} = 78.48309179$

Use CN = 78

**2. Runoff**

Frequency..... yr.  
Rainfall, P (24 - hour) ..... in.  
Runoff, Q ..... in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one: Existing  **Developed**

CN for Sub-basin: Site-1

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0.1	7
C	Lawn / Open Space - Good Condition	74			1.01	74.74
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.35	34.3
Totals =					1.46	116.04

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{116.04}{1.46} = 79.47945205$

Use CN =

**2. Runoff**

Frequency..... yr.  
Rainfall, P (24 - hour) ..... in.  
Runoff, Q ..... in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one: Existing  **Developed**

CN for Sub-basin: Site-1A

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0	0
C	Lawn / Open Space - Good Condition	74			0.06	4.44
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.37	36.26
Totals =					0.43	40.7

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{40.7}{0.43} = 94.65116279$

Use CN = **95**

**2. Runoff**

Frequency . . . . . yr.  
Rainfall, P (24 - hour) . . . . . in.  
Runoff, Q . . . . . in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one:  Existing  Developed

CN for Sub-basin: Site-2

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0	0
C	Lawn / Open Space - Good Condition	74			0.18	13.32
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.13	12.74
Totals =					0.31	26.06

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{26.06}{0.31} = 84.06451613$

Use CN = **84**

**2. Runoff**

Frequency . . . . . yr.  
Rainfall, P (24 - hour) . . . . . in.  
Runoff, Q . . . . . in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one: Existing  **Developed**

CN for Sub-basin: Site-2

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0	0
C	Lawn / Open Space - Good Condition	74			0.07	5.18
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.15	14.7
Totals =					0.22	19.88

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{19.88}{0.22} = 90.36363636$

Use CN = **90**

**2. Runoff**

Frequency..... yr.  
Rainfall, P (24 - hour) ..... in.  
Runoff, Q ..... in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one:  Existing  Developed

CN for Sub-basin: Site-3

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0.7	49
C	Lawn / Open Space - Good Condition	74			2.13	157.62
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.73	71.54
Totals =					3.56	278.16

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{278.16}{3.56} = 78.13483146$

Use CN = 78

**2. Runoff**

Frequency..... yr.  
Rainfall, P (24 - hour) ..... in.  
Runoff, Q ..... in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one: Existing  **Developed**

CN for Sub-basin: Site-3

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0.16	11.2
C	Lawn / Open Space - Good Condition	74			0	0
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.00	0
Totals =					0.16	11.2

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{11.2}{0.16} = 70$

Use CN = 70

**2. Runoff**

Frequency . . . . . yr.  
Rainfall, P (24 - hour) . . . . . in.  
Runoff, Q . . . . . in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3



**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one: Existing  **Developed**

CN for Sub-basin: Site-3A

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area # acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0	0
C	Lawn / Open Space - Good Condition	74			0.46	34.04
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			1.82	178.36
Totals =					2.28	212.4

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{212.4}{2.28} = 93.15789474$

Use CN = **93**

**2. Runoff**

Frequency..... yr.  
Rainfall, P (24 - hour) ..... in.  
Runoff, Q ..... in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one:  Existing     Developed

CN for Sub-basin: Site-4

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0.61	42.7
C	Lawn / Open Space - Good Condition	74			0.3	22.2
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.00	0
Totals =					0.91	64.9

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{64.9}{0.91} = 71.31868132$

Use CN = 71

**2. Runoff**

Frequency..... yr.  
Rainfall, P (24 - hour) ..... in.  
Runoff, Q ..... in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one: Existing  **Developed**

CN for Sub-basin: Site-4

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0.4	28
C	Lawn / Open Space - Good Condition	74			1.37	101.38
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.13	12.74
Totals =					1.9	142.12

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{142.12}{1.9} = 74.8$

Use CN = **75**

**2. Runoff**

Frequency . . . . . yr.  
Rainfall, P (24 - hour) . . . . . in.  
Runoff, Q . . . . . in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one:  Existing  Developed

CN for Sub-basin: Site-5

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			2.5	175
C	Lawn / Open Space - Good Condition	74			2.18	161.32
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.88	86.24
Totals =					5.56	422.56

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{422.56}{5.56} = 76$

Use CN =

**2. Runoff**

Frequency . . . . . yr.  
Rainfall, P (24 - hour) . . . . . in.  
Runoff, Q . . . . . in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one: Existing  **Developed**

CN for Sub-basin: Site-5

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			1.8	126
C	Lawn / Open Space - Good Condition	74			1.84	136.16
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.14	13.72
Totals =					3.78	275.88

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{275.88}{3.78} = 72.98412698$

Use CN = 73

**2. Runoff**

Frequency . . . . . yr.  
Rainfall, P (24 - hour) . . . . . in.  
Runoff, Q . . . . . in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 3-Feb-20

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one: Existing  **Developed**

CN for Sub-basin: Site-5A

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0	0
C	Lawn / Open Space - Good Condition	74			0.83	61.42
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			3.43	336.14
Totals =					4.26	397.56

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{397.56}{4.26} = 93.32394366$

Use CN = **93**

**2. Runoff**

Frequency . . . . . yr.  
Rainfall, P (24 - hour) . . . . . in.  
Runoff, Q . . . . . in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 17-Sep-19

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one:  Existing  Developed

CN for Sub-basin: Off-1

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0.5	35
C	Lawn / Open Space - Good Condition	74			0.93	68.82
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			6.42	629.16
Totals =					7.85	732.98

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{732.98}{7.85} = 93.37324841$

Use CN = 93

**2. Runoff**

Frequency..... yr.  
Rainfall, P (24 - hour) ..... in.  
Runoff, Q ..... in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

**SPARACO & YOUNGBLOOD, PLLC**

18 NORTH MAIN STREET  
HARRIMAN, NY 10926  
845-782-8543

**Worksheet 2: Runoff Curve Number and Runoff**

Project: Oak Tree SY-1385

By: SMS

Date: 17-Sep-19

Location: Town of Haverstraw, NY

Checked:

Date:

Shade one:  Existing  Developed

CN for Sub-basin: Off-2

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi <sup>2</sup> <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			1	70
C	Lawn / Open Space - Good Condition	74			1.62	119.88
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.70	68.6
Totals =					3.32	258.48

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{258.48}{3.32} = 77.85542169$

Use CN =

**2. Runoff**

Frequency . . . . . yr.  
Rainfall, P (24 - hour) . . . . . in.  
Runoff, Q . . . . . in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3



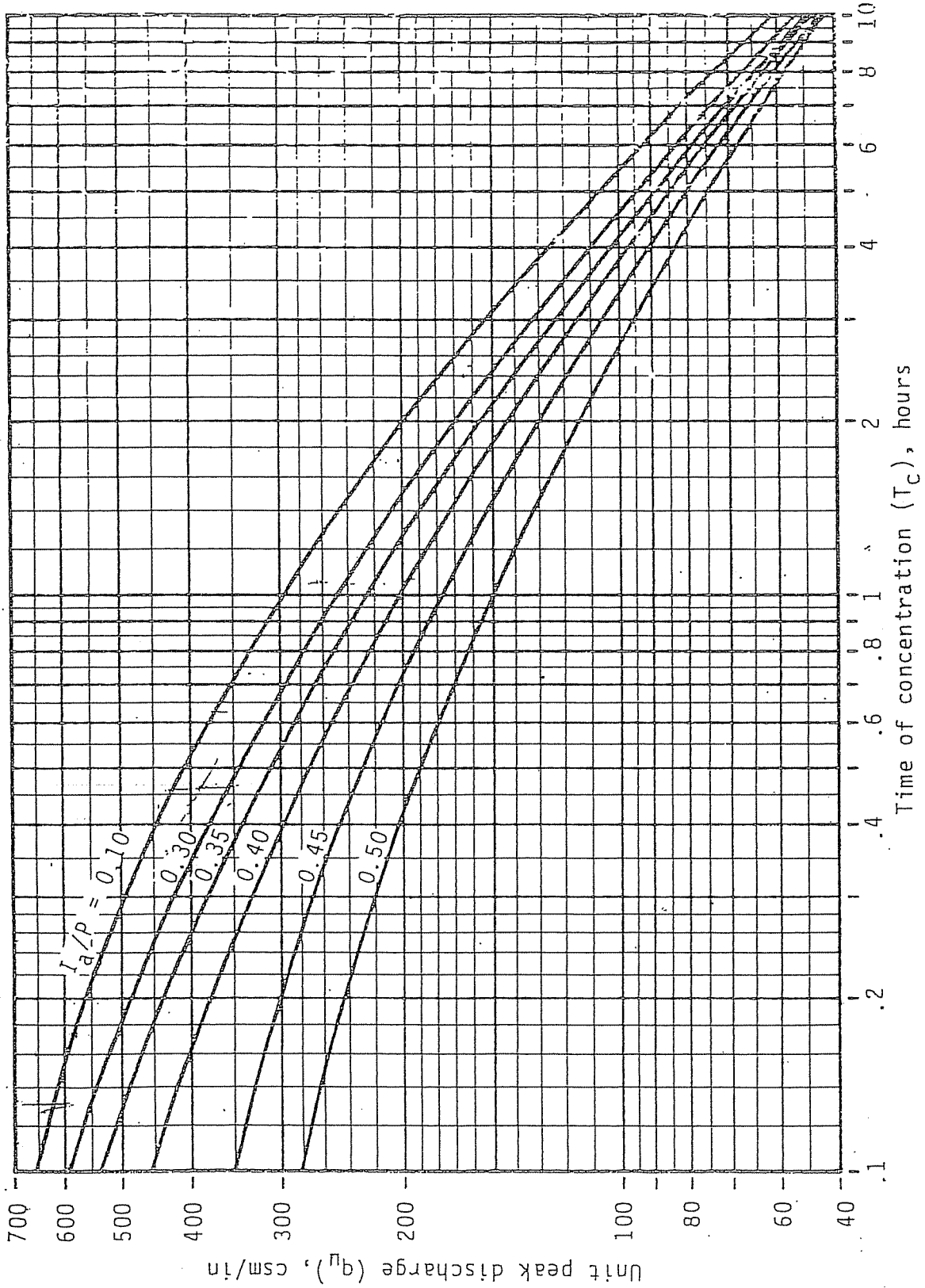
## **Water Quality and Routing Analysis Backup Calculations:**

- *Reference: Exhibit 4-III: Unit Peak Discharge ( $q_u$ ) for SCS type III rainfall distribution (from TR-55 manual)*
- *Reference: Figure 8.5 Detention Time vs. Discharge Ratios (from NYSDEC Water Quality Manual)*

*(The following Data provided for Subareas "Site-1A", "Site-5A" & "Site-3A"):*

- 1.) *Title Sheet*
- 2.) *Plan Views and Details for each Detention System*
- 3.) *Peak Discharge Calculations*
- 4.) *Volume Calculations*
- 5.) *Summary Table WQ-1: Water Quality Calculations*
- 6.) *Summary Table WQ-2: Runoff Reduction Volume Calculations*
- 7.) *Channel Protection Calculations*
- 8.) *Elevation vs. Discharge Summary Chart*

Exhibit 4-III: Unit peak discharge ( $q_u$ ) for SCS type III rainfall distribution



Compute Stream Channel Protection Volume, ( $C_{pv}$ ) (see Section 4.3 and Appendix B)

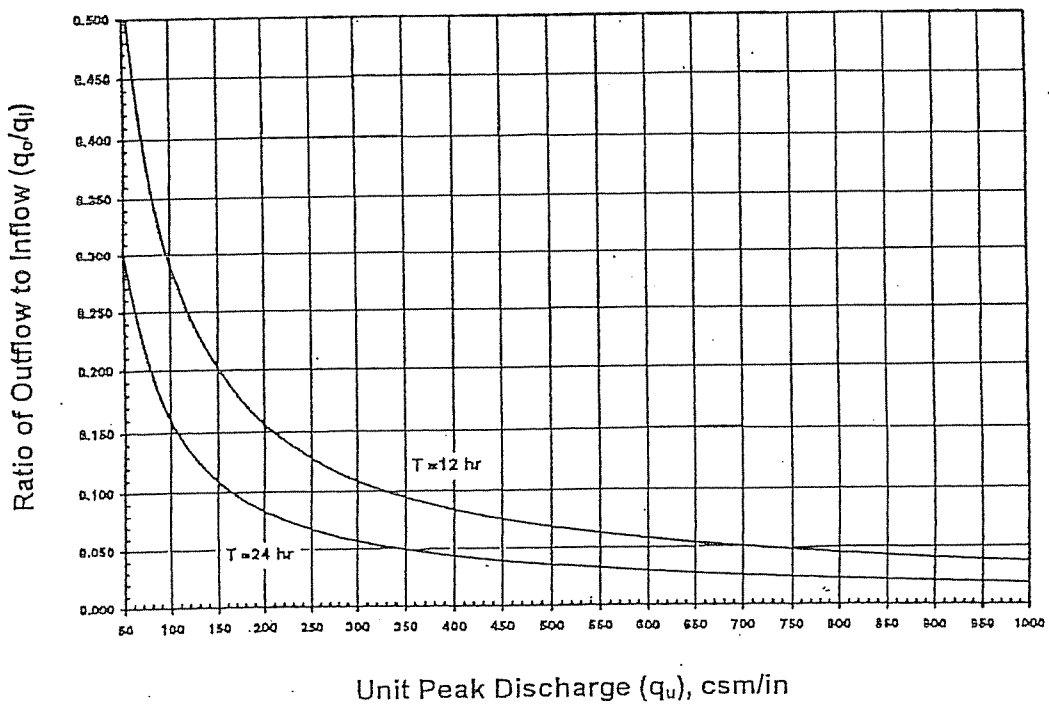
For stream channel protection, provide 24 hours of extended detention (T) for the one-year event.

Compute Channel Protection Storage Volume

First, determine the value of the unit peak discharge ( $q_u$ ) using TR-55 and Type II Rainfall Distribution

- Initial abstraction ( $I_a$ ) for CN of 78 is 0.564: [ $I_a = (200/CN - 2)$ ]
- $I_a/P = (0.564)/2.3 \text{ inches} = 0.245$
- $T_c = 0.35 \text{ hours}$
- Using the above data,  $q_u = 570 \text{ csm/in}$  (cubic feet per second per square mile per year)

Figure 8.5 Detention Time vs. Discharge Ratios (Source: MDE, 2000)



**SPARACO AND YOUNGBLOOD, PLLC**

P.O. Box #818, 18 North Main Street

Harriman, NY 10926

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***WATER QUALITY CALCULATIONS***

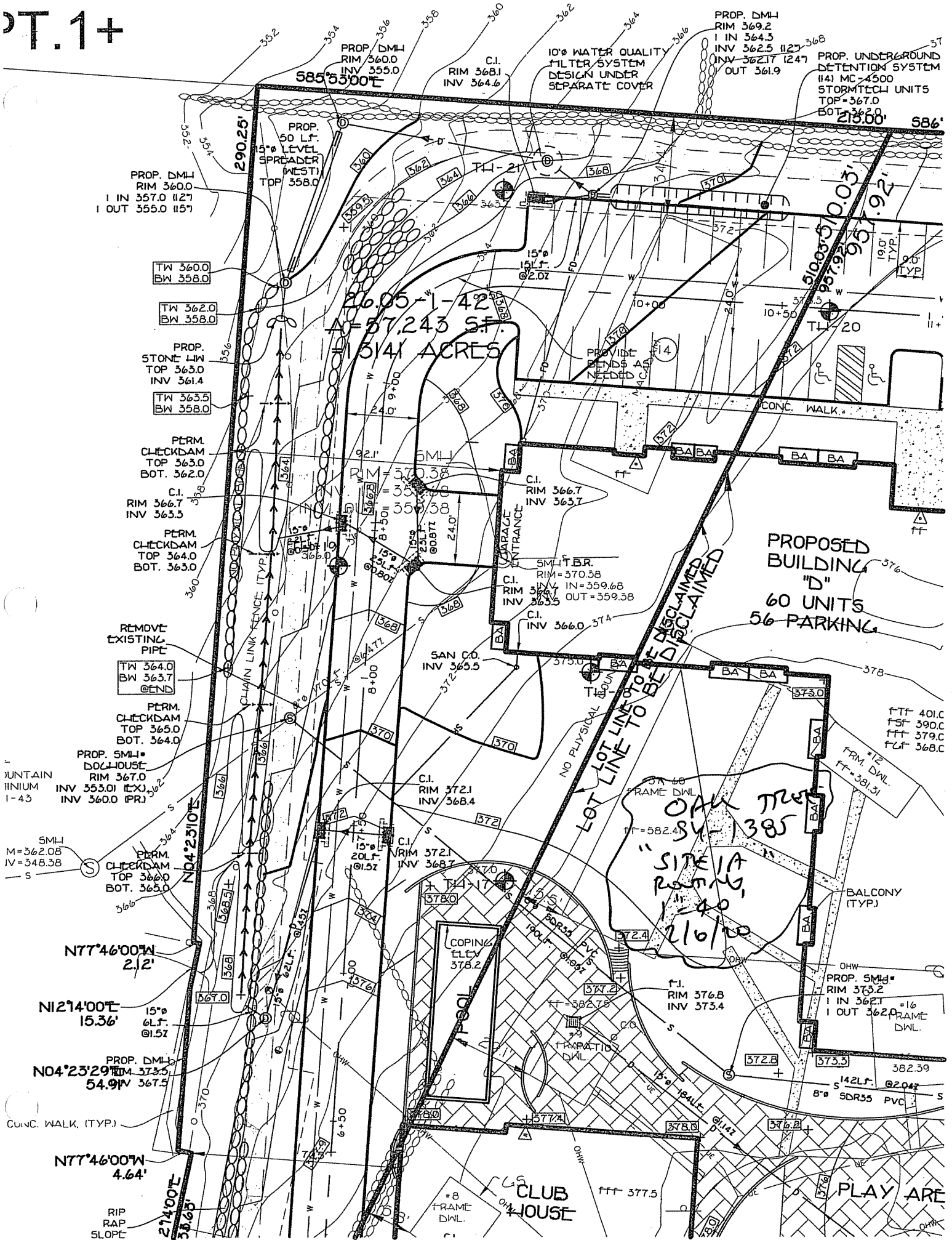
Project: **Oak Tree (SY-1385)**

Location: **Haverstraw, NY**

Drainage Sub-area: **SITE-1A**

Date: **6-Feb-20**

By: **SMS**



PROP. DML  
RIM 360.0  
1 IN 357.0 (127)  
1 OUT 355.0 (157)

TW 360.0  
BW 358.0

TW 362.0  
BW 358.0

PROP. STONE L/W  
TOP 363.0  
INV 361.4

TW 363.5  
BW 358.0

PERM. CHECKDAM  
TOP 363.0  
BOT. 362.0

C.I.  
RIM 366.7  
INV 363.3

PERM. CHECKDAM  
TOP 364.0  
BOT. 363.0

REMOVE EXISTING PIPE

TW 364.0  
BW 363.7  
@END

PERM. CHECKDAM  
TOP 365.0  
BOT. 364.0

PROP. SMLI  
DOCKHOUSE  
RIM 367.0  
1 IN 353.0 (EX) 362  
1 OUT 360.0 (PR) 362

SMLI  
M=362.08  
IV=348.38

PERM. CHECKDAM  
TOP 366.0  
BOT. 365.0

N1214°00'E  
15.36'

15° @L.F.  
@1.57

PROP. DML  
RIM 373.5  
1 IN 367.5  
54.9' @ 367.5

N77°46'00"W  
4.64'

RIP  
RAP  
SLOPE

PROP. DML  
RIM 360.0  
INV 355.0

C.I.  
RIM 368.1  
INV 364.6

10" WATER QUALITY  
FILTER SYSTEM  
DESIGN UNDER  
SEPARATE COVER

PROP. DML  
RIM 369.2  
1 IN 364.3  
INV 362.5 (127)  
OUT 361.9

PROP. UNDERGROUND  
DETECTION SYSTEM  
(14) MC-4500  
STORMTECH UNITS  
TOP=367.0  
BOT=362.0

26.05-1-42  
A=57,243 S.F.  
= 1.3141 ACRES

SMLI T.B.R.  
RIM=370.38  
C.I. RIM 366.7  
INV 363.7

SMLI T.B.R.  
RIM=370.38  
C.I. RIM 366.7  
INV 363.7

SMLI T.B.R.  
RIM=370.38  
C.I. RIM 366.7  
INV 363.7

SAN C.D.  
INV 365.5

C.I.  
RIM 372.1  
INV 368.4

C.I.  
RIM 372.1  
INV 368.7

COPYING  
ELEV 378.2

PROPOSED BUILDING  
"D"  
60 UNITS  
56 PARKING

PROPOSED BUILDING  
"D"  
60 UNITS  
56 PARKING

LOT LINE TO BE DISCLAIMED  
NO PHYSICAL LOT LINE TO BE DISCLAIMED

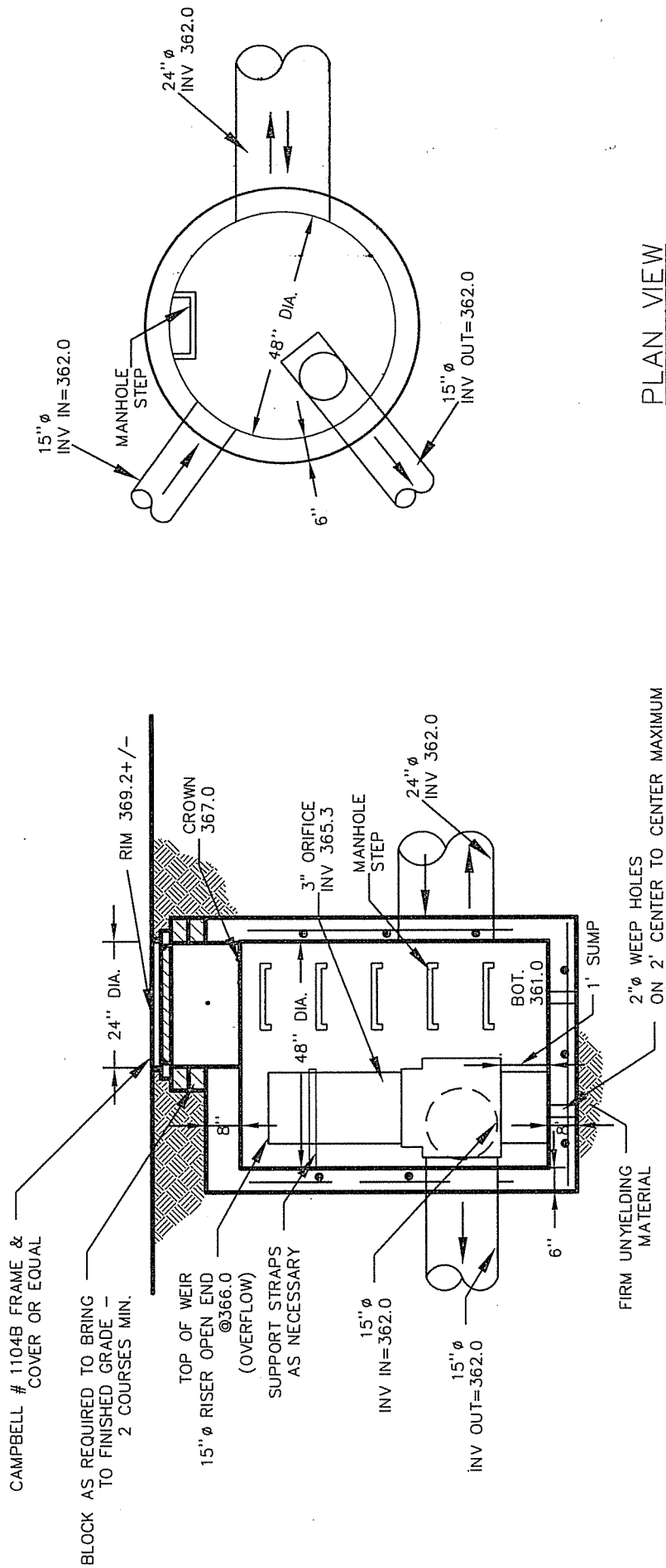
OAK TREE  
SITE 1A  
PLANTING  
1" @ 21/10

FTF 401.C  
FSF 390.C  
FTF 379.C  
FLF 368.C

PROP. SMLI  
RIM 373.2  
1 IN 362.7  
1 OUT 362.0

CLUB  
HOUSE

PLAY AREA



PLAN VIEW

PROFILE VIEW

NOTES:

1. MANHOLE TO CONFORM TO A.S.T.M. C478 (LATEST REVISION).
2. PRECAST CONCRETE MANHOLES WITH RESILIENT SEALS AT JOINTS.
3. MANUFACTURER SHALL CERTIFY ALL COMPONENTS MANHOLE FOR HS20 LOADING
4. RISER SECTION JOINTS SHALL BE FIELD-MORTARED

**OUTLET STRUCTURE (WEST)-MC4500**

N.T.S.

CHAMBERS SHALL CONFORM TO THE REQUIREMENTS OF ASTM F2787  
 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC  
 CORRUGATED WALL STORMWATER COLLECTION CHAMBERS."

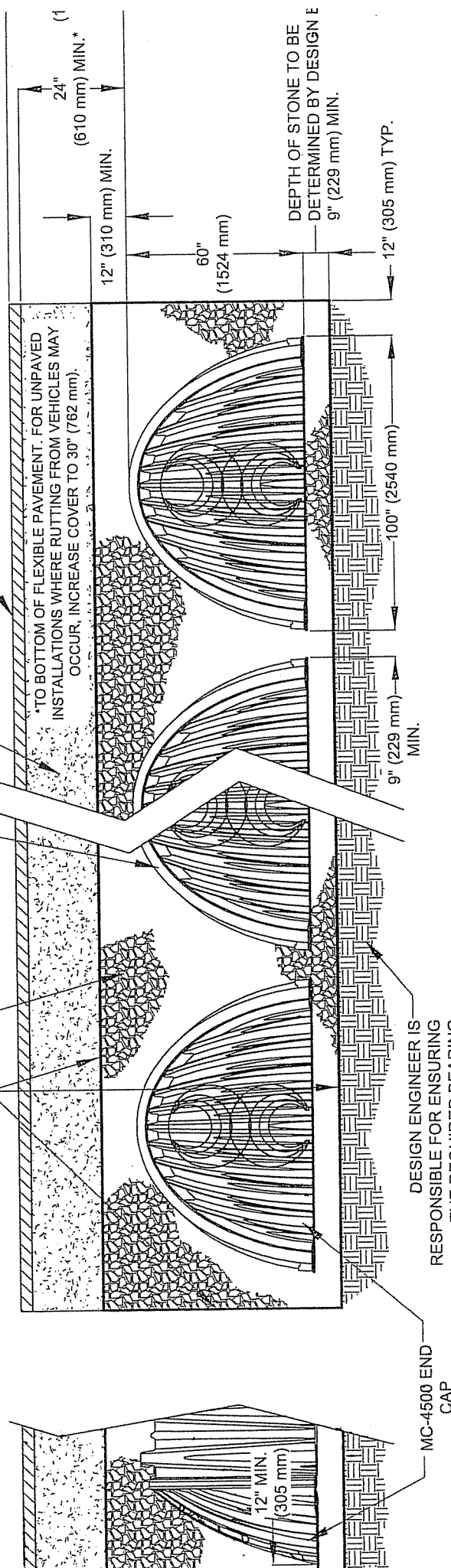
GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES,  
 COMPACT IN 12" (305 mm) MAX LIFTS TO 95% STANDARD PROCTOR  
 DENSITY. SEE THE TABLE OF ACCEPTABLE FILL MATERIALS.

PAVEMENT DESIGN (PER  
 ENGINEER'S DRAWINGS)

\*TO BOTTOM OF FLEXIBLE PAVEMENT. FOR UNPAVED  
 INSTALLATIONS WHERE RUTTING FROM VEHICLES MAY  
 OCCUR, INCREASE COVER TO 30" (762 mm).

NOMINAL 3/4" - 2" (19 mm - 51 mm)  
 CLEAN, CRUSHED, ANGULAR STONE

ADS 601 NON-WOVEN GEOTEXTILE (OR EQUAL)  
 ALL AROUND CLEAN, CRUSHED, ANGULAR STONE

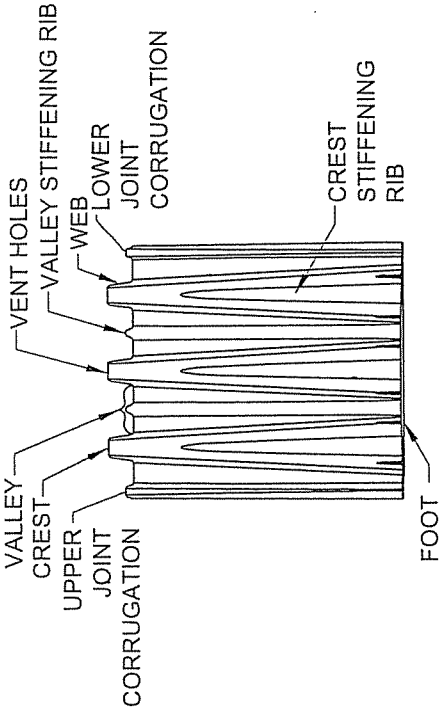
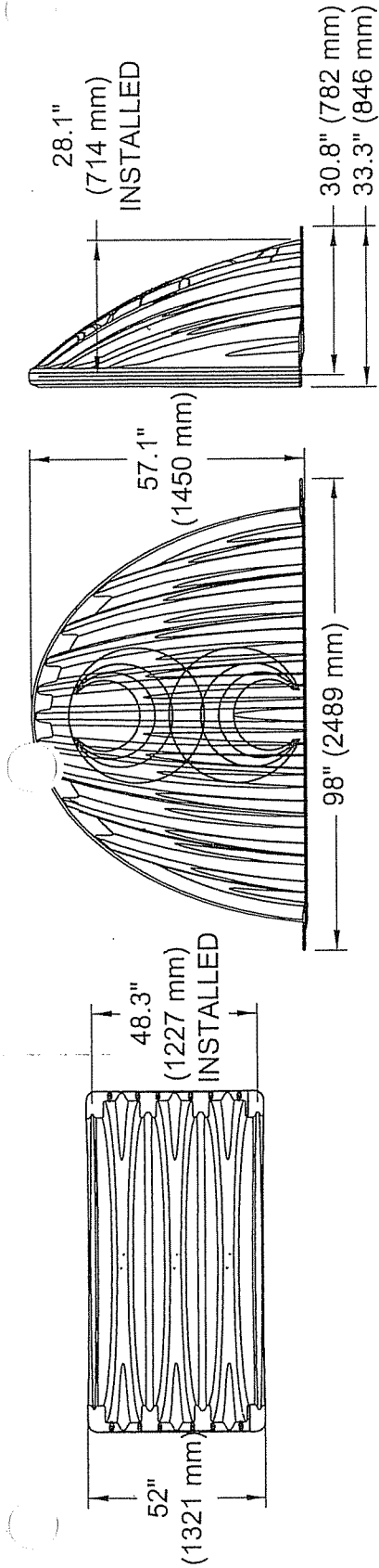


DESIGN ENGINEER IS  
 RESPONSIBLE FOR ENSURING  
 THE REQUIRED BEARING  
 CAPACITY OF SUBGRADE SOILS

THE INSTALLED CHAMBER SYSTEM SHALL PROVIDE THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS  
 SECTION 12.12 FOR EARTH AND LIVE LOADS, WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.

**STORMTECH MC-4500 CROSS-SECTION**

N.T.S.



**NOMINAL CHAMBER SPECIFICATIONS**

SIZE (W x H x INSTALLED LENGTH)  
 100.0" x 60.0" x 48.3" [2540 mm x 1524 mm x 1227 mm]  
 CHAMBER STORAGE  
 106.5 ft³ [3.01 m³]  
 MINIMUM INSTALLED STORAGE\*  
 162.6 ft³ [4.60 m³]  
 NOMINAL WEIGHT  
 128 lbs [58 kg]

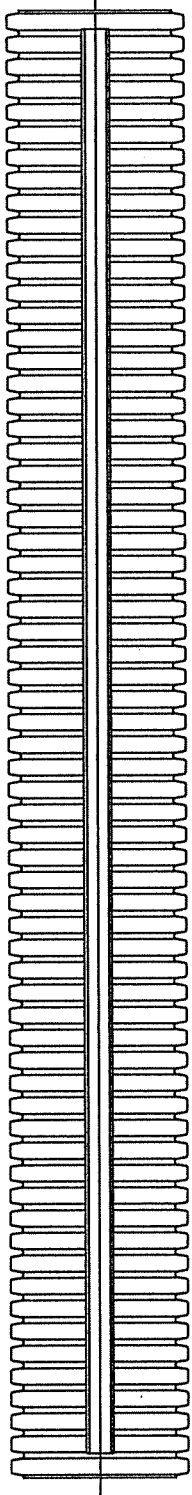
**NOMINAL END CAP SPECIFICATIONS**

SIZE (W x H x INSTALLED LENGTH)  
 98.0" x 57.1" x 28.1" [2489 mm x 1450 mm x 714 mm]  
 END CAP STORAGE  
 26.8 ft³ [0.76 m³]  
 MINIMUM INSTALLED STORAGE\*  
 98.0 ft³ [2.78 m³]  
 NOMINAL WEIGHT  
 80 lbs [36 kg]

**STORMTECH MC-4500 CHAMBER**

N.T.S.



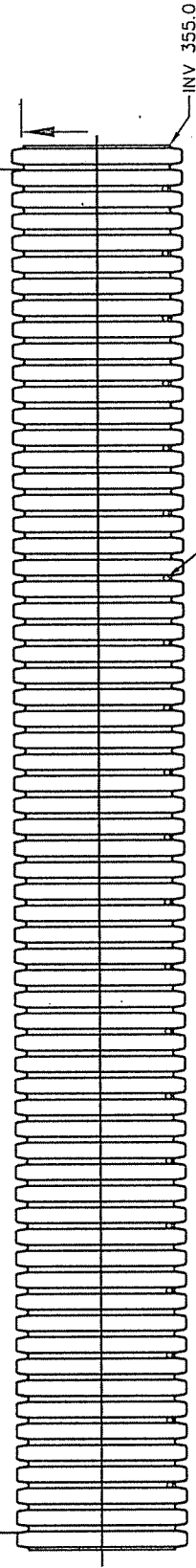


PLAN VIEW

H=12"

TOP 358.00

LEVEL SPREADER



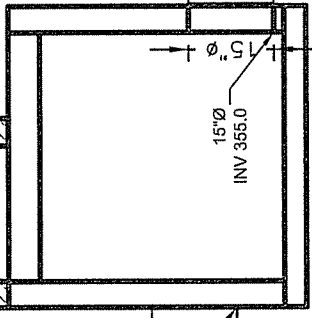
INV 355.0

PERFORATED AS  
PER MANUFACTURER  
PROVIDE STONE AND FILTER FABRIC  
AS PER MANUFACTURER.

ELEVATION VIEW

RIM ELEV 359.0 GRATE

PROPOSED GRADE



15"Ø  
INV IN 355.5

15"Ø  
INV 355.0

15" PIPE  
ADAPTER

40'

PROPOSED GRADE

TOP OF LEVEL SPREADER

15"Ø END CAP

**LEVEL SPREADER (WEST)**

N.T.S.

**SPARACO AND YOUNGBLOOD, PLLC**  
 P.O. Box #818, 18 North Main Street  
 Harriman, NY 10926  
 845-782-8543

**Worksheet 4: Graphical Peak Discharge Method**

Project: **Oak Tree (SY-1385)**  
 Location: **Haverstraw, NY**

By: SMS  
 Date: 6-Feb-20

Shade one: Existing  **Developed**   $q_p$  req'd for Sub-basin: SITE-1A

1. Data:

Drainage Area..... $A_m = \frac{0.0007}{95}$   $mi^2$  (acres/640)  
 Runoff Curve Number..... $CN = 95$  From Worksheet #2 (or calibrated Hec-1 Curve Number)  
 Time of Concentration..... $T_c = 0.083$  hr (From Worksheet #3)  
 Runoff Distribution Type..... = III (I, IA, II, III)  
 Pond and Swamp areas spread  
 throughout watershed..... = 0 percent of  $A_m$  (% acres or  $mi^2$  covered)

	Storm #1	Storm #2	Storm #3
2. Frequency..... yr.	1		
3. Rainfall, P (24 - hour)..... in.	2.5		
4. Initial Abstraction, $I_a$ ..... in. $[I_a = 0.2 \cdot S]$ $[S = 1000/CN - 10] \dots 0.53$	0.105		
5. Compute $I_a/P$ ..... in.	0.042		
6. Unit Peak Discharge, $q_u$ ..... csm/in. (Use $T_c$ and $I_a/P$ with exhibit 4-III)	650		
7. Runoff, Q..... in. $[Q = (P - 0.2S)^2 / (P - 0.8S)]$	1.96		
8. Pond and Swamp Adjustment Factor, $F_p$ ... % (Use percent pond and swamp area with Table 4-2. Factor is 1.0 for zero percent pond and swamp area.)	1		
9. Peak Discharge, $q_p$ ..... cfs (Where $q_p = q_u \cdot A_m \cdot QF_p$ )	0.9		

Project: \_\_\_\_\_



- Chamber Model -
- Units -
- Number of Chambers -
- Number of End Caps -
- Voids in the stone (porosity) -
- Base of Stone Elevation -
- Amount of Stone Above Chambers -
- Amount of Stone Below Chambers -

MC-4500  
 Imperial [Click Here for Metric](#)  
 14  
 2  
 40 %  
 36.25 ft  
 12 in  
 9 in

Individual Chamber Stone Calculations

Height of System (inches)	Incremental Single Chamber (cubic feet)	Incremental Single End Cap (cubic feet)	Incremental Chambers (cubic feet)	Incremental End Cap (cubic feet)	Incremental Stone (cubic feet)	Incremental On EC and Stone (cubic feet)	Cumulative System (cubic feet)	Elevation (feet)
81	0.00	0.00	0.00	0.00	19.22	19.22	2493.96	368.00
80	0.00	0.00	0.00	0.00	19.22	19.22	2474.75	367.92
79	0.00	0.00	0.00	0.00	19.22	19.22	2455.53	367.83
78	0.00	0.00	0.00	0.00	19.22	19.22	2436.32	367.75
77	0.00	0.00	0.00	0.00	19.22	19.22	2417.10	367.67
76	0.00	0.00	0.00	0.00	19.22	19.22	2397.89	367.58
75	0.00	0.00	0.00	0.00	19.22	19.22	2378.67	367.50
74	0.00	0.00	0.00	0.00	19.22	19.22	2359.45	367.42
73	0.00	0.00	0.00	0.00	19.22	19.22	2340.24	367.33
72	0.00	0.00	0.00	0.00	19.22	19.22	2321.02	367.25
71	0.00	0.00	0.00	0.00	19.22	19.22	2301.81	367.17
70	0.00	0.00	0.00	0.00	19.22	19.22	2282.59	367.08
69	0.04	0.00	0.57	0.00	18.99	19.56	2263.38	367.00
68	0.12	0.01	1.63	0.02	18.56	20.20	2243.82	366.92
67	0.16	0.03	2.31	0.05	18.27	20.63	2223.61	366.83
66	0.21	0.05	2.92	0.10	18.01	21.03	2202.98	366.75
65	0.27	0.07	3.76	0.14	17.66	21.55	2181.96	366.67
64	0.45	0.09	6.34	0.18	16.61	23.12	2160.41	366.58
63	0.67	0.11	9.31	0.23	15.40	24.94	2137.28	366.50
62	0.80	0.14	11.19	0.28	14.63	26.10	2112.34	366.42
61	0.91	0.17	12.71	0.34	14.00	27.04	2086.25	366.33
60	1.00	0.19	14.04	0.38	13.45	27.87	2059.20	366.25
59	1.09	0.22	15.22	0.43	12.95	28.61	2031.33	366.17
58	1.16	0.24	16.29	0.48	12.51	29.28	2002.72	366.08
57	1.23	0.27	17.28	0.54	12.09	29.91	1973.45	366.00
56	1.30	0.30	18.20	0.60	11.70	30.49	1943.54	365.92
55	1.36	0.32	19.05	0.65	11.33	31.04	1913.05	365.83
54	1.42	0.35	19.86	0.70	10.99	31.55	1882.01	365.75
53	1.47	0.37	20.63	0.74	10.67	32.04	1850.46	365.67
52	1.53	0.39	21.35	0.79	10.36	32.50	1818.43	365.58
51	1.57	0.42	22.04	0.83	10.06	32.94	1785.93	365.50
50	1.62	0.44	22.70	0.88	9.78	33.36	1752.99	365.42
49	1.67	0.46	23.33	0.93	9.51	33.77	1719.62	365.33
48	1.71	0.48	23.93	0.97	9.26	34.15	1685.86	365.25
47	1.75	0.50	24.50	1.01	9.01	34.52	1651.70	365.17
46	1.79	0.53	25.05	1.05	8.78	34.88	1617.18	365.08
45	1.83	0.55	25.58	1.09	8.55	35.22	1582.30	365.00
44	1.86	0.56	26.09	1.13	8.33	35.55	1547.09	364.92
43	1.90	0.58	26.58	1.17	8.12	35.86	1511.54	364.83
42	1.93	0.60	27.05	1.20	7.92	36.17	1475.68	364.75
41	1.96	0.62	27.50	1.24	7.72	36.46	1439.51	364.67
40	2.00	0.64	27.93	1.28	7.53	36.74	1403.06	364.58
39	2.03	0.66	28.35	1.31	7.35	37.01	1366.32	364.50
38	2.05	0.67	28.75	1.35	7.18	37.28	1329.30	364.42
37	2.08	0.69	29.14	1.38	7.01	37.53	1292.03	364.33
36	2.11	0.71	29.51	1.41	6.84	37.77	1254.50	364.25
35	2.13	0.72	29.87	1.45	6.69	38.01	1216.73	364.17
34	2.16	0.74	30.22	1.48	6.53	38.24	1178.72	364.08
33	2.18	0.76	30.56	1.51	6.39	38.46	1140.48	364.00
32	2.21	0.77	30.88	1.54	6.25	38.67	1102.03	363.92
31	2.23	0.79	31.19	1.57	6.11	38.87	1063.36	363.83
30	2.25	0.80	31.48	1.60	5.98	39.07	1024.49	363.75
29	2.27	0.82	31.77	1.64	5.85	39.26	985.42	363.67
28	2.29	0.84	32.05	1.68	5.72	39.45	946.16	363.58
27	2.31	0.85	32.31	1.69	5.61	39.62	906.70	363.50
26	2.33	0.86	32.56	1.72	5.50	39.78	867.09	363.42
25	2.34	0.87	32.81	1.74	5.40	39.95	827.30	363.33
24	2.36	0.89	33.04	1.77	5.29	40.10	787.36	363.25
23	2.38	0.90	33.26	1.80	5.19	40.25	747.26	363.17
22	2.39	0.91	33.47	1.82	5.10	40.39	707.01	363.08
21	2.41	0.92	33.68	1.84	5.01	40.53	666.61	363.00
20	2.42	0.93	33.87	1.87	4.92	40.66	626.09	362.92
19	2.43	0.95	34.05	1.89	4.84	40.78	585.43	362.83
18	2.44	0.96	34.23	1.91	4.76	40.90	544.65	362.75
17	2.46	0.97	34.39	1.93	4.68	41.01	503.75	362.67
16	2.47	0.98	34.55	1.96	4.61	41.12	462.73	362.58

Oak Tree (SY-1385)  
6-Feb-20

**VOLUME OF SC-3500 SYSTEM  
(ISOLATOR UNITS) FOR: SITE-1A**

STAGE (elev. in ft.)	VOLUME PER UNIT (cubic feet)	VOLUME SYSTEM (ac-ft)
361.25	0.00	0.0000
362.00	172.94	0.0040
363.00	666.61	0.0153
364.00	1140.48	0.0262
365.00	1582.30	0.0363
366.00	1973.45	0.0453
367.00	2263.38	0.0520
368.00	2493.96	0.0573

**VOLUME OF SC-3500 SYSTEM  
(DETENTION UNITS) FOR: SITE-1A**

STAGE (elev. in ft.)	VOLUME PER UNIT (cubic feet)	VOLUME SYSTEM (ac-ft)
361.25	0.00	0.0000
362.00	0.00	0.0000
363.00	0.00	0.0000
364.00	0.00	0.0000
365.00	0.00	0.0000
366.00	0.00	0.0000
367.00	0.00	0.0000
368.00	0.00	0.0000

**COMBINED VOLUME OF SC-3500 SYSTEM FOR:**

STAGE (elev. in ft.)	VOLUME PER UNIT (cubic feet)	VOLUME SYSTEM (ac-ft)
361.25	0.00	0.0000
362.00	172.94	0.0040
363.00	666.61	0.0153
364.00	1140.48	0.0262
365.00	1582.30	0.0363
366.00	1973.45	0.0453
367.00	2263.38	0.0520
368.00	2493.96	0.0573

**SITE-1A**

**SEEPAGE BASIN DATA:**

1) Chamber: 4.03 Ft. Long Chamber End Cap base area: 15.6 sf  
 8.17 Ft. Wide 8 = required number of end caps

Area chambers: 1975.506 sf Area end caps: 124.8 sf

Total Area for Percolation: **2100.306** sf

2) Storage:

$$\begin{aligned} \text{Inside Area of Basin} &= \pi r^2 = \pi (D/2)^2 \\ &= 12.76 \text{ ft}^2 \\ &= 0.00029 \text{ ac} \\ &= 0.0176 \text{ ac} \end{aligned}$$

(for 60 LB)

3) Outflow:

Stage 0.1 Only

Seepage Area (A) = Exterior Area of Base

Stages 1-8

Seepage Area (A) = Sum ( Previous Seepage Area)

$$\begin{aligned} \text{Percolation Rate (V)} &= 1 \text{ inch per } 60 \\ &= 0.000023 \text{ ft./sec} \end{aligned}$$

Minutes (1 Min actual, rounded up for conservative result)

$$\text{Outflow Rate (Q)} = \text{Seepage Area (A)} \times \text{Percolation Rate (V)}$$

Basin Outflow:

**SEEPAGE BASIN STAGE VS. OUTFLOW**

Stage	Area (sq ft)	Seepage Area (ft <sup>2</sup> )	Percolation Rate (ft./sec)	Percolation Rate (ft./sec)	Outflow Rate (g/s)
0.1	361.25	2,100.3	0.000023	0.04862	0.04862
1	362.25	2,100.3	0.000023	0.04862	0.04862
2	363.25	2,100.3	0.000023	0.04862	0.04862
3	364.25	2,100.3	0.000023	0.04862	0.04862
4	365.25	2,100.3	0.000023	0.04862	0.04862
5	366.25	2,100.3	0.000023	0.04862	0.04862

**SPARACO AND YOUNGBLOOD, PLLC**  
P.O. Box #818, 18 North Main Street  
Harriman, NY 10926  
845-782-8543

**Summary Table #WQ-1: Water Quality Volume Calculations**

Project: **Oak Tree (SY-1385)**  
Location: **Haverstraw, NY**  
JOB # **SY-1385**

By: SMS  
Rev. Date: 6-Feb-20

**Water Quality Calculations**

NYSDEC Required Storage Volume:

Sub-Area: SITE-1A

Data:

P: 1.3 = 90% Rainfall Event Number from Figure #1  
Rv: 0.82445 = 0.05 + 0.009(I) (Min. Rv =0.2) Use Rv = 0.82445  
I: 86.05 = Impervious coverage percentage  
A: 0.43 = Site Area to Basin (in acres)

WQV: 0.038 = Req'd Water Quality Volume (in ac-ft)  
=  $\frac{(P)(Rv)(A)}{12}$

Pre Treatment required (20% if percolation rate less than 2-inches per hour and 100% if less than 2-inches per hour):

Percolation Rate: 60 minutes for 1 inch drop.  
Volume percentage required: 100 percent

Pre-treatment volume: 0.038 ac-ft  
Pre-treatment vol. provided: 0.057 ac-ft ok

**Set required WQv Elev:**

Elev. (ft.)	Cumulative Volume (ac-ft)
361.25	0.0453
High: 366.00	0.0000
Low: 361.00	0.0453
Diff. =	

Infiltration System Invert Elevation (EL) = 361.25

Water Quality Storage Elevation Range:

High: 366.00

Low: 361.00

Minimum WQ Volume required above permanent pool = 0.0384 ac-ft

Interpolated Volume Change = ( Higher Cumulative Volume - Req'd WQ Volume over Perm. Pool)/Diff. In Volume in Range

Interpolated Volume Change = ( 0.0453 - 0.0384 ) / 0.0453

Interpolated Volume Ratio = 0.1523

Interpolated Elevation Change = 366.00 - ( 0.1523 x 5.00 )

Interpolated Elevation Change = 365.24 ft.

Minimum Water Quality Volume High Elevation = 365.24 ft.

Set Water Quality Volume Elevation = 365.30 ft.

\*Note: Total Storage at elevation: 365.30 is 0.0390 ac-ft, which is greater than req. 0.0384 ac-ft.

ok

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 845-782-8543

**Summary Table #WQ-2:Runoff Reduction Volume Calculations**

Project: Oak Tree (SY-1385) By: SMS  
 Location: Haverstraw, NY Rev. Date: 6-Feb-20  
 JOB # SY-1385

**Runoff Reduction Volume Calculations**

NYSDEC Required Runoff Reduction Volume for: Sub-Area: SITE-1A

Data: Entire Subarea

P: 1.3 = 90% Rainfall Event Number from Figure #1  
 Rv: 0.950 = 0.05 + 0.009(I) (I=100 percent)  
 Aic: 0.37 = Impervious cover targeted for runoff reduction (in acres)  
 Ai: 0.111 = (S)(Aic) (in acres)  
 S: 0.3 = Hydrologic Soil Group (HSG) Specific Reduction Factor

HSG Type "A" = 0.55  
 HSG Type "B" = 0.4  
 HSG Type "C" = 0.3  
 HSG Type "D" = 0.2

RR<sub>v,i</sub>: 0.011 = Req'd Runoff Reduction Volume (in ac-ft)  
 =  $\frac{(P)(Rv)(Ai)}{12}$

Provided Volume in Stormceptor Chamber system: 0.039 ac-ft up to WQv Elevation. ok, greater than required RR<sub>v,i</sub>.

**\*Note: Current NYSDEC regulations allow RR<sub>v</sub> for 100% of WQv when using infiltration practices.**

Total Available Volume in Stormceptor system: 0.057 ac-ft



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**Channel Protection Storage Volume (Cp<sub>v</sub>): Calculation:**

Project: **Oak Tree (SY-1385)**  
 Location: **Haverstraw, NY**

By: **SMS**  
 Date: **6-Feb-20**

Data:

Water Quality Orifice Invert. . . . . = 361.25 ft.  
 Water Quality Storage Elevation. . . . . = 365.30 ft.

Sub-basin: **SITE-1A**

1.	Unit Peak Discharge, $q_u$ . . . . . =	(csm/in.)	650
	Duration Time, T . . . . . T =	(hr .)	24
	Runoff, Q . . . . . =	(in.)	1.96
	Drainage Area . . . . . Am =	(mi <sup>2</sup> )	0.0007
	Drainage Area (in acres) = $A_m \times 640 = A =$	(acres)	0.43

2. Find  $(q_o/q_i)$  from Figure 8.5. . . . . 0.03  
 ( $q_o/q_i$  = Peak outflow/Peak Inflow discharge)

3. Calculate  $V_s/V_r$  0.642  
 $[V_s/V_r = 0.683 - 1.43(q_o/q_i) + 1.64 (q_o/q_i)^2 - 0.804 (q_o/q_i)^3]$

4.	Solve for $V_s$ . . . . . (ac-ft)	Total $V_s$		(ac-ft)	
		0.0451	<b>0.0451</b>		
	$[V_s = C_{p_v} = (V_s/V_r) \times Q \times A/12]$	(cubic ft.)	1,966	1966	(cubic ft.)

5. Compute Average Release Rate =  $Q_{AVG}$  0.02 (cfs)  
 $[Q_{AVG} = V_s / T * 3600 \text{ sec/hr}]$

**Calculate Required Channel Protection Volume Elevation (Cp<sub>v</sub>E):**

	Elev. (ft.)	Cumulative Volume (ac-ft)	Actual WQ Volume Reser (ac-ft)	Net Volume (ac-ft)
Water Quality Volume Elevation (WQ <sub>vE</sub> ) =	365.30			
Channel Protection Storage Elevation Range: High:	366.00	0.0453	0.0000	0.0453
Low:	361.00	0.0000	0.0000	0.0000
	Diff. =	0.0453	0.0000	0.0453

Min. Channel Protection Volume required = 0.0451 ac-ft

Interpolated Volume Change = ( Higher Net Volume - Req'd Cp Volume over WQ<sub>v</sub>)/Diff. In Volume in Range

Interpolated Volume Ratio = ( 0.0453 - 0.0451 )/ 0.0453

Interpolated Volume Ratio = 0.0038

Interpolated Elevation Change = 366.00 - ( 0.0038 x 5.00 )

Interpolated Elevation Change = 365.98 ft.

Minimum Channel Protection Volume High Elevation = 365.98 ft.

Set Channel Protection Volume Elevation = 366.00 ft.

\*Note: Total Storage at elevation: 366.00 is 0.0453 ac-ft, which is greater than 0.0451 ac-ft.

**Compute the required Cp<sub>v</sub>-ED orifice:**

Required Cpv = 0.0451 ac-ft.

Average ED release rate = 0.0451 x 43560 ft<sup>2</sup>/ac / (24 hr x 3600 sec/hr)

Average ED release rate = 0.02 cfs

\*Size Cpv-ED orifice to release average of: 0.02 - 0.00 cfs

Qavg = 0.02 cfs

Average Cpv-ED orifice rate is:

Average head (h) = (WQ<sub>vE</sub> - WQ<sub>PPE</sub>)/2

Average h =  $\frac{366.00 - 365.30}{2}$

Average h = 0.35 ft.

**\*\*Use the orifice flow equation to calculate the required cross-sectional area and diameter for the Cp<sub>v</sub>-ED orifice:**

[Q=ca(sq. rt. (2gh))]

where:

c = 0.61

g = 32.2

Average h = 0.35

sqrt(2gh) = 4.748

a = 0.008 sq. ft.

used upon: [a=Q/c (sq. rt. (2gh))]

Calculate diameter of pipe based upon area = D = 0.100 ft.

D = 1.200 in.

used upon: [D = sq. rt. (4a/3.15159)]

For Design, Use a 3.00 in. dia. hole. (3" dia. is minimum as per Town Engineer)

Orifice centerline elevation = Orifice invert + (Orifice size in feet/2)

Orifice centerline elevation = 365.30 + 0.13

Orifice centerline elevation = 365.43 ft.

# SPARACO & YOUNGBLOOD, PLLC

Project: Oak Tree (SY-1385)  
 Location: Haverstraw, NY  
 JOB # SY-1385

By: SMS  
 Date: 9-Feb-20  
 Sub-Area: SITE-1A

## Outlet Structure - Elevation vs. Discharge Calculations

Known Data:

### Orifice #1:

Orifice Dia.: 3.00 in.  
 Invert El.: 365.30 ft.  
 Centerline El.: 365.43 ft.  
 A= 0.049 ft<sup>2</sup>

### Orifice #2:

Orifice Dia.: 0.00 in.  
 Invert El.: 366.00 ft.  
 Centerline El.: 366.00 ft.  
 A= 0.000 ft<sup>2</sup>

### Orifice #3:

Orifice Dia.: 0.00 in.  
 Invert El.: 366.00 ft.  
 Centerline El.: 366.00 ft.  
 A= 0.000 ft<sup>2</sup>

### Spillway #1 (Weir):

Spillway Inv. Elev.: 366.0 ft.  
 Spillway Top Elev.: n/a ft.  
 Spillway Length: 3.93 ft.

### Spillway #2 (Top Struct.):

Spillway Inv. Elev.: 0.0 ft.  
 Spillway Top Elev.: n/a ft.  
 Spillway Length: 5.00 ft.

In Orifice Flow Eq. ;  
 $Q=cA\sqrt{2gh}$

c= 0.61 (orifice #1)  
 c= 0.61 (orifice #2)  
 c= 0.61 (orifice #3)  
 c= 0.61 (orifice #4)  
 c= 0.61 (orifice #5)  
 g= 32.2  
 H= (See Below)

In Weir Flow Eq. ;  
 $Q=CLH^{3/2}$

c= 3.0  
 use L= 3.9 > than el.  
 H<sub>1</sub>= (See Below)  
 366.00 ft.

H<sub>1</sub>= Height over orifice centerline  
 H<sub>2</sub>= Height over orifice #2 centerline  
 H<sub>3</sub>= Height over orifice #3 centerline  
 H<sub>4</sub>= Height over orifice #4 invert  
 H<sub>10</sub>= Height over spillway #1 elevation  
 H<sub>11</sub>= Height over spillway #2 elevation

\* c=0.61 for square-edged orifice  
 \*\* c=0.98 for orifice with well-rounded entry  
 (Oct., 1959 Seelye Data Book for Civil Engineers)

**Elevation vs. Discharge**

Elev. (ft.)	Orifice Flows to Orifice #1		Orifice Flows to Orifice #2		Orifice Flows to Orifice #3		Orifice Flows to Orifice #4		Weir Flows over Spillway #1		Weir Flows over Spillway #2		Totals Cumulative Flow (cfs)
	H <sub>1</sub> (ft.)	Flow (cfs)	H <sub>2</sub> (ft.)	Flow (cfs)	H <sub>3</sub> (ft.)	Flow (cfs)	H <sub>4</sub> (ft.)	Flow (cfs)	H <sub>10</sub> (ft.)	Flow (cfs)	H <sub>11</sub> (ft.)	Flow (cfs)	
365.30	0.0	0.00											0.00
365.50	0.0	0.00											0.00
365.70	0.3	0.13											0.13
365.90	0.5	0.17											0.17
366.10	0.7	0.20											0.57
366.30	0.9	0.22							0.1	0.37			2.16
366.50	1.1	0.25							0.5	4.17			4.42
366.70	1.3	0.27							0.7	6.90			7.18
366.90	1.5	0.29							0.9	10.07			10.36
367.10	1.7	0.31							1.1	13.60			13.91
367.30	1.9	0.33							1.3	17.48			17.80
367.40	2.0	0.34							1.4	19.53			19.87
367.60	2.2	0.35							1.6	23.86			24.22
367.80	2.4	0.37							1.8	28.47			28.84
367.90	2.5	0.38							1.9	30.88			31.26
368.00	2.6	0.39							2.0	33.35			33.73
368.10	2.7	0.39							2.1	35.88			36.27
368.20	2.8	0.40							2.2	38.47			38.87
368.30	2.9	0.41							2.3	41.12			41.53
368.40	3.0	0.41							2.4	43.84			44.25
368.50	3.1	0.42							2.5	46.60			47.03
368.60	3.2	0.43							2.6	49.43			49.86
368.70	3.3	0.43							2.7	52.31			52.74
368.80	3.4	0.44							2.8	55.24			55.68
368.90	3.5	0.45							2.9	58.23			58.67
369.00	3.6	0.45							3.0	61.26			61.72
369.10	3.7	0.46							3.1	64.35			64.81
369.20	3.8	0.47							3.2	67.49			67.96
369.30	3.9	0.47							3.3	70.68			71.15
369.40	4.0	0.48							3.4	73.91			74.39
369.50	4.1	0.49							3.5	77.20			77.68
369.60	4.2	0.49							3.6	80.53			81.02
369.70	4.3	0.50							3.7	83.91			84.41
369.80	4.4	0.50							3.8	87.34			87.84
369.90	4.5	0.51							3.9	90.81			91.31
370.00	4.6	0.51							4.0	94.32			94.83
370.10	4.7	0.52							4.1	97.88			98.40
370.20	4.8	0.53							4.2	101.48			102.01
370.30	4.9	0.53							4.3	105.13			105.66
370.40	5.0	0.54							4.4	108.82			109.35
370.50	5.1	0.54							4.5	112.55			113.09
370.60	5.2	0.55							4.6	116.32			116.87
370.70	5.3	0.55							4.7	120.13			120.68
370.80	5.4	0.56							4.8	123.99			124.54
370.90	5.5	0.56							4.9	127.88			128.44
Elev. Flow (cfs)		Orifice #1 Flow (cfs)		Orifice #2 Flow (cfs)		Orifice #3 Flow (cfs)		Orifice #4 Flow (cfs)		Weir #1 Flow (cfs)		Weir #2 Flow (cfs)	Total Flow (cfs)

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***WATER QUALITY CALCULATIONS***

Project: <b><u>Oak Tree SY#1385</u></b>
Location: <b><u>Haverstraw, NY</u></b>
Drainage Sub-area: <b><u>Site-3A</u></b>
Date: <b><u>6-Feb-20</u></b>
By: <b><u>SMS</u></b>

PROPOSED BUILDING "B"  
72 UNITS  
7 PARKING

FTF 403.5  
TSF 392.5  
TTF 381.5  
TGF 370.5

PROP. LHW  
TOP 355.50  
INV 352.0

TOP OF INSITU  
SOILS ELEV. 551.0

12" 80R35 PVC PERFORATED UNDERDRAIN  
10L.F.

TH-2 179.9

PROPOSED  
DETENTION /  
INFILTRATION  
BASIN (EAST)

FOREBAY

PROP. LHW  
TOP 354.0  
INV 350.6

PROP. DMI (DROPI)  
RIM 369.0  
364.6  
359.5

N/F  
GUARINI  
26.05-2-  
LOT 16, BLK. D:

VILLAGE OF WEST HAVEN  
TOWN OF HAVERST

DRAIN #1  
RIM 355.75  
I IN 329.85  
I OUT 329.65

PT 3

25' WIDE  
LANDSCAPE E  
PER FM#7465

RIM 344.48  
INV 336.58 36" CMP  
PROP. INV IN=340.5

HEADWALL  
TW=341.4

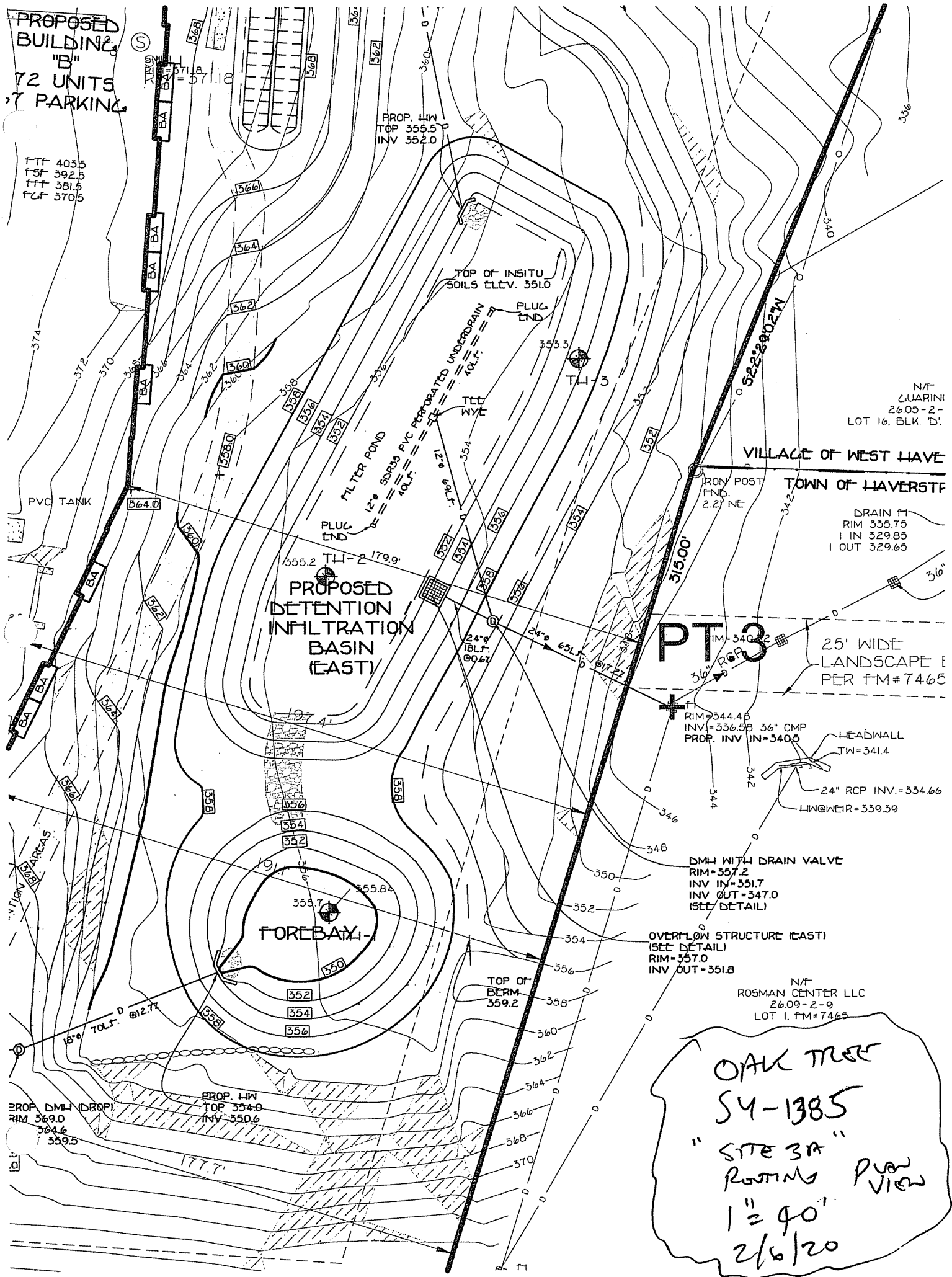
24" RCP INV.=334.66  
LIMOWEIR=339.39

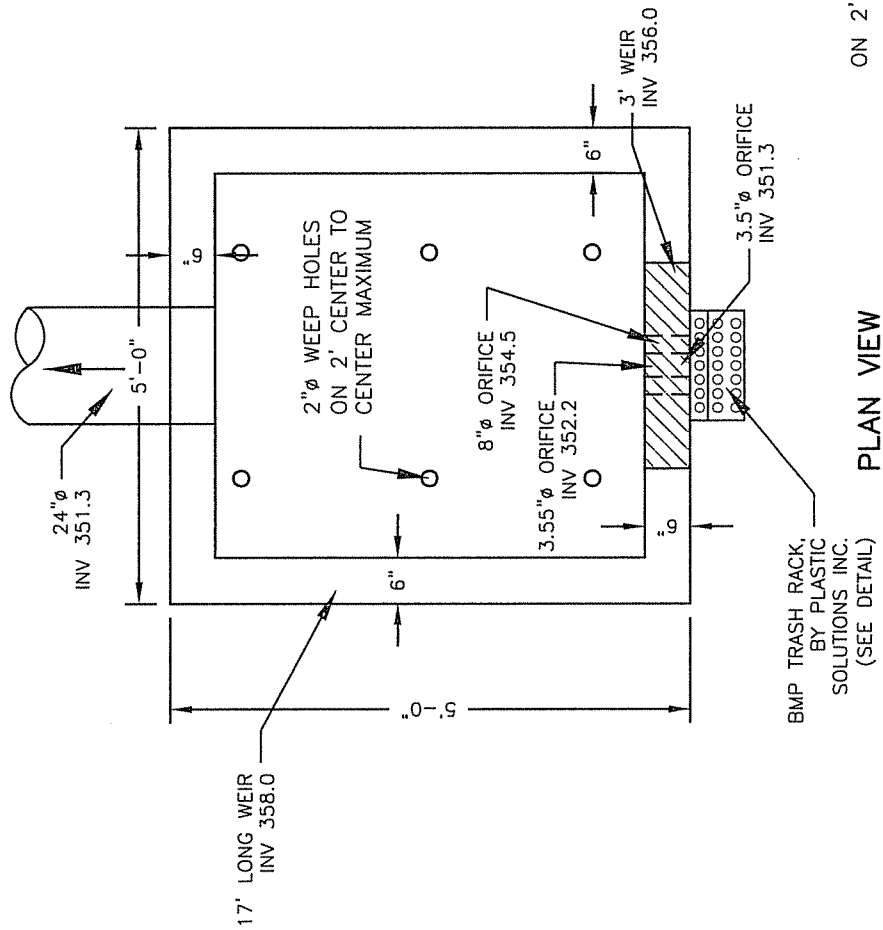
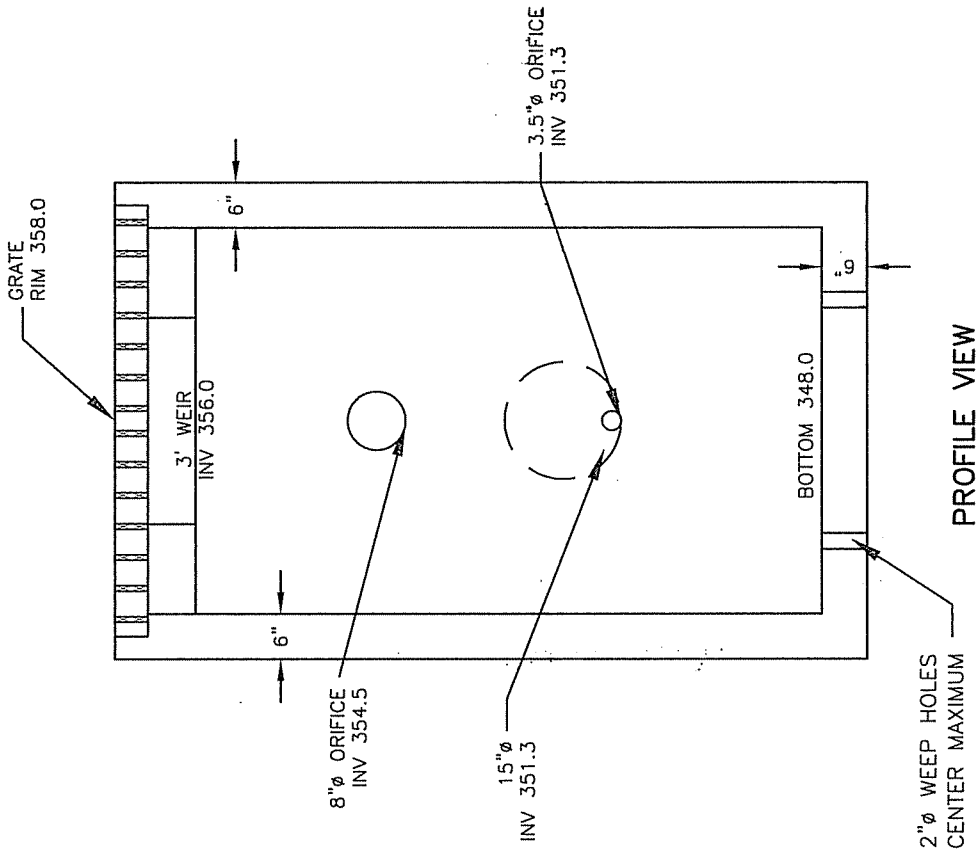
DMI WITH DRAIN VALVE  
RIM=357.2  
INV IN=351.7  
INV OUT=347.0  
(SEE DETAIL)

OVERFLOW STRUCTURE (EAST)  
(SEE DETAIL)  
RIM=357.0  
INV OUT=351.8

N/F  
ROSMAN CENTER LLC  
26.09-2-9  
LOT 1, FM#7465

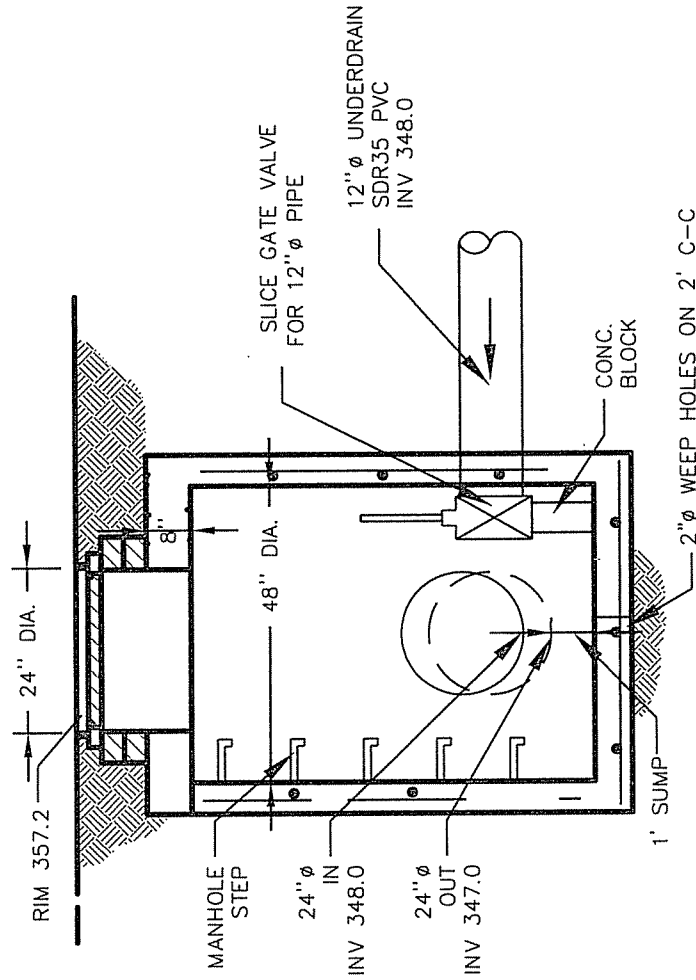
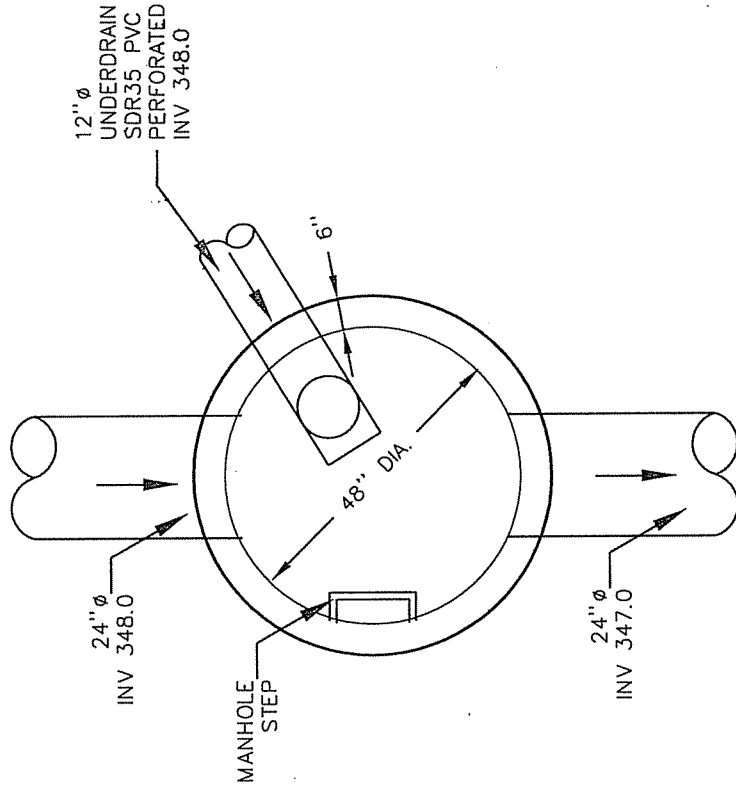
OAK TREE  
54-1385  
"SITE 3A"  
RUMING PLOW VIEW  
1" = 40'  
2/6/20





**OVERFLOW STRUCTURE (EAST)  
DETENTION BASIN**

NTS



**UNDERDRAIN MANHOLE (EAST)**  
N.T.S.



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**Worksheet 2: Runoff Curve Number and Runoff**

Project: **Oak Tree SY#1385**

By: **SMS**

Date: **6-Feb-20**

Location: **Haverstraw, NY**

Checked:

Date:

Shade one: Existing  **Developed**

CN for Sub-basin: **Site-3A**

**1. Runoff Curve Number (CN)**

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> <sup>2</sup> mi <input type="checkbox"/> %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0	0
C	Lawn / Open Space - Good Condition	74			0.46	34.04
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			1.82	178.36
Totals =					2.28	212.4

CN (weighted) =  $\frac{\text{total product}}{\text{total area}} = \frac{212.4}{2.28} = 93.15789474$

Use CN = **93**

**2. Runoff**

Frequency . . . . . yr.  
 Rainfall, P (24 - hour) . . . . . in.  
 Runoff, Q . . . . . in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm #1	Storm #2	Storm #3

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**Worksheet 4: Graphical Peak Discharge Method**

Project: **Oak Tree SY#1385**  
Location: **Haverstraw, NY**

By: SMS  
Date: 6-Feb-20

Shade one: Existing  **Developed**   $q_p$  req'd for Sub-basin: Site-3A

1. Data:

Drainage Area..... $A_m = \frac{0.0036}{1}$  mi<sup>2</sup> (acres/640)  
Runoff Curve Number..... $CN = \frac{93}{1}$  From Worksheet #2 (or calibrated Hec-1 Curve Number)  
Time of Concentration..... $T_c = \frac{0.083}{1}$  hr (From Worksheet #3)  
Runoff Distribution Type..... = III (I, IA, II, III)  
Pond and Swamp areas spread  
throughout watershed..... = 0 percent of  $A_m$  (% acres or mi<sup>2</sup> covered)

Storm #1	Storm #2	Storm #3
----------	----------	----------

2. Frequency..... yr.	1		
3. Rainfall, P (24 - hour)..... in.	2.5		
4. Initial Abstraction, $I_a$ ..... in. $[I_a = 0.2 \cdot S]$ $[S = 1000/CN - 10] \dots \underline{0.73}$	0.147		
5. Compute $I_a/P$ ..... in.	0.059		
6. Unit Peak Discharge, $q_u$ ..... csm/in. (Use $T_c$ and $I_a/P$ with exhibit 4-III)	650		
7. Runoff, Q..... in. $[Q = (P - 0.2S)^2 / (P - 0.8S)]$	1.79		
8. Pond and Swamp Adjustment Factor, $F_p$ ... % (Use percent pond and swamp area with Table 4-2. Factor is 1.0 for zero percent pond and swamp area.)	1		
9. Peak Discharge, $q_p$ ..... cfs (Where $q_p = q_u \cdot A_m \cdot QF_p$ )	4.2		

Oak Tree SY#1385  
6-Feb-20

**Forebay Pond Volume for: Site-3A**

STAGE (elev. in ft.)	DIFFERENCE IN STAGE EL. (ft.)	AREA OF CONTOUR (ft <sup>2</sup> )	AVG. AREA OF CONTOUR (ft <sup>2</sup> )	VOLUME SYSTEM (cubic feet)	VOLUME SYSTEM (ac-ft)
350.00	2.00	1397.00	1161.00	2322	0.0533
352.00	2.00	2322.00	1715.00	3430	0.0787
354.00	2.00	3430.00	2415.00	4830	0.1109
356.00		4830.00			0.2429
Total Volume Forebay					0.2429

**Detention Pond Volume for: Site-3A**

STAGE (elev. in ft.)	DIFFERENCE IN STAGE EL. (ft.)	AREA OF CONTOUR (ft <sup>2</sup> )	AVG. AREA OF CONTOUR (ft <sup>2</sup> )	VOLUME SYSTEM (cubic feet)	VOLUME SYSTEM (ac-ft)
350.00	1.00	0.00	3764.50	3764.5	0.0864
351.00	1.00	7529.00	4416.00	4416	0.1014
352.00	2.00	8832.00	5806.50	11613	0.2666
354.00	2.00	11613.00	7310.00	14620	0.3356
356.00	2.00	14620.00	12778.50	25557	0.5867
358.00	0.50	25557.00	13938.50	6969.25	0.1600
358.50		27877.00			1.5367
Total Volume Pond					1.5367

**SEEPAGE BASIN DATA:**

**Outflow:**

Stage 0.1 Only

Seepage Area (A) = Exterior Area of Base

Stages 1-8

Seepage Area (A) = Sum ( Previous Seepage Area)

Percolation Rate (V) = 1 inch per 60 Minutes  
 = 0.000023 ft/sec

Outflow Rate (Q) = Seepage Area (A) x Percolation Rate (V)

Basin Outflow:

**SEEPAGE BASIN STAGE VS. OUTFLOW**

Stage	Depth (ft)	Seepage Area (ft <sup>2</sup> )	Percolation Rate (ft/sec)	Outflow Rate (g/s)
0.00	350.00	-	0.000023	0.00000
1	351.00	7,529.0	0.000023	<b>0.17428</b>
2	352.00	8,832.0	0.000023	0.20444
3	354.00	11,613.0	0.000023	0.26882
4	356.00	14,620.0	0.000023	0.33843
5	358.00	25,557.0	0.000023	0.59160
6	358.50	27,877.0	0.000023	0.64530

\*Use the bottom of Basin for Outflow Rate for conservative result.

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**Summary Table #WQ-1:Water Quality Volume Calculations**

Project: **Oak Tree SY#1385**  
Location: **Haverstraw, NY**  
JOB # **SY-1385**

By: SMS  
Rev. Date: 6-Feb-20

**Water Quality Calculations**

NYSDEC Required Storage Volume:

Sub-Area: Site-3A

Data:

P: 1.3 = 90% Rainfall Event Number from Figure #1  
Rv: 0.768421 =  $0.05 + 0.009(I)$  (Min. Rv =0.2) Use Rv = 0.768421053  
I: 79.82 = Impervious coverage percentage  
A: 2.28 = Site Area to Basin (in acres)

WQv: 0.190 = Req'd Water Quality Volume (in ac-ft)  
=  $\frac{(P)(Rv)(A)}{12}$

Pre Treatment required (20% if percolation rate less than 2-inches per hour and 100% if less than 2-inches per hour):

Percolation Rate: 60 minutes for 1 inch drop.  
Volume percentage required: 100 percent

Pre-treatment volume Req'd: 0.190 ac-ft  
Pre-treatment Vol. provided: 0.243 ac-ft ok

**Set required WQv Elev:**

Elev. (ft.)	Cumulative Volume (ac-ft)
350.0	
High: 353.00	0.4544
Low: 350.00	0.0000
Diff. =	0.4544

Infiltration System Invert Elevation (I<sub>EL</sub>) =

Water Quality Storage Elevation Range: High: 353.00  
Low: 350.00

Minimum WQ Volume required above permanent pool = 0.1898 ac-ft

Interpolated Volume Change = ( Higher Cumulative Volume - Req'd WQ Volume over Perm. Pool)/Diff. In Volume in Range

Interpolated Volume Change = ( 0.4544 - 0.1898 ) / 0.4544

Interpolated Volume Ratio = 0.5823

Interpolated Elevation Change = 353.00 - ( 0.5823 x 3.00 )

Interpolated Elevation Change = 351.25 ft.

Minimum Water Quality Volume High Elevation = 351.25 ft.

Set Water Quality Volume Elevation = 351.30 ft.

\*Note: Total Storage at elevation: 351.30 is 0.1969 ac-ft, which is greater than req. 0.1898 ac-ft. ok

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**Summary Table #WQ-2:Runoff Reduction Volume Calculations**

Project: Oak Tree SY#1385  
 Location: Haverstraw, NY  
 JOB # SY-1385

By: SMS  
 Rev. Date: 6-Feb-20

**Runoff Reduction Volume Calculations**

NYSDEC Required Runoff Reduction Volume for: Sub-Area: Site-3A

Data: Entire Subarea

P: 1.3 = 90% Rainfall Event Number from Figure #1  
 Rv: 0.950 =  $0.05 + 0.009(I)$  (I=100 percent)  
 Aic: 1.82 = Impervious cover targeted for runoff reduction (in acres)  
 Ai: 0.546 =  $(S)(Aic)$  (in acres)  
 S: 0.3 = Hydrologic Soil Group (HSG) Specific Reduction Factor

HSG Type "A" = 0.55  
 HSG Type "B" = 0.4  
 HSG Type "C" = 0.3  
 HSG Type "D" = 0.2

$RR_{vi} = \frac{0.056}{12} = \text{Req'd Runoff Reduction Volume (in ac-ft)}$
--

Provided Volume in Retention system: 0.197 ac-ft up to WQv Elevation. ok, greater than required  $RR_{vi}$ .

**\*Note: Current NYSDEC regulations allow  $RR_{vi}$  for 100% of WQv when using infiltration practices.**

Total Available Volume in system: 1.537 ac-ft

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**Channel Protection Storage Volume (Cp<sub>v</sub>): Calculation:**

Project: **Oak Tree SY#1385**  
 Location: **Haverstraw, NY**

By: **SMS**  
 Date: **6-Feb-20**

Data:

Water Quality Orifice Invert. . . . . = 350.00 ft.  
 Water Quality Storage Elevation. . . . . = 351.30 ft.

	Sub-basin:	Site-3A
1. Unit Peak Discharge, q <sub>u</sub> . . . . . =	(csm/in.)	650
Duration Time, T . . . . . T =	(hr.)	24
Runoff, Q . . . . . =	(in.)	1.79
Drainage Area . . . . . A <sub>m</sub> =	(mi <sup>2</sup> )	0.0036
Drainage Area (in acres) = A <sub>m</sub> x 640 = A =	(acres)	2.28

2. Find (q<sub>o</sub>/q<sub>i</sub>) from Figure 8.5. . . . . 0.03  
 (q<sub>o</sub>/q<sub>i</sub> = Peak outflow/Peak Inflow discharge)

3. Calculate V<sub>s</sub>/V<sub>r</sub> 0.642  
 [V<sub>s</sub>/V<sub>r</sub> = 0.683-1.43(q<sub>o</sub>/q<sub>i</sub>) + 1.64 (q<sub>o</sub>/q<sub>i</sub>)<sup>2</sup>-0.804 (q<sub>o</sub>/q<sub>i</sub>)<sup>3</sup>]

	Total V <sub>s</sub>	
4. Solve for V <sub>s</sub> . . . . . (ac-ft)	0.2186	<b>0.2186</b> (ac-ft)
[V <sub>s</sub> =Cp <sub>v</sub> = (V <sub>s</sub> /V <sub>r</sub> ) x Q x A/12] (cubic ft.)	9,522	9522 (cubic ft.)

5. Compute Average Release Rate = Q<sub>AVG</sub> 0.11 (cfs)  
 [Q<sub>AVG</sub> = V<sub>s</sub> / T \* 3600 sec/hr]



**Calculate Required Channel Protection Volume Elevation (Cp<sub>v</sub>E):**

Water Quality Volume Elevation (WQ <sub>v</sub> E) =		Elev. (ft.)	Cumulative Volume (ac-ft)	Actual WQ Volume Reserved (ac-ft)	Net Volume (ac-ft)
Channel Protection Storage Elevation Range:		High: 353.00	0.4544	0.0000	0.4544
		Low: 350.00	0.0000	0.0000	0.0000
		Diff. =	0.4544	0.0000	0.4544

Min. Channel Protection Volume required = 0.2186 ac-ft

Interpolated Volume Change = ( Higher Net Volume - Req'd Cp Volume over WQv)/Diff. In Volume in Range

Interpolated Volume Ratio = ( 0.4544 - 0.2186 ) / 0.4544

Interpolated Volume Ratio = 0.5189

Interpolated Elevation Change = 353.00 - ( 0.5189 x 3.00 )

Interpolated Elevation Change = 351.44 ft.

Minimum Channel Protection Volume High Elevation = 351.44 ft.

**Set Channel Protection Volume Elevation = 351.50 ft.**

**\*Note: Total Storage at elevation: 351.50 is 0.2272 ac-ft, which is greater than 0.2186 ac-ft.**

**Compute the required Cp<sub>v</sub>-ED orifice:**

Required Cpv = 0.2186 ac-ft.

Average ED release rate = 0.2186 x 43560 ft<sup>2</sup>/ac / (24 hr x 3600 sec/hr)

Average ED release rate = 0.11 cfs

\*Size Cpv-ED orifice to release average of : 0.11 - 0.00 cfs

**Qavg = 0.11 cfs**

Average Cpv-ED orifice rate is:

Average head (h) = (WQ<sub>v</sub>E - WQ<sub>PPE</sub>)/2

Average h =  $\frac{351.50 - 351.30}{2}$

**Average h = 0.10 ft.**

**\*\*Use the orifice flow equation to calculate the required cross-sectional area and diameter for the Cp<sub>v</sub>-ED orifice:**

[Q=ca(sq. rt. (2gh))]

where:

c = 0.61

g = 32.2

Average h = 0.10

sqrt(2gh) = 2.538

a = 0.071 sq. ft.

Based upon: [a=Q/c (sq. rt. (2gh))]

Calculate diameter of pipe based upon area = D = 0.301 ft.

D = 3.613 in.

Based upon: [D = sq. rt. (4a/3.15159)]

**For Design, Use a 3.50 in. dia. hole. (1" dia. is minimum as per NYSDEC)**

Orifice centerline elevation = Orifice invert + (Orifice size in feet/2)

Orifice centerline elevation = 351.30 + 0.15

**Orifice centerline elevation = 351.45 ft.**

# SPARACO & YOUNGBLOOD, PLLC

Project: Oak Tree SY#1385  
 Location: Town of Haverstraw, NY  
 JOB # SY-1385

By: SMS  
 Date: 6-Feb-20  
 Sub-Area: Site-3A

## Outlet Structure - Elevation vs. Discharge Calculations

Known Data:

### Orifice #1:

Orifice Dia.: 3.50 in.  
 Invert El.: 351.30 ft.  
 Centerline El.: 351.45 ft.  
 A= 0.067 ft<sup>2</sup>

### Orifice #2:

Orifice Dia.: 8.00 in.  
 Invert El.: 354.50 ft.  
 Centerline El.: 354.83 ft.  
 A= 0.349 ft<sup>2</sup>

### Orifice #3:

Orifice Dia.: 0.00 in.  
 Invert El.: 355.00 ft.  
 Centerline El.: 355.00 ft.  
 A= 0.000 ft<sup>2</sup>

### Spillway #1 (Weir):

Spillway Inv. Elev.: 356.0 ft.  
 Spillway Top Elev.: n/a ft.  
 Spillway Length: 3.00 ft.

### Spillway #2 (Top Struct.):

Spillway Inv. Elev.: 356.0 ft.  
 Spillway Top Elev.: n/a ft.  
 Spillway Length: 17.00 ft.

In Orifice Flow Eq. :  
 $Q=cA\sqrt{2gh}$

c= 0.61 (orifice #1)  
 c= 0.61 (orifice #2)  
 c= 0.61 (orifice #3)  
 c= 0.61 (orifice #4)  
 c= 0.61 (orifice #5)  
 g= 32.2  
 H= (See Below)

c= 0.61 (orifice #6)  
 c= 0.61 (orifice #7)  
 c= 0.61 (orifice #8)  
 c= 0.61 (orifice #9)

In Weir Flow Eq. :  
 $Q=cLH^{3/2}$

c= 3.0  
 use L= 3.0 > than el.  
 $H_1 =$  (See Below)  
 356.00 ft.

H<sub>1</sub>= Height over orifice centerline  
 H<sub>2</sub>= Height over orifice #2 centerline  
 H<sub>3</sub>= Height over orifice #3 centerline  
 H<sub>4</sub>= Height over orifice #4 invert  
 H<sub>10</sub>= Height over spillway #1 elevation  
 H<sub>11</sub>= Height over spillway #2 elevation

\* c=0.61 for square-edged orifice  
 \*\* c=0.98 for orifice with well-rounded entry  
 (Oct., 1959 Seebye Data Book for Civil Engineers)

**Elevation vs. Discharge**

Elev. (ft.)	Orifice Flows to Orifice #1		Orifice Flows to Orifice #2		Orifice Flows to Orifice #3		Orifice Flows to Orifice #4		Weir Flows over Spillway #1		Weir Flows over Spillway #2		Totals Cumulative Flow (cfs)
	H <sub>1</sub> (ft.)	Flow (cfs)	H <sub>2</sub> (ft.)	Flow (cfs)	H <sub>3</sub> (ft.)	Flow (cfs)	H <sub>4</sub> (ft.)	Flow (cfs)	H <sub>10</sub> (ft.)	Flow (cfs)	H <sub>11</sub> (ft.)	Flow (cfs)	
351.30	0.0	0.00											0.00
351.50	0.1	0.08											0.08
351.70	0.3	0.16											0.16
351.90	0.5	0.22											0.22
352.10	0.7	0.26											0.26
352.30	0.9	0.30											0.30
352.50	1.1	0.34											0.34
352.70	1.3	0.37											0.37
352.90	1.5	0.39											0.39
353.10	1.7	0.42											0.42
353.30	1.9	0.45											0.45
353.40	2.0	0.46											0.46
353.50	2.1	0.47											0.47
353.60	2.2	0.48											0.48
353.80	2.4	0.50											0.50
354.00	2.6	0.52											0.52
354.20	2.8	0.54											0.54
354.40	3.0	0.56											0.56
354.60	3.2	0.58											0.58
354.80	3.4	0.60											0.60
355.00	3.6	0.62											1.31
355.20	3.8	0.63											1.67
355.40	4.0	0.65											1.94
355.60	4.2	0.67											2.16
355.80	4.4	0.68											2.36
356.00	4.6	0.70											2.54
356.20	4.8	0.71											3.52
356.40	5.0	0.73											5.14
356.60	5.2	0.74											7.20
356.80	5.4	0.76											9.59
357.00	5.6	0.77											12.29
357.20	5.8	0.78											15.24
357.40	6.0	0.80											18.44
357.60	6.2	0.81											21.87
357.80	6.4	0.82											25.50
358.00	6.6	0.84											29.33
358.20	6.8	0.85											37.92
358.40	7.0	0.86											50.45
358.60	7.2	0.87											65.63
358.80	7.4	0.89											82.95
359.00	7.6	0.90											102.15
359.20	7.8	0.91											123.04
359.40	8.0	0.92											145.48
359.60	8.2	0.93											169.36
359.80	8.4	0.95											194.58

Elev. Flow (cfs)      Orifice #1 Flow (cfs)      Orifice #2 Flow (cfs)      Orifice #3 Flow (cfs)      Weir #1 Flow (cfs)      Weir #2 Flow (cfs)      Total Flow (cfs)

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Harriman, NY 10926

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***WATER QUALITY CALCULATIONS***

Project: **Oak Tree**

Location: **Haverstraw, NY**

Drainage Sub-area: **Site-5A**

Date: **6-Feb-20**

By: **SMS**

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**Worksheet 4: Graphical Peak Discharge Method**

Project: **Oak Tree**  
Location: **Haverstraw, NY**

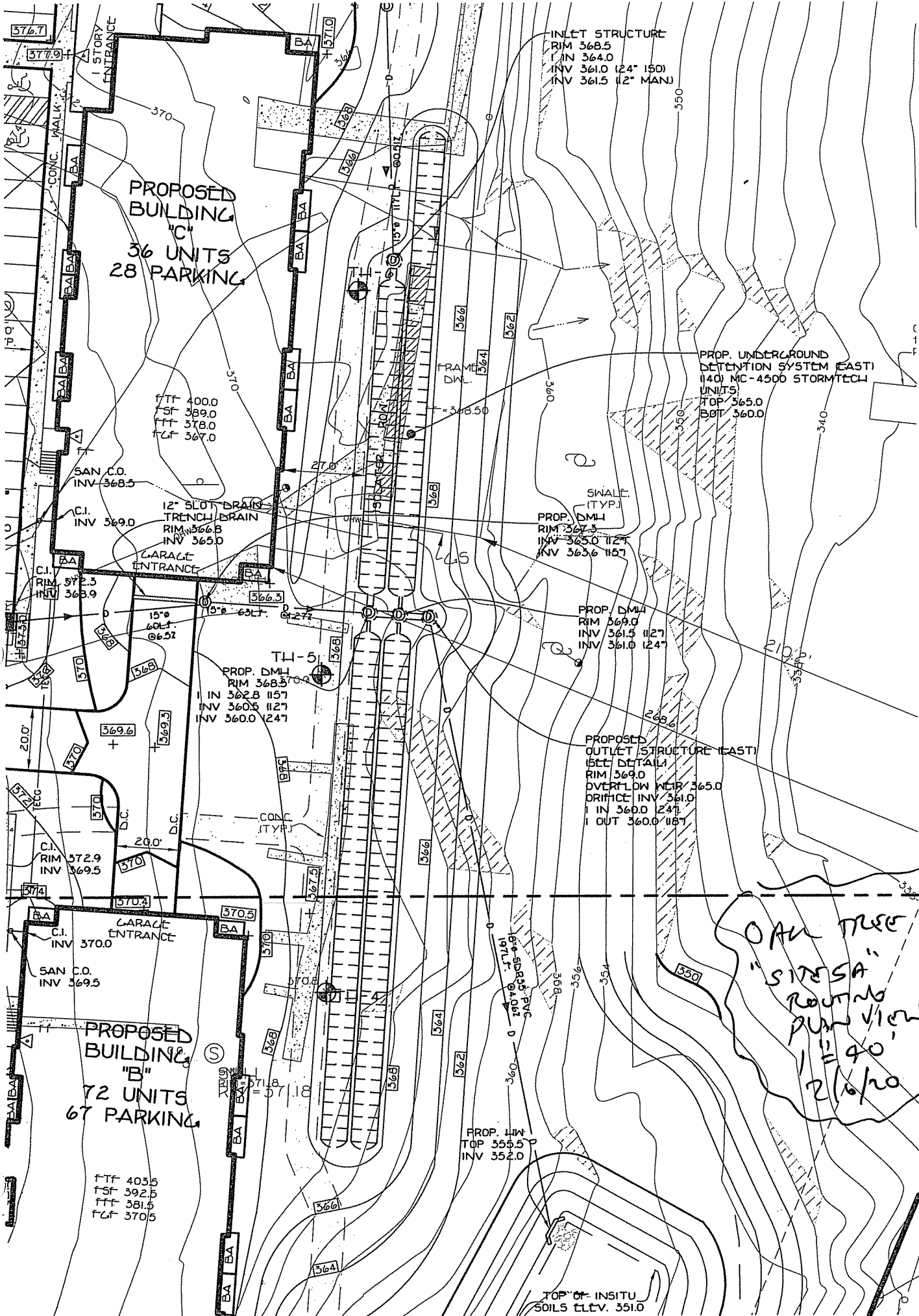
By: SMS  
Date: 6-Feb-20

Shade one: Existing  **Developed**   $q_p$  req'd for Sub-basin: Site-5A

1. Data:

Drainage Area..... $A_m = \frac{0.0067}{1}$  mi<sup>2</sup> (acres/640)  
Runoff Curve Number..... $CN = \frac{93}{1}$  From Worksheet #2 (or calibrated Hec-1 Curve Number)  
Time of Concentration..... $T_c = \frac{0.083}{1}$  hr (From Worksheet #3)  
Runoff Distribution Type..... = III (I, IA, II, III)  
Pond and Swamp areas spread  
throughout watershed..... = 0 percent of  $A_m$  (% acres or mi<sup>2</sup> covered)

	Storm # 1	Storm # 2	Storm # 3
2. Frequency..... yr.	1		
3. Rainfall, P (24 - hour)..... in.	2.5		
4. Initial Abstraction, $I_a$ ..... in. $[I_a = 0.2*S]$ $[S = 1000/CN - 10] \dots 0.75$	0.151		
5. Compute $I_a/P$ ..... in.	0.060		
6. Unit Peak Discharge, $q_u$ ..... csm/in. (Use $T_c$ and $I_a/P$ with exhibit 4-III)	650		
7. Runoff, Q..... in. $[Q = (P - 0.2S)^2 / (P - 0.8S)]$	1.78		
8. Pond and Swamp Adjustment Factor, $F_p$ ... % (Use percent pond and swamp area with Table 4-2. Factor is 1.0 for zero percent pond and swamp area.)	1		
9. Peak Discharge, $q_p$ ..... cfs (Where $q_p = q_u A_m Q F_p$ )	7.7		



INLET STRUCTURE  
 RIM 368.5  
 1 IN 364.0  
 INV 361.0 (24" 150)  
 INV 361.5 (12" MAN)

PROPOSED BUILDING "A"  
 36 UNITS  
 28 PARKING

PROP. UNDERGROUND DETENTION SYSTEM (EAST) (40) MC-4500 STORMTECH UNITS  
 TOP 365.0  
 BOT 360.0

FTF 400.0  
 SF 389.0  
 FTF 378.0  
 TCF 367.0

SAN C.O.  
 INV 368.5

12" SLOT DRAIN TRENCH DRAIN  
 RIM 366.8  
 INV 365.0

PROP. DMH  
 RIM 367.3  
 INV 365.0 (12")  
 INV 363.6 (15")

PROP. DMH  
 RIM 369.0  
 INV 361.5 (12")  
 INV 361.0 (24")

PROP. DMH  
 RIM 368.3  
 INV 362.8 (15")  
 INV 360.5 (12")  
 INV 360.0 (24")

PROPOSED OUTLET STRUCTURE (EAST)  
 SEE DETAIL  
 RIM 369.0  
 OVERTFLOW W/12" 365.0  
 DRIFTCR INV 361.0  
 1 IN 360.0 (24")  
 1 OUT 360.0 (18")

C.I.  
 RIM 372.9  
 INV 369.5

CARAGE ENTRANCE  
 SAN C.O.  
 INV 369.5

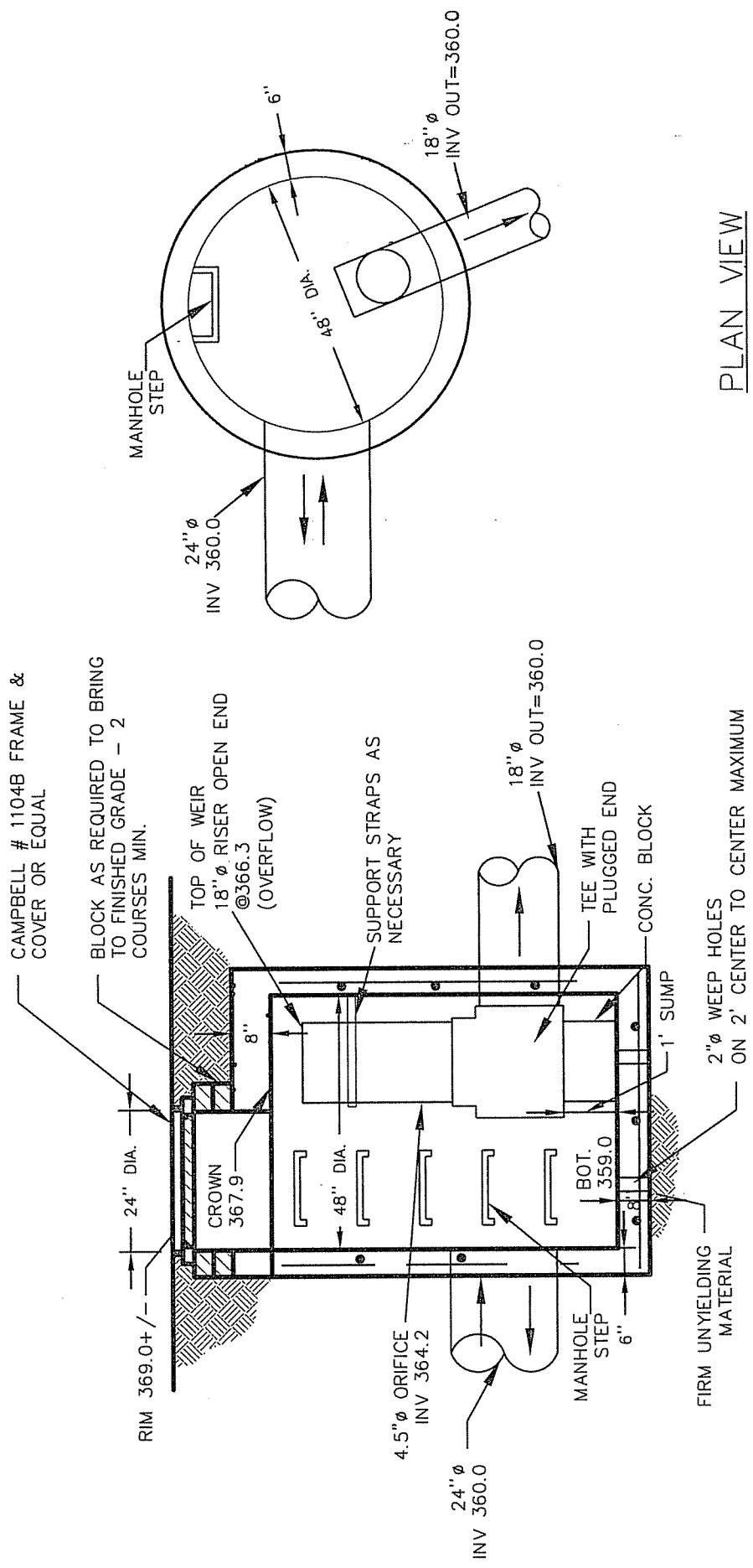
PROPOSED BUILDING "B"  
 72 UNITS  
 67 PARKING

FTF 403.5  
 SF 392.5  
 FTF 381.5  
 TCF 370.5

PROP. LHM  
 TOP 355.5  
 INV 352.0

TOP OF INSITU SOILS ELEV. 351.0

OAK TREE 59-1385  
 "SITE SA"  
 ROUNDED PLAN VIEW  
 1" = 90'  
 2/6/20



PLAN VIEW

PROFILE VIEW

NOTES:

1. MANHOLE TO CONFORM TO A.S.T.M. C478 (LATEST REVISION).
2. PRECAST CONCRETE MANHOLES WITH RESILIENT SEALS AT JOINTS.
3. MANUFACTURER SHALL CERTIFY ALL COMPONENTS MANHOLE FOR HS20 LOADING
4. RISER SECTION JOINTS SHALL BE FIELD-MORTARED

**OUTLET STRUCTURE (EAST)-MC4500**

N.T.S.

CHAMBERS SHALL CONFORM TO THE REQUIREMENTS OF ASTM F2787  
 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC  
 CORRUGATED WALL STORMWATER COLLECTION CHAMBERS."

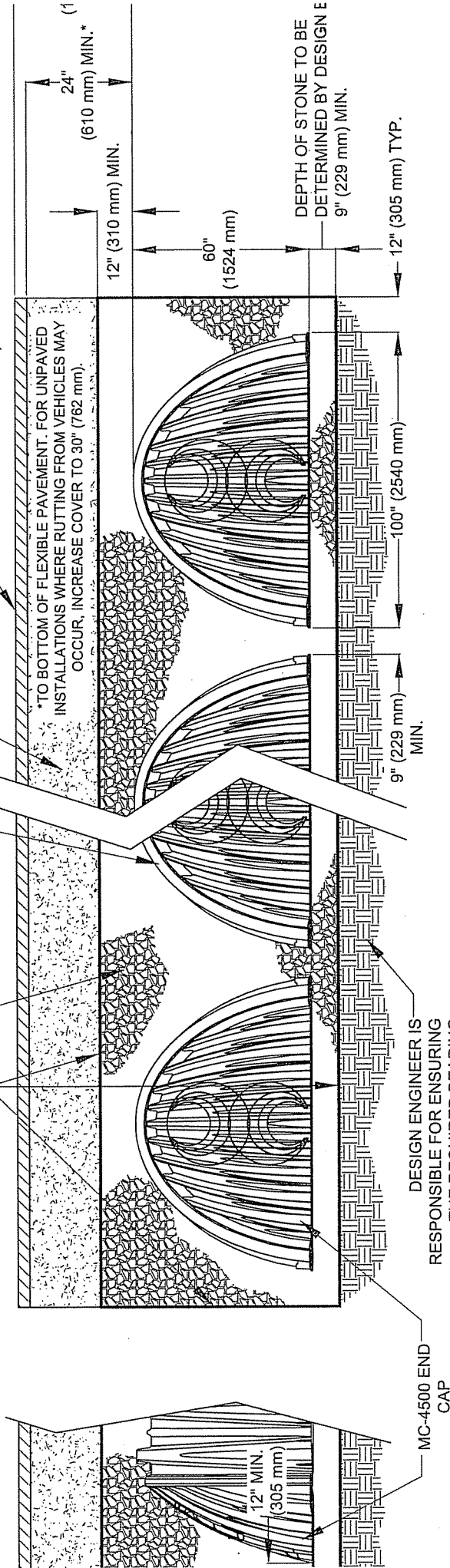
NOMINAL 3/4" - 2" (19 mm - 51 mm)  
 CLEAN, CRUSHED, ANGULAR STONE

ADS 601 NON-WOVEN GEOTEXTILE (OR EQUAL)  
 ALL AROUND CLEAN, CRUSHED, ANGULAR STONE

GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES,  
 COMPACT IN 12" (305 mm) MAX LIFTS TO 95% STANDARD PROCTOR  
 DENSITY. SEE THE TABLE OF ACCEPTABLE FILL MATERIALS.

PAVEMENT DESIGN (PER  
 ENGINEER'S DRAWINGS)

\*TO BOTTOM OF FLEXIBLE PAVEMENT. FOR UNPAVED  
 INSTALLATIONS WHERE RUTTING FROM VEHICLES MAY  
 OCCUR, INCREASE COVER TO 30" (762 mm).



DESIGN ENGINEER IS  
 RESPONSIBLE FOR ENSURING  
 THE REQUIRED BEARING  
 CAPACITY OF SUBGRADE SOILS

MC-4500 END  
 CAP

DEPTH OF STONE TO BE  
 DETERMINED BY DESIGN E  
 9" (229 mm) MIN.

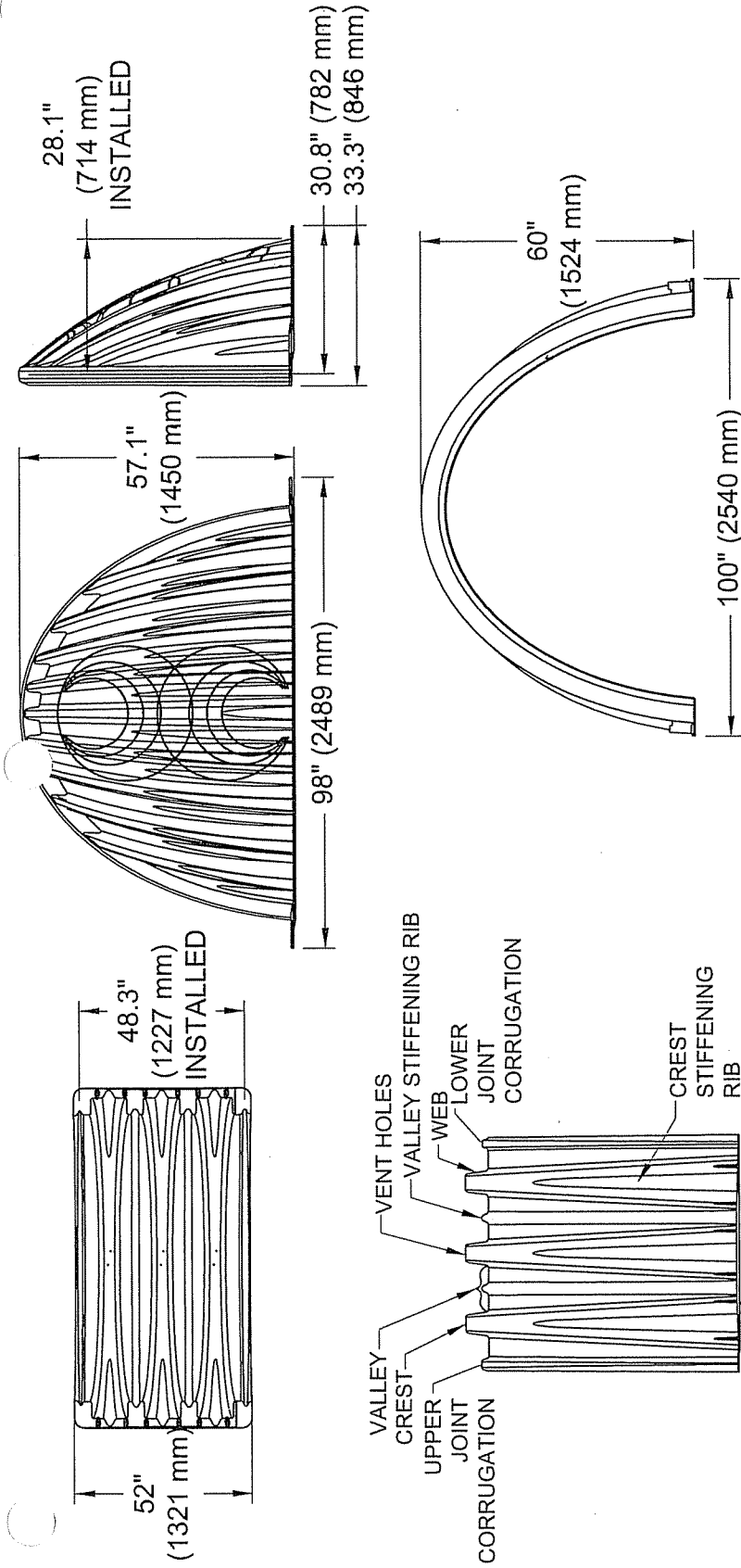
12" (305 mm) TYP.

THE INSTALLED CHAMBER SYSTEM SHALL PROVIDE THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS  
 SECTION 12.12 FOR EARTH AND LIVE LOADS, WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.

**STORMTECH MC-4500 CROSS-SECTION**

N.T.S.





**NOMINAL CHAMBER SPECIFICATIONS**

SIZE (W x H x INSTALLED LENGTH) 100.0" x 60.0" x 48.3" [2540 mm x 1524 mm x 1227 mm]  
 CHAMBER STORAGE 106.5 ft<sup>3</sup> [3.01 m<sup>3</sup>]  
 MINIMUM INSTALLED STORAGE\* 162.6 ft<sup>3</sup> [4.60 m<sup>3</sup>]  
 NOMINAL WEIGHT 128 lbs [58 kg]

**NOMINAL END CAP SPECIFICATIONS**

SIZE (W x H x INSTALLED LENGTH) 98.0" x 57.1" x 28.1" [2489 mm x 1450 mm x 714 mm]  
 END CAP STORAGE 26.8 ft<sup>3</sup> [0.76 m<sup>3</sup>]  
 MINIMUM INSTALLED STORAGE\* 98.0 ft<sup>3</sup> [2.78 m<sup>3</sup>]  
 NOMINAL WEIGHT 80 lbs [36 kg]

**STORMTECH MC-4500 CHAMBER**

N.T.S.

Project: \_\_\_\_\_

- Chamber Model -
- Units -
- Number of Chambers -
- Number of End Caps -
- Voids in the stone (porosity) -
- Base of Stone Elevation -
- Amount of Stone Above Chambers -
- Amount of Stone Below Chambers -

[Click Here for Metric](#)  
 %  
 ft  
 in  
 in  
 in



Initial Perimeter Stone Calculations

SUBAREA  
"SITE 5A"  
ISOLATOR  
ROW

Height of System (inches)	Incremental Single Chamber (cubic feet)	Incremental Single End Cap (cubic feet)	Incremental Chambers (cubic feet)	Incremental End Cap (cubic feet)	Incremental Stone (cubic feet)	Incremental Grand Stone (cubic feet)	Cumulative System (cubic feet)	Elevation (feet)
81	0.00	0.00	0.00	0.00	31.40	31.40	4120.09	365.75
80	0.00	0.00	0.00	0.00	31.40	31.40	4088.69	365.67
79	0.00	0.00	0.00	0.00	31.40	31.40	4057.29	365.58
78	0.00	0.00	0.00	0.00	31.40	31.40	4025.89	365.50
77	0.00	0.00	0.00	0.00	31.40	31.40	3994.49	365.42
76	0.00	0.00	0.00	0.00	31.40	31.40	3963.09	365.33
75	0.00	0.00	0.00	0.00	31.40	31.40	3931.68	365.25
74	0.00	0.00	0.00	0.00	31.40	31.40	3900.28	365.17
73	0.00	0.00	0.00	0.00	31.40	31.40	3868.88	365.08
72	0.00	0.00	0.00	0.00	31.40	31.40	3837.48	365.00
71	0.00	0.00	0.00	0.00	31.40	31.40	3806.08	364.92
70	0.00	0.00	0.00	0.00	31.40	31.40	3774.67	364.83
69	0.04	0.00	0.98	0.00	31.01	31.99	3743.27	364.75
68	0.12	0.01	2.79	0.02	30.28	33.09	3711.28	364.67
67	0.16	0.03	3.95	0.05	29.80	33.81	3678.20	364.58
66	0.21	0.05	5.01	0.10	29.36	34.46	3644.39	364.50
65	0.27	0.07	6.44	0.14	28.77	35.35	3609.92	364.42
64	0.45	0.09	10.87	0.18	26.98	38.03	3574.58	364.33
63	0.67	0.11	15.97	0.23	24.92	41.12	3536.55	364.25
62	0.80	0.14	19.18	0.28	23.62	43.08	3495.43	364.17
61	0.91	0.17	21.80	0.34	22.55	44.68	3452.36	364.08
60	1.00	0.19	24.07	0.38	21.62	46.07	3407.68	364.00
59	1.09	0.22	26.10	0.43	20.79	47.32	3361.60	363.92
58	1.16	0.24	27.92	0.48	20.04	48.45	3314.28	363.83
57	1.23	0.27	29.62	0.54	19.34	49.50	3265.84	363.75
56	1.30	0.30	31.19	0.60	18.69	50.47	3216.34	363.67
55	1.36	0.32	32.66	0.65	18.08	51.39	3165.87	363.58
54	1.42	0.35	34.05	0.70	17.50	52.25	3114.48	363.50
53	1.47	0.37	35.36	0.74	16.96	53.06	3062.23	363.42
52	1.53	0.39	36.60	0.79	16.45	53.84	3009.17	363.33
51	1.57	0.42	37.79	0.83	15.95	54.58	2955.33	363.25
50	1.62	0.44	38.91	0.88	15.48	55.28	2900.76	363.17
49	1.67	0.46	39.99	0.93	15.04	55.95	2845.48	363.08
48	1.71	0.48	41.02	0.97	14.61	56.59	2789.53	363.00
47	1.75	0.50	42.00	1.01	14.20	57.21	2732.93	362.92
46	1.79	0.53	42.94	1.05	13.80	57.80	2675.72	362.83
45	1.83	0.55	43.85	1.09	13.42	58.37	2617.93	362.75
44	1.86	0.56	44.72	1.13	13.06	58.91	2559.56	362.67
43	1.90	0.58	45.56	1.17	12.71	59.44	2500.65	362.58
42	1.93	0.60	46.36	1.20	12.37	59.94	2441.21	362.50
41	1.96	0.62	47.14	1.24	12.05	60.43	2381.27	362.42
40	2.00	0.64	47.88	1.28	11.74	60.90	2320.84	362.33
39	2.03	0.66	48.60	1.31	11.44	61.35	2259.94	362.25
38	2.05	0.67	49.29	1.35	11.15	61.78	2198.59	362.17
37	2.08	0.69	49.96	1.38	10.87	62.20	2136.81	362.08
36	2.11	0.71	50.59	1.41	10.60	62.61	2074.60	362.00
35	2.13	0.72	51.21	1.45	10.34	63.00	2012.00	361.92
34	2.16	0.74	51.81	1.48	10.09	63.37	1949.00	361.83
33	2.18	0.76	52.38	1.51	9.84	63.74	1885.62	361.75
32	2.21	0.77	52.93	1.54	9.61	64.09	1821.89	361.67
31	2.23	0.79	53.46	1.57	9.39	64.42	1757.80	361.58
30	2.25	0.80	53.97	1.60	9.17	64.75	1693.37	361.50
29	2.27	0.82	54.46	1.64	8.96	65.07	1628.63	361.42
28	2.29	0.84	54.94	1.68	8.75	65.37	1563.56	361.33
27	2.31	0.85	55.39	1.69	8.57	65.65	1498.19	361.25
26	2.33	0.86	55.82	1.72	8.39	65.93	1432.54	361.17
25	2.34	0.87	56.24	1.74	8.21	66.19	1366.61	361.08
24	2.36	0.89	56.64	1.77	8.04	66.45	1300.42	361.00
23	2.38	0.90	57.02	1.80	7.88	66.69	1233.98	360.92
22	2.39	0.91	57.38	1.82	7.72	66.92	1167.28	360.83
21	2.41	0.92	57.73	1.84	7.57	67.15	1100.36	360.75
20	2.42	0.93	58.06	1.87	7.43	67.36	1033.21	360.67
19	2.43	0.95	58.38	1.89	7.29	67.56	965.85	360.58
18	2.44	0.96	58.68	1.91	7.17	67.76	898.29	360.50
17	2.46	0.97	58.96	1.93	7.04	67.94	830.53	360.42
16	2.47	0.98	59.23	1.96	6.93	68.11	762.60	360.33

Project: \_\_\_\_\_

- Chamber Model -
- Units -
- Number of Chambers -
- Number of End Caps -
- Voids in the stone (porosity) -
- Base of Stone Elevation -
- Amount of Stone Above Chambers -
- Amount of Stone Below Chambers -

4500	ft	%	ft	in	in
Imperial					
416					
40					
45900					
12					
9					

Click Here for Metric



Include Perimeter Stoning Calculations

SUBAREA  
 "SITE A"  
 DETENTION  
 Ponds

Height of System (inches)	Incremental Single Chamber (cubic feet)	Incremental Single End Cap (cubic feet)	Incremental Chambers (cubic feet)	Incremental End Cap (cubic feet)	Incremental Stone (cubic feet)	Incremental Chamber and Stone (cubic feet)	Cumulative System (cubic feet)	Elevation (feet)
81	0.00	0.00	0.00	0.00	143.52	143.52	19080.50	365.75
80	0.00	0.00	0.00	0.00	143.52	143.52	18936.99	365.67
79	0.00	0.00	0.00	0.00	143.52	143.52	18793.47	365.58
78	0.00	0.00	0.00	0.00	143.52	143.52	18649.96	365.50
77	0.00	0.00	0.00	0.00	143.52	143.52	18506.44	365.42
76	0.00	0.00	0.00	0.00	143.52	143.52	18362.92	365.33
75	0.00	0.00	0.00	0.00	143.52	143.52	18219.41	365.25
74	0.00	0.00	0.00	0.00	143.52	143.52	18075.89	365.17
73	0.00	0.00	0.00	0.00	143.52	143.52	17932.38	365.08
72	0.00	0.00	0.00	0.00	143.52	143.52	17788.86	365.00
71	0.00	0.00	0.00	0.00	143.52	143.52	17645.34	364.92
70	0.00	0.00	0.00	0.00	143.52	143.52	17501.83	364.83
69	0.04	0.00	4.75	0.00	141.62	146.37	17358.31	364.75
68	0.12	0.01	13.47	0.02	138.12	151.61	17211.95	364.67
67	0.16	0.03	19.11	0.05	135.85	155.01	17060.34	364.58
66	0.21	0.05	24.21	0.10	133.79	158.10	16905.32	364.50
65	0.27	0.07	31.13	0.14	131.01	162.27	16747.22	364.42
64	0.45	0.09	52.52	0.18	122.44	175.14	16584.95	364.33
63	0.67	0.11	77.17	0.23	112.56	189.95	16409.81	364.25
62	0.80	0.14	92.69	0.28	106.33	199.30	16219.86	364.17
61	0.91	0.17	105.34	0.34	101.24	206.92	16020.56	364.08
60	1.00	0.19	116.34	0.38	96.83	213.55	15813.64	364.00
59	1.09	0.22	126.13	0.43	92.89	219.45	15600.09	363.92
58	1.16	0.24	134.96	0.48	89.34	224.78	15380.64	363.83
57	1.23	0.27	143.15	0.54	86.04	229.73	15155.86	363.75
56	1.30	0.30	150.76	0.60	82.97	234.33	14926.13	363.67
55	1.36	0.32	157.88	0.65	80.11	238.63	14691.80	363.58
54	1.42	0.35	164.57	0.70	77.41	242.68	14453.17	363.50
53	1.47	0.37	170.91	0.74	74.86	246.50	14210.49	363.42
52	1.53	0.39	176.92	0.79	72.43	250.14	13963.99	363.33
51	1.57	0.42	182.64	0.83	70.13	253.60	13713.85	363.25
50	1.62	0.44	188.08	0.88	67.93	256.89	13460.25	363.17
49	1.67	0.46	193.28	0.93	65.83	260.04	13203.35	363.08
48	1.71	0.48	198.26	0.97	63.83	263.05	12943.31	363.00
47	1.75	0.50	203.01	1.01	61.91	265.93	12680.26	362.92
46	1.79	0.53	207.56	1.05	60.07	268.68	12414.33	362.83
45	1.83	0.55	211.95	1.09	58.30	271.34	12145.65	362.75
44	1.86	0.56	216.16	1.13	56.60	273.89	11874.31	362.67
43	1.90	0.58	220.21	1.17	54.97	276.34	11600.42	362.58
42	1.93	0.60	224.09	1.20	53.40	278.69	11324.08	362.50
41	1.96	0.62	227.83	1.24	51.89	280.96	11045.39	362.42
40	2.00	0.64	231.43	1.28	50.43	283.14	10764.43	362.33
39	2.03	0.66	234.90	1.31	49.03	285.24	10481.29	362.25
38	2.05	0.67	238.24	1.35	47.68	287.27	10196.04	362.17
37	2.08	0.69	241.45	1.38	46.38	289.22	9908.77	362.08
36	2.11	0.71	244.54	1.41	45.14	291.09	9619.56	362.00
35	2.13	0.72	247.53	1.45	43.93	292.90	9328.47	361.92
34	2.16	0.74	250.41	1.48	42.76	294.65	9035.57	361.83
33	2.18	0.76	253.17	1.51	41.64	296.33	8740.92	361.75
32	2.21	0.77	255.84	1.54	40.56	297.95	8444.59	361.67
31	2.23	0.79	258.41	1.57	39.52	299.50	8146.65	361.58
30	2.25	0.80	260.87	1.60	38.53	301.00	7847.14	361.50
29	2.27	0.82	263.24	1.64	37.56	302.45	7546.14	361.42
28	2.29	0.84	265.52	1.68	36.63	303.84	7243.70	361.33
27	2.31	0.85	267.71	1.69	35.75	305.16	6939.86	361.25
26	2.33	0.86	269.81	1.72	34.91	306.43	6634.70	361.17
25	2.34	0.87	271.82	1.74	34.09	307.66	6328.27	361.08
24	2.36	0.89	273.75	1.77	33.31	308.83	6020.61	361.00
23	2.38	0.90	275.59	1.80	32.56	309.95	5711.78	360.92
22	2.39	0.91	277.35	1.82	31.85	311.02	5401.84	360.83
21	2.41	0.92	279.03	1.84	31.16	312.04	5090.82	360.75
20	2.42	0.93	280.63	1.87	30.51	313.02	4778.77	360.67
19	2.43	0.95	282.16	1.89	29.90	313.94	4465.75	360.58
18	2.44	0.96	283.60	1.91	29.31	314.82	4151.81	360.50
17	2.46	0.97	284.97	1.93	28.75	315.66	3836.99	360.42
16	2.47	0.98	286.26	1.96	28.23	316.45	3521.33	360.33

Oak Tree  
 SY-1385  
 6-Feb-20

**VOLUME OF SC-3500 SYSTEM  
 (ISOLATOR UNITS) FOR:** Site-5A

STAGE (elev. in ft.)	VOLUME PER UNIT (cubic feet)	VOLUME SYSTEM (ac-ft)
359.08	0.00	0.0000
359.75	282.62	0.0065
360.75	1100.36	0.0253
361.75	1885.62	0.0433
362.75	2617.93	0.0601
363.75	3265.84	0.0750
364.75	3743.27	0.0859
365.75	4120.09	0.0946

**VOLUME OF SC-3500 SYSTEM  
 (DETENTION UNITS) FOR:** Site-5A

STAGE (elev. in ft.)	VOLUME PER UNIT (cubic feet)	VOLUME SYSTEM (ac-ft)
359.08	0.00	0.0000
359.75	1291.64	0.0297
360.75	5090.82	0.1169
361.75	8740.92	0.2007
362.75	12145.65	0.2788
363.75	15155.86	0.3479
364.75	17358.31	0.3985
365.75	19080.50	0.4380

**COMBINED VOLUME OF SC-3500 SYSTEM FOR:**

STAGE (elev. in ft.)	VOLUME PER UNIT (cubic feet)	VOLUME SYSTEM (ac-ft)
359.08	0.00	0.0000
359.75	1574.26	0.0361
360.75	6191.18	0.1421
361.75	10626.55	0.2440
362.75	14763.58	0.3389
363.75	18421.70	0.4229
364.75	21101.59	0.4844
365.75	23200.60	0.5326

Site-5A

**SEEPAGE BASIN DATA:**

1) Chamber: 4.03 Ft. Long Chamber End Cap base area: 15.6 sf  
 8.17 Ft. Wide 8 = required number of end caps

Area chambers: 4609.514 sf Area end caps: 124.8 sf

Total Area for Percolation: **4734.314** sf

**2) Storage:**

$$\begin{aligned} \text{Inside Area of Basin} &= \pi r^2 = \pi (D/2)^2 \\ &= 12.76 \text{ ft}^2 \\ &= 0.00029 \text{ ac} \\ &= 0.0410 \text{ ac} \end{aligned} \quad (\text{for } 140 \text{ LB})$$

**3) Outflow:**

Stage 0.1 Only

Seepage Area (A) = Exterior Area of Base

Stages 1-8

Seepage Area (A) = Sum ( Previous Seepage Area)

$$\begin{aligned} \text{Percolation Rate (V)} &= 1 \text{ inch per } 14 \text{ Minutes} \\ &= 0.000099 \text{ ft./sec} \end{aligned}$$

$$\text{Outflow Rate (Q)} = \text{Seepage Area (A)} \times \text{Percolation Rate (V)}$$

Basin Outflow:

**SEEPAGE BASIN STAGE VS. OUTFLOW**

Stage	Area (ft <sup>2</sup> )	Seepage Area (ft <sup>2</sup> )	Percolation Rate (ft./sec)	Outflow Rate (ft <sup>3</sup> /s)
0.1	359.08	4,734.3	0.000099	0.46967
1	360.08	4,734.3	0.000099	0.46967
2	361.08	4,734.3	0.000099	0.46967
3	362.08	4,734.3	0.000099	0.46967
4	363.08	4,734.3	0.000099	0.46967
5	364.08	4,734.3	0.000099	0.46967

**SPARACO AND YOUNGBLOOD, PLLC**  
P.O. Box #818, 18 North Main Street  
Harriman, NY 10926  
845-782-8543

**Summary Table #WQ-1:Water Quality Volume Calculations**

Project: Oak Tree  
Location: Haverstraw, NY  
JOB # SY-1385

By: SMS  
Rev. Date: 6-Feb-20

**Water Quality Calculations**

NYSDEC Required Storage Volume:

Sub-Area: Site-5A

Data:

P: 1.3 = 90% Rainfall Event Number from Figure #1  
Rv: 0.77468 = 0.05 + 0.009(I) (Min. Rv =0.2) Use Rv = 0.77468  
I: 80.52 = Impervious coverage percentage  
A: 4.26 = Site Area to Basin (in acres)

WQv: 0.358 = Req'd Water Quality Volume (in ac-ft)  
=  $\frac{(P)(Rv)(A)}{12}$

Pre Treatment required (20% if percolation rate less than 2-inches per hour and 100% if less than 2-inches per hour):

Percolation Rate: 14 minutes for 1 inch drop.  
Volume percentage required: 20 percent

Pre-treatment volume:	0.072 ac-ft
Pre-treatment vol. provided:	0.095 ac-ft
	ok

**Set required WQv Elev:**

Elev. (ft.)	Cumulative Volume (ac-ft)
82.5	
High: 364.75	0.3985
Low: 359.00	0.0000
Diff. =	0.3985

Infiltration System Invert Elevation (EL) =

Water Quality Storage Elevation Range:

High:

Low:

Minimum WQ Volume required above permanent pool = 0.3575 ac-ft

Interpolated Volume Change = ( Higher Cumulative Volume - Req'd WQ Volume over Perm. Pool)/Diff. In Volume in Range

Interpolated Volume Change = ( 0.3985 - 0.3575 ) / 0.3985

Interpolated Volume Ratio = 0.1028

Interpolated Elevation Change = 364.75 - ( 0.1028 x 5.75 )

Interpolated Elevation Change = 364.16 ft.

Minimum Water Quality Volume High Elevation = 364.16 ft.

Set Water Quality Volume Elevation = 364.20 ft.

\*Note: Total Storage at elevation: 364.20 is 0.3604 ac-ft, which is greater than req. 0.3575 ac-ft.

ok

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**Summary Table #WQ-2:Runoff Reduction Volume Calculations**

Project: Oak Tree By: SMS  
 Location: Haverstraw, NY Rev. Date: 6-Feb-20  
 JOB # SY-1385

**Runoff Reduction Volume Calculations**

NYSDEC Required Runoff Reduction Volume for: Sub-Area: Site-5A

Data: Entire Subarea

P: 1.3 = 90% Rainfall Event Number from Figure #1  
 Rv: 0.950 = 0.05 + 0.009(I) (I=100 percent)  
 Aic: 3.43 = Impervious cover targeted for runoff reduction (in acres)  
 Ai: 1.029 = (S)(Aic) (in acres)  
 S: 0.3 = Hydrologic Soil Group (HSG) Specific Reduction Factor

HSG Type "A" = 0.55  
 HSG Type "B" = 0.4  
 HSG Type "C" = 0.3  
 HSG Type "D" = 0.2

RR<sub>v,i</sub>: 0.106 = Req'd Runoff Reduction Volume (in ac-ft)  
 $= \frac{(P)(Rv)(Ai)}{12}$

Provided Volume in Stormceptor Chamber system: 0.360 ac-ft up to WQv Elevation. ok, greater than required RR<sub>v,i</sub>.

**\*Note: Current NYSDEC regulations allow RR<sub>v</sub> for 100% of WQv when using infiltration practices.**

Total Available Volume in Stormceptor system: 0.438 ac-ft



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**Channel Protection Storage Volume (Cp<sub>v</sub>): Calculation:**

Project: **Oak Tree**  
 Location: **Haverstraw, NY**

By: SMS  
 Date: 6-Feb-20

Data:

Water Quality Orifice Invert. . . . . = 82.50 ft.  
 Water Quality Storage Elevation. . . . . = 364.20 ft.

		Sub-basin:	Site-5A
1.	Unit Peak Discharge, $q_u$ . . . . . =	(csm/in.)	650
	Duration Time, T . . . . . T =	(hr .)	24
	Runoff, Q . . . . . =	(in.)	1.78
	Drainage Area . . . . . Am =	(mi <sup>2</sup> )	0.0067
	Drainage Area (in acres) = $A_m \times 640 = A =$	(acres)	4.26

2. Find  $(q_o/q_i)$  from Figure 8.5. . . . . 0.03  
 ( $q_o/q_i$  = Peak outflow/Peak Inflow discharge)

3. Calculate  $V_s/V_r$  0.642  
 $[V_s/V_r = 0.683 - 1.43(q_o/q_i) + 1.64 (q_o/q_i)^2 - 0.804 (q_o/q_i)^3]$

		Total $V_s$	
4.	Solve for $V_s$ (ac-ft)	0.4053	<b>0.4053</b> (ac-ft)
	$[V_s = Cp_v = (V_s/V_r) \times Q \times A/12]$ (cubic ft.)	17,653	17653 (cubic ft.)

5. Compute Average Release Rate =  $Q_{AVG}$  0.20 (cfs)  
 $[Q_{AVG} = V_s / T * 3600 \text{ sec/hr}]$

**Calculate Required Channel Protection Volume Elevation (Cp<sub>v</sub>E):**

Elev. (ft.)	Cumulative Volume (ac-ft)	Actual WQ Volume Reser (ac-ft)	Net Volume (ac-ft)
Water Quality Volume Elevation (WQ <sub>VE</sub> ) = 364.20			
Channel Protection Storage Elevation Range: High: 364.75	0.4380	0.0000	0.4380
Low: 359.00	0.0000	0.0000	0.0000
Diff. =	0.4380	0.0000	0.4380

Min. Channel Protection Volume required = 0.4053 ac-ft

Interpolated Volume Change = ( Higher Net Volume - Req'd Cp Volume over WQ<sub>v</sub>)/Diff. In Volume in Range

Interpolated Volume Ratio = ( 0.4380 - 0.4053 ) / 0.4380

Interpolated Volume Ratio = 0.0748

Interpolated Elevation Change = 364.75 - ( 0.0748 x 5.75 )

Interpolated Elevation Change = 364.32 ft.

Minimum Channel Protection Volume High Elevation = 364.32 ft.

Set Channel Protection Volume Elevation = 364.40 ft.

\*Note: Total Storage at elevation: 364.40 is 0.4114 ac-ft, which is greater than 0.4053 ac-ft.

**Compute the required Cp<sub>v</sub>-ED orifice:**

Required Cpv = 0.4053 ac-ft.

Average ED release rate = 0.4053 x 43560 ft<sup>2</sup>/ac / (24 hr x 3600 sec/hr)

Average ED release rate = 0.20 cfs

\*Size Cpv-ED orifice to release average of : 0.20 - 0.00 cfs

Qavg = 0.20 cfs

Average Cpv-ED orifice rate is:

Average head (h) = (WQ<sub>VE</sub> - WQ<sub>PPE</sub>)/2

Average h =  $\frac{364.40 - 364.20}{2}$

Average h = 0.10 ft.

**\*\*Use the orifice flow equation to calculate the required cross-sectional area and diameter for the Cp<sub>v</sub>-ED orifice:**

[Q=ca(sq. rt. (2gh))]

where:

c = 0.61

g = 32.2

Average h = 0.10

sqrt(2gh) = 2.538

a = 0.132 sq. ft.

based upon: [a=Q/c (sq. rt. (2gh))]

Calculate diameter of pipe based upon area = D = 0.410 ft.

D = 4.919 in.

based upon: [D = sq. rt. (4a/3.15159)]

For Design, Use a 4.50 in. dia. hole. (1" dia. is minimum as per NYSDEC)

Orifice centerline elevation = Orifice invert + (Orifice size in feet/2)

Orifice centerline elevation = 364.20 + 0.19

Orifice centerline elevation = 364.39 ft.

# SPARACO & YOUNGBLOOD, PLLC

Project: Oak Tree  
 Location: Town of Haverstraw, NY  
 JOB # SY-1385

By: SMS  
 Date: 9-Feb-20  
 Sub-Area: Site-5A

## Outlet Structure - Elevation vs. Discharge Calculations

Known Data:

### Orifice #1:

Orifice Dia.: 4.50 in.  
 Invert El.: 364.20 ft.  
 Centerline El.: 364.39 ft.  
 A= 0.110 ft<sup>2</sup>

### Orifice #2:

Orifice Dia.: 0.00 in.  
 Invert El.: 364.40 ft.  
 Centerline El.: 364.40 ft.  
 A= 0.000 ft<sup>2</sup>

### Orifice #3:

Orifice Dia.: 0.00 in.  
 Invert El.: 364.40 ft.  
 Centerline El.: 364.40 ft.  
 A= 0.000 ft<sup>2</sup>

### Spillway #1 (Weir):

Spillway Inv. Elev.: 366.3 ft.  
 Spillway Top Elev.: n/a ft.  
 Spillway Length: 4.71 ft.

### Spillway #2 (Top Struct.):

Spillway Inv. Elev.: 368.0 ft.  
 Spillway Top Elev.: n/a ft.  
 Spillway Length: 5.00 ft.

In Orifice Flow Eq. ;  
 $Q=cA(\text{sq. ft.})(2gh)^{1/2}$

c= 0.61 (orifice #1)  
 c= 0.61 (orifice #2)  
 c= 0.61 (orifice #3)  
 c= 0.61 (orifice #4)  
 c= 0.61 (orifice #5)  
 g= 32.2  
 H= (See Below)

In Weir Flow Eq. ;  
 $Q=cLH^{3/2}$

c= 3.0  
 use L= 4.7 > than el.  
 H<sub>1</sub>= (See Below) 366.30 ft.

H<sub>1</sub>= Height over orifice centerline  
 H<sub>2</sub>= Height over orifice #2 centerline  
 H<sub>3</sub>= Height over orifice #3 centerline  
 H<sub>4</sub>= Height over orifice #4 invert  
 H<sub>10</sub>= Height over spillway #1 elevation  
 H<sub>11</sub>= Height over spillway #2 elevation

\* c=0.61 for square-edged orifice  
 \*\* c=0.98 for orifice with well-rounded entry  
 (Oct., 1959 Seelye Data Book for Civil Engineers)

**Elevation vs. Discharge**

Elev. (ft.)	Orifice Flows to Orifice #1		Orifice Flows to Orifice #2		Orifice Flows to Orifice #3		Orifice Flows to Orifice #4		Weir Flows over Spillway #1		Weir Flows over Spillway #2		Totals Cumulative Flow (cfs)
	H <sub>1</sub> (ft.)	Flow (cfs)	H <sub>2</sub> (ft.)	Flow (cfs)	H <sub>3</sub> (ft.)	Flow (cfs)	H <sub>4</sub> (ft.)	Flow (cfs)	H <sub>10</sub> (ft.)	Flow (cfs)	H <sub>11</sub> (ft.)	Flow (cfs)	
364.20	0.0	0.00											0.00
364.40	0.0	0.00											0.00
364.60	0.2	0.25											0.25
364.80	0.4	0.35											0.35
365.00	0.6	0.42											0.42
365.20	0.8	0.49											0.49
365.40	1.0	0.54											0.54
365.60	1.2	0.60											0.60
365.80	1.4	0.64											0.64
366.00	1.6	0.69											0.69
366.20	1.8	0.73											0.73
366.40	2.0	0.77							0.1	0.45			1.21
366.60	2.2	0.80							0.3	2.32			3.13
366.80	2.4	0.84							0.5	5.00			5.84
367.00	2.6	0.87							0.7	8.28			9.15
367.20	2.8	0.91							0.9	12.06			12.97
367.40	3.0	0.94							1.1	16.30			17.24
367.60	3.2	0.97							1.3	20.94			21.91
367.80	3.4	1.00							1.5	25.96			26.96
368.00	3.6	1.03							1.7	31.32			32.35
368.20	3.8	1.06							1.9	37.01			38.06
368.40	4.0	1.08							2.1	43.00			44.08
368.60	4.2	1.11							2.3	49.29			50.40
368.80	4.4	1.14							2.5	55.85			56.99
369.00	4.6	1.16							2.7	62.69			63.85
369.20	4.8	1.19							2.9	69.78			70.97
369.40	5.0	1.21							3.1	77.12			78.33
369.60	5.2	1.23							3.3	84.71			85.94
369.80	5.4	1.26							3.5	92.52			93.78
370.00	5.6	1.28							3.7	100.56			101.85
370.20	5.8	1.30							3.9	108.83			110.13
370.40	6.0	1.33							4.1	117.31			118.63
370.60	6.2	1.35							4.3	125.99			127.34
370.80	6.4	1.37							4.5	134.88			136.25
371.00	6.6	1.39							4.7	143.98			145.37
371.20	6.8	1.41							4.9	153.26			154.67
371.40	7.0	1.43							5.1	162.74			164.17
371.60	7.2	1.45							5.3	172.41			173.86
371.80	7.4	1.47							5.5	182.26			183.73
372.00	7.6	1.49							5.7	192.29			193.78
372.20	7.8	1.51							5.9	202.50			204.01
372.40	8.0	1.53							6.1	212.88			214.41
372.60	8.2	1.55							6.3	223.44			224.99
372.80	8.4	1.57							6.5	234.16			235.73
373.00	8.6	1.59							6.7	245.05			246.64

Elev. Flow (cfs) Orifice #1 Flow (cfs) Orifice #2 Flow (cfs) Orifice #3 Flow (cfs) Weir #1 Flow (cfs) Weir #2 Flow (cfs) Total Flow (cfs)

*Hec-1 Analyses:*

- 1.) Existing Conditions Hec-1 Model*
- 2.) Developed Conditions Hec-1 Model*

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1U *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 09/17/19 TIME 15:41:00 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *
*****

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## OAK TREE DEVELOPMENT #SY-1385: EXISTING CONDITIONS HEC-1 ANALYSIS

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION. NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE:GREEN AND AMPT INFILTRATION. KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM.

1

HEC-1 INPUT

PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID -----input file:EX-R.ih1-----
2 ID
3 ID HYDROLOGY FOR: OAK TREE(SY #1385)
4 ID TOWN OF HAVERSTRAW, ROCKLAND COUNTY, NEW YORK
5 ID DATE: 9-17-19
6 ID
7 ID ANALYSIS PREPARED BY: SPARACO & YOUNGBLOOD, PLLC
8 ID
9 ID ANALYSIS PARAMETERS:
10 ID EXISTING CONDITIONS RUN
11 ID STORM RECURRENCE INTERVALS = 1, 2, 5, 10, 25 & 100 YEAR
12 ID HYDROGRAPH METHOD: SCS
13 ID RAINFALL DISTRIBUTION: SCS TYPE III
14 ID
15 ID 24 HOUR RAINFALL DATA:
16 ID 1 YEAR: 2.8 INCHES
17 ID 2 YEAR: 3.5 INCHES
18 ID 5 YEAR: 4.5 INCHES
19 ID 10 YEAR: 5.1 INCHES
20 ID 25 YEAR: 6.0 INCHES
21 ID 100 YEAR: 9.0 INCHES
22 ID
23 ID
24 ID *DIAGRAM
24 IT 6 0 0 300
25 IO 3 0
26 JR PREC 2.8 3.5 4.5 5.1 6 9
27 KK SITE-1NORTHWESTERLY SITE RUNOFF TOWARD PT.1
28 KM
29 KM *****
30 KM * DRAINAGE AREA = 4.14 AC = 0.0065 SQ. MI. CN=78 *
31 KM * TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 *
32 KM *****
33 KM
34 BA 0.0065
35 PB 1
36 IN 6
37 PC 0 0.001 0.002 0.003 0.004 0.005 0.006 0.007 0.008 0.009
38 PC 0.010 0.011 0.012 0.013 0.014 0.015 0.016 0.017 0.018 0.019
39 PC 0.020 0.021 0.022 0.023 0.024 0.026 0.027 0.028 0.029 0.030
40 PC 0.0305 0.031 0.032 0.034 0.035 0.036 0.037 0.038 0.040 0.041
41 PC 0.042 0.043 0.045 0.046 0.047 0.049 0.050 0.051 0.053 0.054
42 PC 0.055 0.057 0.058 0.060 0.061 0.063 0.064 0.066 0.067 0.069
43 PC 0.070 0.072 0.074 0.075 0.077 0.079 0.080 0.082 0.084 0.085
44 PC 0.087 0.089 0.091 0.093 0.095 0.097 0.100 0.103 0.106 0.109
45 PC 0.112 0.115 0.118 0.121 0.124 0.127 0.130 0.134 0.137 0.140
46 PC 0.144 0.148 0.151 0.155 0.159 0.163 0.167 0.171 0.176 0.180
47 PC 0.185 0.189 0.194 0.199 0.205 0.210 0.216 0.222 0.228 0.235
48 PC 0.242 0.250 0.258 0.266 0.276 0.287 0.298 0.312 0.328 0.363
49 PC 0.416 0.500 0.584 0.638 0.673 0.689 0.702 0.714 0.725 0.734
50 PC 0.743 0.751 0.758 0.766 0.772 0.779 0.785 0.790 0.796 0.801
51 PC 0.806 0.811 0.816 0.821 0.825 0.829 0.834 0.838 0.842 0.845
52 PC 0.849 0.853 0.857 0.860 0.864 0.867 0.870 0.874 0.877 0.880
53 PC 0.886 0.889 0.892 0.895 0.898 0.900 0.903 0.906 0.908 0.910

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
54      PC   0.911  0.913  0.915  0.917  0.919  0.920  0.922  0.924  0.925  0.927
55      PC   0.929  0.930  0.932  0.933  0.935  0.936  0.938  0.939  0.941  0.942
56      PC   0.944  0.945  0.946  0.948  0.949  0.951  0.952  0.953  0.955  0.956
57      PC   0.957  0.958  0.960  0.961  0.962  0.963  0.965  0.966  0.967  0.968
58      PC   0.969  0.971  0.972  0.973  0.974  0.975  0.976  0.977  0.978  0.979
59      PC   0.981  0.982  0.983  0.984  0.985  0.986  0.987  0.988  0.989  0.990
60      PC   0.991  0.992  0.993  0.994  0.995  0.996  0.997  0.998  0.999  1.000
61      LS    1      78
62      UD    0.1

63      KK   SITE-2SOUTHWESTERLY SITE RUNOFF TOWARD PT.1
64      KM
65      KM *****
66      KM * DRAINAGE AREA = 0.31 AC = 0.0005 SQ. MI.      CN=84      *
67      KM * TIME OF CONCENTRATION = 5 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 *
68      KM *****
69      KM
70      BA   0.0005
71      LS    1      84
72      UD    0.05

73      KK   SITE-3SOUTHEASTERLY SITE RUNOFF TOWARD PT.3
74      KM
75      KM *****
76      KM * DRAINAGE AREA = 3.56 AC = 0.0056 SQ. MI.      CN=78      *
77      KM * TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 *
78      KM *****
79      KM
80      BA   0.0056
81      LS    1      78
82      UD    0.1

83      KK   SITE-4CENTRAL/EASTERLY SITE RUNOFF TOWARD PT.4
84      KM
85      KM *****
86      KM * DRAINAGE AREA = 0.91 AC = 0.0014 SQ. MI.      CN=71      *
87      KM * TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 *
88      KM *****
89      KM
90      BA   0.0014
91      LS    1      71
92      UD    0.1

93      KK   OFF-1OFFSITE SOUTHEASTERLY RUNOFF TOWARD PT.3
94      KM
95      KM *****
96      KM * DRAINAGE AREA = 7.85 AC = 0.0123 SQ. MI.      CN=93      *
97      KM * TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 *
98      KM *****
99      KM
100     BA   0.0123
101     LS    1      93
102     UD    0.1

```

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
103     KK   PT.3ADD SITE-3, SITE-4 AND OFF-1 HYDROGRAPHS
104     HC    3

105     KK   LAG-3LAG PT.2 COMBINED HYDROGRAPH TO PT.4
106     RT    0      0      1

107     KK   SITE-5NORTHEASTERLY SITE RUNOFF TOWARD PT.4
108     KM
109     KM *****
110     KM * DRAINAGE AREA = 5.56 AC = 0.0087 SQ. MI.      CN=76      *
111     KM * TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 *
112     KM *****
113     KM
114     BA   0.0087
115     LS    1      76
116     UD    0.1

117     KK   OFF-2OFFSITE EASTERLY RUNOFF TOWARD PT.4
118     KM
119     KM *****
120     KM * DRAINAGE AREA = 3.32 AC = 0.0052 SQ. MI.      CN=78      *
121     KM * TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 *
122     KM *****
123     KM
124     BA   0.0052
125     LS    1      78
126     UD    0.1

127     KK   PT.4ADD LAG-2, SITE-5 AND OFF-2 HYDROGRAPHS
128     HC    3
129     ZZ

```

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.      (.) CONNECTOR  (<---) RETURN OF DIVERTED OR PUMPED FLOW

27      SITE-1
      .
      .
63      .      SITE-2
      .
      .
73      .      .      SITE-3
      .
      .
83      .      .      .      SITE-4
      .
      .
93      .      .      .      .      OFF-1
      .
      .
103     .      .      .      .      .      PT.3.....
      .      .      .      .      .      V
      .      .      .      .      .      V
105     .      .      .      .      .      LAG-3
      .
      .
107     .      .      .      .      .      .      SITE-5
      .
      .
117     .      .      .      .      .      .      .      OFF-2
      .
      .
127     .      .      .      .      .      .      .      .      PT.4.....

```

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* MAY 1991
* VERSION 4.0.1U
* Lahey F77L-EM/32 version 5.01
* Dodson & Associates, Inc.
* RUN DATE 09/17/19 TIME 15:41:00
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*
*****

```

-----input file:EX-R.ih1-----

HYDROLOGY FOR: OAK TREE(SY #1385)  
TOWN OF HAVERSTRAW, ROCKLAND COUNTY, NEW YORK  
DATE: 9-17-19

ANALYSIS PREPARED BY: SPARACO & YOUNGBLOOD, PLLC

ANALYSIS PARAMETERS:  
EXISTING CONDITIONS RUN  
STORM RECURRENCE INTERVALS = 1, 2, 5, 10, 25 & 100 YEAR  
HYDROGRAPH METHOD: SCS  
RAINFALL DISTRIBUTION: SCS TYPE III

24 HOUR RAINFALL DATA:  
1 YEAR: 2.8 INCHES  
2 YEAR: 3.5 INCHES  
5 YEAR: 4.5 INCHES  
10 YEAR: 5.1 INCHES  
25 YEAR: 6.0 INCHES  
100 YEAR: 9.0 INCHES

```

25 IO      OUTPUT CONTROL VARIABLES
      IPRNT      3      PRINT CONTROL
      IPLOT      0      PLOT CONTROL
      QSCAL      0.      HYDROGRAPH PLOT SCALE

```

```

IT      HYDROGRAPH TIME DATA
      NMIN      6      MINUTES IN COMPUTATION INTERVAL
      IDATE      1      0      STARTING DATE
      ITIME      0000      STARTING TIME
      NQ      300      NUMBER OF HYDROGRAPH ORDINATES
      NDDATE      2      0      ENDING DATE
      NDTIME      0554      ENDING TIME
      ICENT      19      CENTURY MARK

```

COMPUTATION INTERVAL 0.10 HOURS  
TOTAL TIME BASE 29.90 HOURS

ENGLISH UNITS  
DRAINAGE AREA SQUARE MILES  
PRECIPITATION DEPTH INCHES  
LENGTH, ELEVATION FEET  
FLOW CUBIC FEET PER SECOND



STORAGE VOLUME      ACRE- FEET  
SURFACE AREA        ACRES  
TEMPERATURE        DEGREES FAHRENHEIT

JP            MULTI-PLAN OPTION  
              NPLAN            1    NUMBER OF PLANS

JR            MULTI-RATIO OPTION  
              RATIOS OF PRECIPITATION  
              2.80    3.50    4.50    5.10    6.00    9.00

\*\*\*\*\*

27' KK        \*\*\*\*\*  
              \*                    \*  
              \*    SITE-1    \*            NORTHWESTERLY SITE RUNOFF TOWARD PT.1  
              \*                    \*  
              \*\*\*\*\*

\*\*\*\*\*  
\* DRAINAGE AREA = 4.14 AC = 0.0065 SQ. MI.            CN=78            \*  
\* TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100            \*  
\*\*\*\*\*

36 IN        TIME DATA FOR INPUT TIME SERIES  
              JXMIN            6    TIME INTERVAL IN MINUTES  
              JXDATE        1    0    STARTING DATE  
              JXTIME        0    0    STARTING TIME

SUBBASIN RUNOFF DATA

34 BA        SUBBASIN CHARACTERISTICS  
              TAREA            0.01    SUBBASIN AREA

PRECIPITATION DATA

35 PB        STORM            1.00    BASIN TOTAL PRECIPITATION

37 PI        INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.01	0.00	0.01	0.00	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.02	0.03	0.05
0.08	0.08	0.05	0.03	0.02	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.00	0.01	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

61 LS        SCS LOSS RATE  
              STRTL            1.00    INITIAL ABSTRACTION  
              CRVNBR        78.00    CURVE NUMBER  
              RTIMP            0.00    PERCENT IMPERVIOUS AREA

62 UD        SCS DIMENSIONLESS UNITGRAPH  
              TLAG            0.10    LAG

\*\*\*

UNIT HYDROGRAPH  
7 END-OF-PERIOD ORDINATES

16.	17.	6.	2.	1.	0.	0.
TOTAL RAINFALL =	1.00,	TOTAL LOSS =	1.00,	TOTAL EXCESS =	0.00	
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
+    0.	0.10	0.	0.	0.	0.	
		(INCHES)	0.000	0.000	0.000	0.000
		(AC-FT)	0.	0.	0.	0.
		CUMULATIVE AREA =	0.01 SQ MI			

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION    SITE-1  
FOR PLAN 1, RATIO = 2.80

TOTAL RAINFALL =    2.80, TOTAL LOSS =    2.10, TOTAL EXCESS =    0.70

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	2.	12.30	(CFS)	0.	0.	0.	0.
			(INCHES)	0.574	0.701	0.701	0.701
			(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA =			0.01 SQ MI				

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION    SITE-1  
FOR PLAN 1, RATIO = 3.50

TOTAL RAINFALL =    3.50, TOTAL LOSS =    2.33, TOTAL EXCESS =    1.17

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	4.	12.30	(CFS)	1.	0.	0.	0.
			(INCHES)	0.982	1.175	1.175	1.175
			(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA =			0.01 SQ MI				

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION    SITE-1  
FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL =    4.50, TOTAL LOSS =    2.56, TOTAL EXCESS =    1.94

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	7.	12.30	(CFS)	1.	0.	0.	0.
			(INCHES)	1.630	1.938	1.938	1.938
			(AC-FT)	1.	1.	1.	1.
CUMULATIVE AREA =			0.01 SQ MI				

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION    SITE-1  
FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL =    5.10, TOTAL LOSS =    2.67, TOTAL EXCESS =    2.43

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	9.	12.30	(CFS)	1.	0.	0.	0.
			(INCHES)	2.040	2.429	2.429	2.429
			(AC-FT)	1.	1.	1.	1.
CUMULATIVE AREA =			0.01 SQ MI				

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION    SITE-1  
FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL =    6.00, TOTAL LOSS =    2.80, TOTAL EXCESS =    3.20

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	12.	12.20	(CFS)	2.	1.	0.	0.
			(INCHES)	2.678	3.197	3.197	3.197
			(AC-FT)	1.	1.	1.	1.
CUMULATIVE AREA =			0.01 SQ MI				

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION    SITE-1  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 3.09, TOTAL EXCESS = 5.91

PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 + (CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + 22. 12.20 (CFS) 3. 1. 1. 1.  
 (INCHES) 4.869 5.915 5.915 5.915  
 (AC-FT) 2. 2. 2. 2.  
 CUMULATIVE AREA = 0.01 SQ MI

\*\*\* \*\*

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 \* \*  
 63 KK \* SITE-2 \* SOUTHWESTERLY SITE RUNOFF TOWARD PT.1  
 \* \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DRAINAGE AREA = 0.31 AC = 0.0005 SQ. MI. CN=84 \*  
 \* TIME OF CONCENTRATION = 5 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 \*  
 \*\*\*\*\*

SUBBASIN RUNOFF DATA

70 BA SUBBASIN CHARACTERISTICS  
 TAREA 0.00 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN  
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
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 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.02 0.03  
 0.08 0.08 0.05 0.03 0.02 0.01 0.01 0.01 0.01 0.01  
 0.01 0.01 0.01 0.01 0.01 0.01 0.00 0.01 0.00 0.00  
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.01  
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
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 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

71 LS SCS LOSS RATE  
 STRFL 1.00 INITIAL ABSTRACTION  
 CRVNER 84.00 CURVE NUMBER  
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

72 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 0.05 LAG

\*\*\*

UNIT HYDROGRAPH  
 5 END-OF-PERIOD ORDINATES

2. 1. 0. 0. 0.

TOTAL RAINFALL = 1.00, TOTAL LOSS = 1.00, TOTAL EXCESS = 0.00

PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 + (CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + 0. 0.10 (CFS) 0. 0. 0. 0.  
 (INCHES) 0.000 0.000 0.000 0.000  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITE-2

FOR PLAN 1, RATIO = 2.80

TOTAL RAINFALL = 2.80, TOTAL LOSS = 1.93, TOTAL EXCESS = 0.87

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	12.20	0.	0.	0.	0.
		(INCHES) 0.724	0.875	0.875	0.875
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-2  
FOR PLAN 1, RATIO = 3.50

TOTAL RAINFALL = 3.50, TOTAL LOSS = 2.08, TOTAL EXCESS = 1.42

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	12.20	0.	0.	0.	0.
		(INCHES) 1.200	1.419	1.419	1.419
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-2  
FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL = 4.50, TOTAL LOSS = 2.23, TOTAL EXCESS = 2.27

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
1.	12.20	0.	0.	0.	0.
		(INCHES) 1.924	2.267	2.267	2.267
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-2  
FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL = 5.10, TOTAL LOSS = 2.30, TOTAL EXCESS = 2.80

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
1.	12.20	0.	0.	0.	0.
		(INCHES) 2.370	2.799	2.799	2.799
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-2  
FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 2.38, TOTAL EXCESS = 3.62

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
1.	12.20	0.	0.	0.	0.
		(INCHES) 3.054	3.621	3.621	3.621
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-2  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 2.54, TOTAL EXCESS = 6.46

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
-----------	------	----------------------	--	--	--

			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	2.	12.20				
		(CFS)	0.	0.	0.	0.
		(INCHES)	5.322	6.462	6.462	6.462
		(AC-FT)	0.	0.	0.	0.
		CUMULATIVE AREA =	0.00 SQ MI			

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*****
*                               *
73 KK * SITE-3 * SOUTHEASTERLY SITE RUNOFF TOWARD PT.3
*                               *
*****

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*****
* DRAINAGE AREA = 3.56 AC = 0.0056 SQ. MI.           CN=78      *
* TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 *
*****

```

SUBBASIN RUNOFF DATA

80 BA SUBBASIN CHARACTERISTICS  
TAREA 0.01 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.01	0.00	0.01	0.00	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.02	0.03	0.05
0.08	0.08	0.05	0.03	0.02	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.00	0.01	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

81 LS SCS LOSS RATE  
STRTL 1.00 INITIAL ABSTRACTION  
CRVNBR 78.00 CURVE NUMBER  
RTIMP 0.00 PERCENT IMPERVIOUS AREA

82 UD SCS DIMENSIONLESS UNITGRAPH  
TLAG 0.10 LAG

\*\*\*

UNIT HYDROGRAPH  
7 END-OF-PERIOD ORDINATES

	14.	15.	5.	2.	1.	0.	0.
TOTAL RAINFALL =	1.00,		TOTAL LOSS = 1.00,		TOTAL EXCESS = 0.00		
PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)					
+	0.	0.10					
		(CFS)	0.	0.	0.	0.	
		(INCHES)	0.000	0.000	0.000	0.000	
		(AC-FT)	0.	0.	0.	0.	
		CUMULATIVE AREA =	0.01 SQ MI				

\*\*\*

HYDROGRAPH AT STATION SITE-3  
FOR PLAN 1, RATIO = 2.80

TOTAL RAINFALL = 2.80, TOTAL LOSS = 2.10, TOTAL EXCESS = 0.70

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
2.	12.30	(CFS)	0.	0.	0.
		(INCHES)	0.574	0.701	0.701
		(AC-FT)	0.	0.	0.
		CUMULATIVE AREA =	0.01 SQ MI		

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION SITE-3  
FOR PLAN 1, RATIO = 3.50

TOTAL RAINFALL = 3.50, TOTAL LOSS = 2.33, TOTAL EXCESS = 1.17

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
4.	12.30	(CFS)	1.	0.	0.
		(INCHES)	0.982	1.175	1.175
		(AC-FT)	0.	0.	0.
		CUMULATIVE AREA =	0.01 SQ MI		

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION SITE-3  
FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL = 4.50, TOTAL LOSS = 2.56, TOTAL EXCESS = 1.94

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
6.	12.30	(CFS)	1.	0.	0.
		(INCHES)	1.630	1.938	1.938
		(AC-FT)	0.	1.	1.
		CUMULATIVE AREA =	0.01 SQ MI		

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION SITE-3  
FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL = 5.10, TOTAL LOSS = 2.67, TOTAL EXCESS = 2.43

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
8.	12.30	(CFS)	1.	0.	0.
		(INCHES)	2.040	2.429	2.429
		(AC-FT)	1.	1.	1.
		CUMULATIVE AREA =	0.01 SQ MI		

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION SITE-3  
FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 2.80, TOTAL EXCESS = 3.20

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
10.	12.20	(CFS)	2.	0.	0.
		(INCHES)	2.678	3.197	3.197
		(AC-FT)	1.	1.	1.
		CUMULATIVE AREA =	0.01 SQ MI		

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION SITE-3  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 3.09, TOTAL EXCESS = 5.91

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
		(CFS)			

+ 19. 12.20 3. 1. 1. 1. (INCHES) 4.869 5.915 5.915 5.915 (AC-FT) 1. 2. 2. 2.  
CUMULATIVE AREA = 0.01 SQ MI

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\* \*  
83 KK \* SITE-4 \* CENTRAL/EASTERLY SITE RUNOFF TOWARD PT.4  
\* \*  
\*\*\*\*\*

\*\*\*\*\*  
\* DRAINAGE AREA = 0.91 AC = 0.0014 SQ. MI. CN=71 \*  
\* TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 \*  
\*\*\*\*\*

SUBBASIN RUNOFF DATA

90 BA SUBBASIN CHARACTERISTICS  
TAREA 0.00 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
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0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

91 LS SCS LOSS RATE  
STRTL 1.00 INITIAL ABSTRACTION  
CRVNR 71.00 CURVE NUMBER  
RTIMP 0.00 PERCENT IMPERVIOUS AREA

92 UD SCS DIMENSIONLESS UNITGRAPH  
TLAG 0.10 LAG

\*\*\*

UNIT HYDROGRAPH  
7 END-OF-PERIOD ORDINATES

3. 4. 1. 0. 0. 0.  
TOTAL RAINFALL = 1.00, TOTAL LOSS = 1.00, TOTAL EXCESS = 0.00  
PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
(CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
+ 0. 0.10 (CFS) 0. 0. 0. 0.  
(INCHES) 0.000 0.000 0.000 0.000  
(AC-FT) 0. 0. 0. 0.  
CUMULATIVE AREA = 0.00 SQ MI

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HYDROGRAPH AT STATION SITE-4  
FOR PLAN 1, RATIO = 2.80

TOTAL RAINFALL = 2.80, TOTAL LOSS = 2.25, TOTAL EXCESS = 0.55  
PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
6-HR 24-HR 72-HR 29.90-HR

+	(CFS)	(HR)	(CFS)				
+	0.	12.30	0.	0.	0.	0.	0.
			(INCHES)	0.446	0.551	0.551	0.551
			(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-4  
FOR PLAN 1, RATIO = 3.50

TOTAL RAINFALL = 3.50, TOTAL LOSS = 2.55, TOTAL EXCESS = 0.95

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	1.	12.30	0.	0.	0.	0.	
			(INCHES)	0.786	0.949	0.949	0.949
			(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-4  
FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL = 4.50, TOTAL LOSS = 2.88, TOTAL EXCESS = 1.62

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	1.	12.30	0.	0.	0.	0.	
			(INCHES)	1.346	1.615	1.615	1.615
			(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-4  
FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL = 5.10, TOTAL LOSS = 3.05, TOTAL EXCESS = 2.05

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	2.	12.30	0.	0.	0.	0.	
			(INCHES)	1.712	2.054	2.054	2.054
			(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-4  
FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 3.25, TOTAL EXCESS = 2.75

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	2.	12.30	0.	0.	0.	0.	
			(INCHES)	2.288	2.752	2.752	2.752
			(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-4  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 3.70, TOTAL EXCESS = 5.30

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	4.	12.20	1.	0.	0.	0.	
			(INCHES)	4.354	5.296	5.296	5.296
			(AC-FT)	0.	0.	0.	0.



CUMULATIVE AREA = 0.00 SQ MI

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\* OFF-1 \* OFFSITE SOUTHEASTERLY RUNOFF TOWARD PT.3  
\*  
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\*\*\*\*\*  
\* DRAINAGE AREA = 7.85 AC = 0.0123 SQ. MI. CN=93 \*  
\* TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 \*  
\*\*\*\*\*

SUBBASIN RUNOFF DATA

100 BA SUBBASIN CHARACTERISTICS  
TAREA 0.01 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.02	0.03
0.08	0.08	0.05	0.03	0.02	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

101 LS SCS LOSS RATE  
STRTL 1.00 INITIAL ABSTRACTION  
CRVNBR 93.00 CURVE NUMBER  
RTIMP 0.00 PERCENT IMPERVIOUS AREA

102 UD SCS DIMENSIONLESS UNITGRAPH  
TLAG 0.10 LAG

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UNIT HYDROGRAPH  
7 END-OF-PERIOD ORDINATES

30.	33.	11.	4.	1.	0.	0.
TOTAL RAINFALL = 1.00, TOTAL LOSS = 1.00, TOTAL EXCESS = 0.00						
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
+	0.	0.10	0.	0.	0.	0.
		(CFS)	(CFS)	(CFS)	(CFS)	(CFS)
		(INCHES)	0.000	0.000	0.000	0.000
		(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA = 0.01 SQ MI						

\*\*\*

HYDROGRAPH AT STATION OFF-1  
FOR PLAN 1, RATIO = 2.80

TOTAL RAINFALL = 2.80, TOTAL LOSS = 1.53, TOTAL EXCESS = 1.27						
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
+	10.	12.30	1.	0.	0.	0.
		(CFS)	(CFS)	(CFS)	(CFS)	(CFS)

(INCHES) 1.078 1.269 1.269 1.269  
 (AC-FT) 1. 1. 1. 1.

CUMULATIVE AREA = 0.01 SQ MI

\*\*\* \*\*\* \*\*\* \*\*\* \*\*\*

HYDROGRAPH AT STATION OFF-1  
 FOR PLAN 1, RATIO = 3.50

TOTAL RAINFALL = 3.50, TOTAL LOSS = 1.58, TOTAL EXCESS = 1.92

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
15.	12.30	2.	1.	1.	1.
		(INCHES) 1.659	1.921	1.921	1.921
		(AC-FT) 1.	1.	1.	1.

CUMULATIVE AREA = 0.01 SQ MI

\*\*\* \*\*\* \*\*\* \*\*\* \*\*\*

HYDROGRAPH AT STATION OFF-1  
 FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL = 4.50, TOTAL LOSS = 1.62, TOTAL EXCESS = 2.88

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
23.	12.20	3.	1.	1.	1.
		(INCHES) 2.484	2.881	2.881	2.881
		(AC-FT) 2.	2.	2.	2.

CUMULATIVE AREA = 0.01 SQ MI

\*\*\* \*\*\* \*\*\* \*\*\* \*\*\*

HYDROGRAPH AT STATION OFF-1  
 FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL = 5.10, TOTAL LOSS = 1.64, TOTAL EXCESS = 3.46

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
27.	12.20	4.	1.	1.	1.
		(INCHES) 2.976	3.464	3.464	3.464
		(AC-FT) 2.	2.	2.	2.

CUMULATIVE AREA = 0.01 SQ MI

\*\*\* \*\*\* \*\*\* \*\*\* \*\*\*

HYDROGRAPH AT STATION OFF-1  
 FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 1.65, TOTAL EXCESS = 4.35

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
33.	12.20	5.	1.	1.	1.
		(INCHES) 3.691	4.346	4.346	4.346
		(AC-FT) 2.	3.	3.	3.

CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION OFF-1  
 FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 1.69, TOTAL EXCESS = 7.31

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
52.	12.20	8.	2.	2.	2.
		(INCHES) 5.979	7.312	7.312	7.312
		(AC-FT) 4.	5.	5.	5.

CUMULATIVE AREA = 0.01 SQ MI

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 \*  
 103 KK \* PT.3 \* ADD SITE-3, SITE-4 AND OFF-1 HYDROGRAPHS  
 \*  
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104 HC HYDROGRAPH COMBINATION  
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION PT.3  
 FOR PLAN 1, RATIO = 2.80

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				29.90-HR
		6-HR	24-HR	72-HR		
12.	12.30	2.	1.	0.	0.	
		(INCHES) 0.885	1.052	1.052	1.052	
		(AC-FT) 1.	1.	1.	1.	
CUMULATIVE AREA =		0.02 SQ MI				

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HYDROGRAPH AT STATION PT.3  
 FOR PLAN 1, RATIO = 3.50

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				29.90-HR
		6-HR	24-HR	72-HR		
19.	12.30	3.	1.	1.	1.	
		(INCHES) 1.399	1.634	1.634	1.634	
		(AC-FT) 1.	2.	2.	2.	
CUMULATIVE AREA =		0.02 SQ MI				

\*\*\* \*\*\* \*\*\* \*\*\* \*\*\*

HYDROGRAPH AT STATION PT.3  
 FOR PLAN 1, RATIO = 4.50

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				29.90-HR
		6-HR	24-HR	72-HR		
30.	12.20	4.	1.	1.	1.	
		(INCHES) 2.151	2.515	2.515	2.515	
		(AC-FT) 2.	3.	3.	3.	
CUMULATIVE AREA =		0.02 SQ MI				

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HYDROGRAPH AT STATION PT.3  
 FOR PLAN 1, RATIO = 5.10

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				29.90-HR
		6-HR	24-HR	72-HR		
36.	12.20	5.	2.	1.	1.	
		(INCHES) 2.610	3.061	3.061	3.061	
		(AC-FT) 3.	3.	3.	3.	
CUMULATIVE AREA =		0.02 SQ MI				

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HYDROGRAPH AT STATION PT.3  
 FOR PLAN 1, RATIO = 6.00

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				29.90-HR
		6-HR	24-HR	72-HR		
46.	12.20	7.	2.	2.	2.	
		(INCHES) 3.292	3.897	3.897	3.897	
		(AC-FT) 3.	4.	4.	4.	
CUMULATIVE AREA =		0.02 SQ MI				

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***          ***          ***          ***          ***
HYDROGRAPH AT STATION    PT.3
FOR PLAN 1, RATIO = 9.00

PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      29.90-HR
+   76.        12.20          (CFS)
                                11.         4.         3.         3.
                                (INCHES)  5.531     6.760     6.760     6.760
                                (AC-FT)   6.         7.         7.         7.

CUMULATIVE AREA = 0.02 SQ MI

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*****
*
105 KK * LAG-3 * LAG PT.2 COMBINED HYDROGRAPH TO PT.4
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HYDROGRAPH ROUTING DATA

106 RT TATUM OR STRADDLE-STAGGER ROUTING
NSTPS 0 NUMBER OF TATUM STEPS
NSTDL 0 NUMBER OF ORDINATES TO BE AVERAGED
LAG 1 NUMBER OF INTERVALS TO LAG HYDROGRAPH

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***          ***          ***          ***          ***
HYDROGRAPH AT STATION    LAG-3
FOR PLAN 1, RATIO = 2.80

PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      29.90-HR
+   12.        12.40          (CFS)
                                2.         1.         0.         0.
                                (INCHES)  0.885     1.052     1.052     1.052
                                (AC-FT)   1.         1.         1.         1.

CUMULATIVE AREA = 0.02 SQ MI

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```

***          ***          ***          ***          ***
HYDROGRAPH AT STATION    LAG-3
FOR PLAN 1, RATIO = 3.50

PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      29.90-HR
+   19.        12.40          (CFS)
                                3.         1.         1.         1.
                                (INCHES)  1.399     1.634     1.634     1.634
                                (AC-FT)   1.         2.         2.         2.

CUMULATIVE AREA = 0.02 SQ MI

```

```

***          ***          ***          ***          ***
HYDROGRAPH AT STATION    LAG-3
FOR PLAN 1, RATIO = 4.50

PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      29.90-HR
+   30.        12.30          (CFS)
                                4.         1.         1.         1.
                                (INCHES)  2.151     2.515     2.515     2.515
                                (AC-FT)   2.         3.         3.         3.

CUMULATIVE AREA = 0.02 SQ MI

```

```

***          ***          ***          ***          ***
HYDROGRAPH AT STATION    LAG-3
FOR PLAN 1, RATIO = 5.10

PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      29.90-HR
+                                (CFS)

```

+ 36. 12.30 5. 2. 1. 1.  
(INCHES) 2.610 3.061 3.061 3.061  
(AC-FT) 3. 3. 3. 3.

CUMULATIVE AREA = 0.02 SQ MI

\*\*\* \*\*\* \*\*\* \*\*\* \*\*\*

HYDROGRAPH AT STATION LAG-3  
FOR PLAN 1, RATIO = 6.00

PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
(CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
+ 46. 12.30  
(CFS) 7. 2. 2. 2.  
(INCHES) 3.292 3.897 3.897 3.897  
(AC-FT) 3. 4. 4. 4.

CUMULATIVE AREA = 0.02 SQ MI

\*\*\* \*\*\* \*\*\* \*\*\* \*\*\*

HYDROGRAPH AT STATION LAG-3  
FOR PLAN 1, RATIO = 9.00

PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
(CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
+ 76. 12.30  
(CFS) 11. 4. 3. 3.  
(INCHES) 5.531 6.760 6.760 6.760  
(AC-FT) 6. 7. 7. 7.

CUMULATIVE AREA = 0.02 SQ MI

\*\*\* \*\*

107 KK \*\*\*\*\*  
\* \* SITE-5 \* NORTHEASTERLY SITE RUNOFF TOWARD PT.4  
\* \*

\*\*\*\*\*  
\* DRAINAGE AREA = 5.56 AC = 0.0087 SQ. MI. CN=76 \*  
\* TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 \*  
\*\*\*\*\*

SUBBASIN RUNOFF DATA

114 BA SUBBASIN CHARACTERISTICS  
TAREA 0.01 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
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0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

115 LS SCS LOSS RATE  
STRLL 1.00 INITIAL ABSTRACTION  
CRVNR 76.00 CURVE NUMBER  
RTIMP 0.00 PERCENT IMPERVIOUS AREA

\*\*\*

UNIT HYDROGRAPH  
7 END-OF-PERIOD ORDINATES

	21.	23.	8.	3.	1.	0.	0.
TOTAL RAINFALL =	1.00,	TOTAL LOSS =	1.00,	TOTAL EXCESS =	0.00		
PEAK FLOW	TIME		6-HR	24-HR	72-HR	29.90-HR	
+ (CFS)	(HR)	(CFS)					
+ 0.	0.10	0.000	0.000	0.000	0.000	0.000	
		(INCHES)	0.000	0.000	0.000	0.000	
		(AC-FT)	0.	0.	0.	0.	
		CUMULATIVE AREA =	0.01 SQ MI				

\*\*\*

HYDROGRAPH AT STATION SITE-5  
FOR PLAN 1, RATIO = 2.80

TOTAL RAINFALL =	2.80,	TOTAL LOSS =	2.15,	TOTAL EXCESS =	0.65		
PEAK FLOW	TIME		6-HR	24-HR	72-HR	29.90-HR	
+ (CFS)	(HR)	(CFS)					
+ 3.	12.30	0.	0.	0.	0.	0.	
		(INCHES)	0.533	0.654	0.654	0.654	
		(AC-FT)	0.	0.	0.	0.	
		CUMULATIVE AREA =	0.01 SQ MI				

\*\*\*

HYDROGRAPH AT STATION SITE-5  
FOR PLAN 1, RATIO = 3.50

TOTAL RAINFALL =	3.50,	TOTAL LOSS =	2.40,	TOTAL EXCESS =	1.10		
PEAK FLOW	TIME		6-HR	24-HR	72-HR	29.90-HR	
+ (CFS)	(HR)	(CFS)					
+ 5.	12.30	1.	0.	0.	0.	0.	
		(INCHES)	0.921	1.105	1.105	1.105	
		(AC-FT)	0.	1.	1.	1.	
		CUMULATIVE AREA =	0.01 SQ MI				

\*\*\*

HYDROGRAPH AT STATION SITE-5  
FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL =	4.50,	TOTAL LOSS =	2.66,	TOTAL EXCESS =	1.84		
PEAK FLOW	TIME		6-HR	24-HR	72-HR	29.90-HR	
+ (CFS)	(HR)	(CFS)					
+ 9.	12.30	1.	0.	0.	0.	0.	
		(INCHES)	1.543	1.840	1.840	1.840	
		(AC-FT)	1.	1.	1.	1.	
		CUMULATIVE AREA =	0.01 SQ MI				

\*\*\*

HYDROGRAPH AT STATION SITE-5  
FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL =	5.10,	TOTAL LOSS =	2.78,	TOTAL EXCESS =	2.32		
PEAK FLOW	TIME		6-HR	24-HR	72-HR	29.90-HR	
+ (CFS)	(HR)	(CFS)					
+ 12.	12.30	2.	1.	0.	0.	0.	
		(INCHES)	1.941	2.316	2.316	2.316	
		(AC-FT)	1.	1.	1.	1.	
		CUMULATIVE AREA =	0.01 SQ MI				

```

***          ***          ***          ***          ***
          HYDROGRAPH AT STATION SITE-5
          FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 2.94, TOTAL EXCESS = 3.06

PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
(CFS)          (HR)          6-HR      24-HR      72-HR      29.90-HR
+
+ 15.          12.20          (CFS)
          (INCHES) 2.          1.          1.          1.
          (AC-FT) 2.562 3.065 3.065 3.065
          (AC-FT) 1.          1.          1.          1.

CUMULATIVE AREA = 0.01 SQ MI

```

```

***          ***          ***          ***          ***
          HYDROGRAPH AT STATION SITE-5
          FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 3.26, TOTAL EXCESS = 5.74

PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
(CFS)          (HR)          6-HR      24-HR      72-HR      29.90-HR
+
+ 29.          12.20          (CFS)
          (INCHES) 4.721 5.736 5.736 5.736
          (AC-FT) 2.          3.          3.          3.

CUMULATIVE AREA = 0.01 SQ MI

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*****
*
117 KK * OFF-2 * OFFSITE EASTERLY RUNOFF TOWARD PT.4
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*****
* DRAINAGE AREA = 3.32 AC = 0.0052 SQ. MI. CN=78 *
* TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 *
*****

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SUBBASIN RUNOFF DATA

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124 BA SUBBASIN CHARACTERISTICS
      TAREA 0.01 SUBBASIN AREA

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PRECIPITATION DATA

```

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

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```

37 PI INCREMENTAL PRECIPITATION PATTERN
      0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
      0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
      0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
      0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
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      0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
      0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
      0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

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125 LS SCS LOSS RATE
      STRTL 1.00 INITIAL ABSTRACTION
      CRVNBR 78.00 CURVE NUMBER
      RTIMP 0.00 PERCENT IMPERVIOUS AREA

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126 UD SCS DIMENSIONLESS UNITGRAPH
      TLAG 0.10 LAG

```

\*\*\*

UNIT HYDROGRAPH  
7 END-OF-PERIOD ORDINATES

	13.	14.	5.	2.	1.	0.	0.
TOTAL RAINFALL =	1.00,	TOTAL LOSS =	1.00,	TOTAL EXCESS =	0.00		
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW			
+ (CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	29.90-HR	
+ 0.	0.10	0.	0.	0.	0.	0.	
		(INCHES)	0.000	0.000	0.000	0.000	0.000
		(AC-FT)	0.	0.	0.	0.	0.
		CUMULATIVE AREA =	0.01 SQ MI				

\*\*\*

HYDROGRAPH AT STATION OFF-2  
FOR PLAN 1, RATIO = 2.80

TOTAL RAINFALL =	2.80,	TOTAL LOSS =	2.10,	TOTAL EXCESS =	0.70		
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW			
+ (CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	29.90-HR	
+ 2.	12.30	0.	0.	0.	0.	0.	
		(INCHES)	0.574	0.701	0.701	0.701	0.701
		(AC-FT)	0.	0.	0.	0.	0.
		CUMULATIVE AREA =	0.01 SQ MI				

\*\*\*

HYDROGRAPH AT STATION OFF-2  
FOR PLAN 1, RATIO = 3.50

TOTAL RAINFALL =	3.50,	TOTAL LOSS =	2.33,	TOTAL EXCESS =	1.17		
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW			
+ (CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	29.90-HR	
+ 3.	12.30	1.	0.	0.	0.	0.	
		(INCHES)	0.982	1.175	1.175	1.175	1.175
		(AC-FT)	0.	0.	0.	0.	0.
		CUMULATIVE AREA =	0.01 SQ MI				

\*\*\*

HYDROGRAPH AT STATION OFF-2  
FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL =	4.50,	TOTAL LOSS =	2.56,	TOTAL EXCESS =	1.94		
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW			
+ (CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	29.90-HR	
+ 6.	12.30	1.	0.	0.	0.	0.	
		(INCHES)	1.630	1.938	1.938	1.938	1.938
		(AC-FT)	0.	1.	1.	1.	1.
		CUMULATIVE AREA =	0.01 SQ MI				

\*\*\*

HYDROGRAPH AT STATION OFF-2  
FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL =	5.10,	TOTAL LOSS =	2.67,	TOTAL EXCESS =	2.43		
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW			
+ (CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	29.90-HR	
+ 7.	12.30	1.	0.	0.	0.	0.	
		(INCHES)	2.040	2.429	2.429	2.429	2.429
		(AC-FT)	1.	1.	1.	1.	1.
		CUMULATIVE AREA =	0.01 SQ MI				

\*\*\*

HYDROGRAPH AT STATION OFF-2



FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 2.80, TOTAL EXCESS = 3.20

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
10.	12.20	(CFS)	1.	0.	0.	0.
		(INCHES)	2.678	3.197	3.197	3.197
		(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = 0.01 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION OFF-2  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 3.09, TOTAL EXCESS = 5.91

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
18.	12.20	(CFS)	3.	1.	1.	1.
		(INCHES)	4.869	5.915	5.915	5.915
		(AC-FT)	1.	2.	2.	2.

CUMULATIVE AREA = 0.01 SQ MI

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\*\*\*\*\*

127 KK \* PT.4 \* ADD LAG-2, SITE-5 AND OFF-2 HYDROGRAPHS

\*\*\*\*\*

128 HC HYDROGRAPH COMBINATION

ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\* \*\*

HYDROGRAPH AT STATION PT.4  
FOR PLAN 1, RATIO = 2.80

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
16.	12.40	(CFS)	3.	1.	1.	1.
		(INCHES)	0.744	0.893	0.893	0.893
		(AC-FT)	1.	2.	2.	2.

CUMULATIVE AREA = 0.03 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION PT.4  
FOR PLAN 1, RATIO = 3.50

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
28.	12.30	(CFS)	4.	1.	1.	1.
		(INCHES)	1.208	1.424	1.424	1.424
		(AC-FT)	2.	3.	3.	3.

CUMULATIVE AREA = 0.03 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION PT.4  
FOR PLAN 1, RATIO = 4.50

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
45.	12.30	(CFS)	7.	2.	2.	2.
		(INCHES)	1.910	2.248	2.248	2.248
		(AC-FT)	3.	4.	4.	4.

CUMULATIVE AREA = 0.03 SQ MI

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION      PT.4  
FOR PLAN 1, RATIO = 5.10

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
55.	12.30	8.	2.	2.	2.
		(INCHES) 2.344	2.767	2.767	2.767
		(AC-FT) 4.	5.	5.	5.
CUMULATIVE AREA = 0.03 SQ MI					

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION      PT.4  
FOR PLAN 1, RATIO = 6.00

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
71.	12.30	11.	3.	3.	3.
		(INCHES) 3.004	3.569	3.569	3.569
		(AC-FT) 5.	6.	6.	6.
CUMULATIVE AREA = 0.03 SQ MI					

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION      PT.4  
FOR PLAN 1, RATIO = 9.00

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
121.	12.30	19.	6.	5.	5.
		(INCHES) 5.213	6.359	6.359	6.359
		(AC-FT) 9.	11.	11.	11.
CUMULATIVE AREA = 0.03 SQ MI					

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
VOLUME IN ACRE-FEET, TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION						
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6	
				2.80	3.50	4.50	5.10	6.00	9.00	
HYDROGRAPH AT +	SITE-1	0.007	1	FLOW	2.28	4.27	7.30	9.18	12.14	22.48
				TIME	12.30	12.30	12.30	12.30	12.20	12.20
				VOLUME	0.24	0.41	0.67	0.84	1.11	2.05
HYDROGRAPH AT +	SITE-2	0.001	1	FLOW	0.25	0.47	0.78	0.96	1.23	2.11
				TIME	12.20	12.20	12.20	12.20	12.20	12.20
				VOLUME	0.02	0.04	0.06	0.07	0.10	0.17
HYDROGRAPH AT +	SITE-3	0.006	1	FLOW	1.97	3.68	6.29	7.90	10.45	19.37
				TIME	12.30	12.30	12.30	12.30	12.20	12.20
				VOLUME	0.21	0.35	0.58	0.73	0.95	1.77
HYDROGRAPH AT +	SITE-4	0.001	1	FLOW	0.37	0.71	1.27	1.63	2.19	4.27
				TIME	12.30	12.30	12.30	12.30	12.30	12.20
				VOLUME	0.04	0.07	0.12	0.15	0.21	0.40
HYDROGRAPH AT +	OFF-1	0.012	1	FLOW	9.62	15.04	22.65	26.90	32.99	52.19
				TIME	12.30	12.30	12.20	12.20	12.20	12.20
				VOLUME	0.83	1.26	1.89	2.27	2.85	4.80
3 COMBINED AT +	PT.3	0.019	1	FLOW	11.95	19.43	29.95	36.30	45.62	75.83
				TIME	12.30	12.30	12.20	12.20	12.20	12.20
				VOLUME	1.08	1.68	2.59	3.15	4.01	6.96
ROUTED TO +	LAG-3	0.019	1	FLOW	11.95	19.43	29.95	36.30	45.62	75.83
				TIME	12.40	12.40	12.30	12.30	12.30	12.30
				VOLUME	1.08	1.68	2.59	3.15	4.01	6.96

HYDROGRAPH AT										
+	SITE-5	0.009	1	FLOW	2.80	5.30	9.19	11.63	15.41	29.07
				TIME	12.30	12.30	12.30	12.30	12.20	12.20
				VOLUME	0.30	0.51	0.85	1.07	1.42	2.66
HYDROGRAPH AT										
+	OFF-2	0.005	1	FLOW	1.82	3.41	5.84	7.34	9.71	17.98
				TIME	12.30	12.30	12.30	12.30	12.20	12.20
				VOLUME	0.19	0.33	0.54	0.67	0.89	1.64
3 COMBINED AT										
+	PT.4	0.033	1	FLOW	16.12	27.58	44.98	55.27	70.59	121.08
				TIME	12.40	12.30	12.30	12.30	12.30	12.30
				VOLUME	1.58	2.52	3.98	4.90	6.32	11.26

\*\*\* NORMAL END OF HEC-1 \*\*\*

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* MAY 1991
* VERSION 4.0.IU
* Lahey F77L-EM/32 version 5.01
* Dodson & Associates, Inc.
* RUN DATE 02/06/20 TIME 13:30:24
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*****

```

## OAK TREE DEVELOPMENT #SY-1385: DEVELOPED CONDITIONS HEC-1 ANALYSIS

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID -----input file:DEV-R4.in1-----
2 ID
3 ID HYDROLOGY FOR: OAK TREE(SY #1385)
4 ID TOWN OF HAVERSTRAW, ROCKLAND COUNTY, NEW-YORK
5 ID DATE: 2-6-20
6 ID
7 ID ANALYSIS PREPARED BY: SPARACO & YOUNGBLOOD, PLLC
8 ID
9 ID ANALYSIS PARAMETERS:
10 ID DEVELOPED CONDITIONS RUN
11 ID STORM RECURRENCE INTERVALS = 1, 2, 5, 10, 25 & 100 YEAR
12 ID HYDROGRAPH METHOD: SCS
13 ID RAINFALL DISTRIBUTION: SCS TYPE III
14 ID
15 ID 24 HOUR RAINFALL DATA:
16 ID 1 YEAR: 2.8 INCHES
17 ID 2 YEAR: 3.5 INCHES
18 ID 5 YEAR: 4.5 INCHES
19 ID 10 YEAR: 5.1 INCHES
20 ID 25 YEAR: 6.0 INCHES
21 ID 100 YEAR: 9.0 INCHES
22 ID
23 ID
24 ID *DIAGRAM
24 IT 6 0 0 300
25 IO 3 0
26 JR PREC 2.8 3.5 4.5 5.1 6 9
27 KK SITE1ANORTHWESTERLY SITE DEV. ROAD AND PARK. LOT RUNOFF TOWARD PT.1
28 KM
29 KM *****
30 KM * DRAINAGE AREA = 0.37 AC = 0.0006 SQ. MI. CN=95 *
31 KM * TIME OF CONCENTRATION = 5 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 *
32 KM *****
33 KM
34 BA 0.0006
35 PB 1
36 IN 6
37 PC 0 0.001 0.002 0.003 0.004 0.005 0.006 0.007 0.008 0.009
38 PC 0.010 0.011 0.012 0.013 0.014 0.015 0.016 0.017 0.018 0.019
39 PC 0.020 0.021 0.022 0.023 0.024 0.026 0.027 0.028 0.029 0.030
40 PC 0.0305 0.031 0.032 0.034 0.035 0.036 0.037 0.038 0.040 0.041
41 PC 0.042 0.043 0.045 0.046 0.047 0.049 0.050 0.051 0.053 0.054
42 PC 0.055 0.057 0.058 0.060 0.061 0.063 0.064 0.066 0.067 0.069
43 PC 0.070 0.072 0.074 0.075 0.077 0.079 0.080 0.082 0.084 0.085
44 PC 0.087 0.089 0.091 0.093 0.095 0.097 0.100 0.103 0.106 0.109
45 PC 0.112 0.115 0.118 0.121 0.124 0.127 0.130 0.134 0.137 0.140
46 PC 0.144 0.148 0.151 0.155 0.159 0.163 0.167 0.171 0.176 0.180
47 PC 0.185 0.189 0.194 0.199 0.205 0.210 0.216 0.222 0.228 0.235
48 PC 0.242 0.250 0.258 0.266 0.276 0.287 0.298 0.312 0.328 0.363
49 PC 0.416 0.500 0.584 0.638 0.673 0.689 0.702 0.714 0.725 0.734
50 PC 0.743 0.751 0.758 0.766 0.772 0.779 0.785 0.790 0.796 0.801
51 PC 0.806 0.811 0.816 0.821 0.825 0.829 0.834 0.838 0.842 0.845
52 PC 0.849 0.853 0.857 0.860 0.864 0.867 0.870 0.874 0.877 0.880
53 PC 0.886 0.889 0.892 0.895 0.898 0.900 0.903 0.906 0.908 0.910

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
54      PC  0.911  0.913  0.915  0.917  0.919  0.920  0.922  0.924  0.925  0.927
55      PC  0.929  0.930  0.932  0.933  0.935  0.936  0.938  0.939  0.941  0.942
56      PC  0.944  0.945  0.946  0.948  0.949  0.951  0.952  0.953  0.955  0.956
57      PC  0.957  0.958  0.960  0.961  0.962  0.963  0.965  0.966  0.967  0.968
58      PC  0.969  0.971  0.972  0.973  0.974  0.975  0.976  0.977  0.978  0.979
59      PC  0.981  0.982  0.983  0.984  0.985  0.986  0.987  0.988  0.989  0.990
60      PC  0.991  0.992  0.993  0.994  0.995  0.996  0.997  0.998  0.999  1.000
61      LS      1      95
62      UD      0.05

63      KK  ROUTLAROUTING IN UNDERGROUND STORAGE SYSTEM FOR SITE-1A
64      KM
65      KM  OULET STRUCTURE DATA: 14 STORMTECH MC-4500 UNITS
66      KM  *****
67      KM  * WEIR LENGTH = 3.93' WEIR OVERFLOW AT EL.: 366.0 *
68      KM  * 3.0-INCH DIAMETER CPV ORIFICE AT EL. 365.3 *
69      KM  *****
70      KM
71      RS      1      ELEV 361.25
72      SV      0      0.004  0.0153  0.0262  0.0363  0.0453  0.052  0.0573  0.0573
73      SE 361.25      362      363      364      365      366      367      368      369.2
74      SQ      0      0.13  0.17  0.57  2.16  4.42  7.18  10.36  13.91  17.8
75      SE 365.3 365.7 365.9 366.1 366.3 366.5 366.7 366.9 367.1 367.3

76      KK  SITE-1NORTHWESTERLY SITE DEV. ROAD AND TRAIL RUNOFF TOWARD PT.1
77      KM
78      KM  *****
79      KM  * DRAINAGE AREA = 1.46 AC = 0.0023 SQ. MI.      CN=79 *
80      KM  * TIME OF CONCENTRATION = 5 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 *
81      KM  *****
82      KM
83      BA  0.0023
84      LS      1      79
85      UD      0.05

86      KK  PT.1ADD SITE-1A AND SITE-1 HYDROGRAPHS
87      HC      2

88      KK  SITE-2SOUTHWESTERLY SITE RUNOFF TOWARD PT.1
89      KM
90      KM  *****
91      KM  * DRAINAGE AREA = 0.22 AC = 0.0003 SQ. MI.      CN=90 *
92      KM  * TIME OF CONCENTRATION = 5 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 *
93      KM  *****
94      KM
95      BA  0.0003
96      LS      1      90
97      UD      0.05

98      KK  SITE3ASOUTHEASTERLY DEVELOPED SITE RUNOFF TOWARD PT.3
99      KM
100     KM  *****
101     KM  * DRAINAGE AREA = 2.28 AC = 0.0036 SQ. MI.      CN=93 *
102     KM  * TIME OF CONCENTRATION = 5 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 *
103     KM  *****

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
104     KM
105     BA  0.0036
106     LS      1      93
107     UD      0.05

108     KK  SITE-4SOUTHEASTERLY SITE RUNOFF (DETENTION AREA) TOWARD PT.3
109     KM
110     KM  *****
111     KM  * DRAINAGE AREA = 1.90 AC = 0.0030 SQ. MI.      CN=75 *
112     KM  * TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 *
113     KM  *****
114     KM
115     BA  0.003
116     LS      1      75
117     UD      0.1

118     KK  SITESANORTHEASTERLY DEVELOPED SITE RUNOFF TOWARD PT.5
119     KM
120     KM  *****
121     KM  * DRAINAGE AREA = 4.26 AC = 0.0067 SQ. MI.      CN=93 *
122     KM  * TIME OF CONCENTRATION = 5 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 *
123     KM  *****
124     KM
125     BA  0.0067
126     LS      1      93
127     UD      0.05

128     KK  SUB5A
129     DT  PERC5A      0.47
130     DI  5.91  9.48  13.86  16.3  19.84  31.08
131     DQ  5.44  9.01  13.39  15.83  19.37  30.61

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132      KK  ROUT5AROUTING IN UNDERGROUND STORAGE SYSTEM FOR SITE-5A
133      KM
134      KM  OUTLET STRUCTURE DATA: 140 STORMTECH MC-4500 UNITS
135      KM  *****
136      KM  * WEIR LENGTH = 4.71' WEIR OVERFLOW AT EL.: 366.3      *
137      KM  * 4.5-INCH DIAMETER CPV ORIFICE AT EL.: 364.2      *
138      KM  *****
139      KM
140      RS      1      ELEV      359
141      SV      0      0.0297      0.1169      0.2007      0.2788      0.3479      0.3985      0.438      0.438
142      SE      359      359.75      360.75      361.75      362.75      363.75      364.75      365.75      368.5
143      SQ      0      0.25      0.73      1.21      3.13      5.84      9.15      12.97      21.91      38.06
144      SE      364.2      364.6      366.2      366.4      366.6      366.8      367      367.2      367.6      368.2

145      KK  PT.AADD SITE-3A, SITE-4 AND SITESA HYDROGRAPHS
146      HC      3

147      KK  SUBA
148      DT  PERCA      0.37
149      DI      3.91      6.68      10.4      15.75      35.2      57.16
150      DQ      3.54      6.31      10.03      15.38      34.83      56.79

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HEC-1 INPUT

PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

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151      KK  ROUTAROUTING IN ABOVE GROUND STORAGE SYSTEM FOR COMB-3
152      KM
153      KM  OUTLET STRUCTURE DATA:
154      KM  *****
155      KM  * WEIR LENGTH = 3.0' WEIR OVERFLOW AT EL.: 356.0      *
156      KM  * 3.50-INCH DIAMETER CPV ORIFICE AT EL. 351.3      *
157      KM  * 8-INCH DIAMETER ORIFICE AT EL. 354.5      *
158      KM  *****
159      KM
160      RS      1      ELEV      350
161      SV      0      0.0864      0.1878      0.4544      0.79      1.3767      1.5367      1.5367
162      SE      350      350.5      351.5      353      355      357      358.25      358
163      SQ      0      0.08      0.6      1.31      2.54      3.52      29.93      37.92      50.45      65.63
164      SE      351.9      351.8      354.8      355      356      356.2      358      358.2      358.4      358.6

165      KK  SITE-3SOUTHEASTERLY UNIMPROVED SITE RUNOFF TOWARD PT.3
166      KM
167      KM  *****
168      KM  * DRAINAGE AREA = 0.16 AC = 0.0003 SQ. MI.      CN=70      *
169      KM  * TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100      *
170      KM  *****
171      KM
172      BA      0.0003
173      LS      1      70
174      UD      0.1

175      KK  PT.BADD ROUTE3 AND SITE-3 HYDROGRAPHS
176      HC      2

177      KK  OFF-1OFFSITE SOUTHEASTERLY RUNOFF TOWARD PT.3
178      KM
179      KM  *****
180      KM  * DRAINAGE AREA = 7.85 AC = 0.0123 SQ. MI.      CN=93      *
181      KM  * TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100      *
182      KM  *****
183      KM
184      BA      0.0123
185      LS      1      93
186      UD      0.1

187      KK  PT.3ADD PT.B AND OFF-1 HYDROGRAPHS
188      HC      2

189      KK  LAG-3LAG PT.2 COMBINED HYDROGRAPH TO PT.4
190      RT      0      0      1

191      KK  SITE-5NORTHEASTERLY UNDEVELOPED SITE RUNOFF TOWARD PT.4
192      KM
193      KM  *****
194      KM  * DRAINAGE AREA = 3.78 AC = 0.0059 SQ. MI.      CN=73      *
195      KM  * TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100      *
196      KM  *****
197      KM
198      BA      0.0059

```

HEC-1 INPUT

PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

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199      LS      1      73
200      UD      0.1

201      KK  OFF-2OFFSITE EASTERLY RUNOFF TOWARD PT.4
202      KM
203      KM  *****
204      KM  * DRAINAGE AREA = 3.32 AC = 0.0052 SQ. MI.      CN=78      *
205      KM  * TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100      *
206      KM  *****
207      KM
208      BA      0.0052

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209      LS      1      78
210      UD      0.1

211      KK      PT.4ADD LAG-3, SITE-5 AND OFF-2 HYDROGRAPHS
212      HC      3
213      ZZ

```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE   (V) ROUTING      (---->) DIVERSION OR PUMP FLOW
NO.    (.) CONNECTOR  (<----) RETURN OF DIVERTED OR PUMPED FLOW

27     SITE1A
      V
      V
63     ROUT1A
      .
      .
76     .             SITE-1
      .
      .
86     PT.1.....
      .
      .
88     .             SITE-2
      .
      .
98     .             SITE3A
      .
      .
108    .             SITE-4
      .
      .
118    .             SITESA
      .
      .
129    .             -----> PERCSA
128    .             SUB5A
      .             V
      .             V
132    .             ROUT5A
      .
      .
145    .             PT.A.....
      .
      .
148    .             -----> PERCA
147    .             SUBA
      .             V
      .             V
151    .             ROUTA
      .
      .
165    .             SITE-3
      .
      .
175    .             PT.B.....
      .
      .
177    .             OFF-1
      .
      .
187    .             PT.3.....
      .             V
      .             V
189    .             LAG-3
      .
      .
191    .             SITE-5
      .
      .
201    .             OFF-2
      .
      .
211    .             PT.4.....

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1U *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 02/06/20 TIME 13:30:24 *
*****

```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *
*****

```

-----input file:DEV-R4.ihl-----

HYDROLOGY FOR: OAK TREE(SY #1385)

ANALYSIS PREPARED BY: SPARACO & YOUNGBLOOD, PLLC

ANALYSIS PARAMETERS:  
DEVELOPED CONDITIONS RUN  
STORM RECURRENCE INTERVALS = 1, 2, 5, 10, 25 & 100 YEAR  
HYDROGRAPH METHOD: SCS  
RAINFALL DISTRIBUTION: SCS TYPE III

24 HOUR RAINFALL DATA:  
1 YEAR: 2.8 INCHES  
2 YEAR: 3.5 INCHES  
5 YEAR: 4.5 INCHES  
10 YEAR: 5.1 INCHES  
25 YEAR: 6.0 INCHES  
100 YEAR: 9.0 INCHES

25 IO OUTPUT CONTROL VARIABLES  
IPRNT 3 PRINT CONTROL  
IPLT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
NMIN 6 MINUTES IN COMPUTATION INTERVAL  
IDATE 1 0 STARTING DATE  
ITIME 0000 STARTING TIME  
NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
NDDATE 2 0 ENDING DATE  
NDTIME 0554 ENDING TIME  
ICENT 19 CENTURY MARK  
  
COMPUTATION INTERVAL 0.10 HOURS  
TOTAL TIME BASE 29.90 HOURS

ENGLISH UNITS  
DRAINAGE AREA SQUARE MILES  
PRECIPITATION DEPTH INCHES  
LENGTH, ELEVATION FEET  
FLOW CUBIC FEET PER SECOND  
STORAGE VOLUME ACRE-FEET  
SURFACE AREA ACRES  
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION  
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION  
RATIOS OF PRECIPITATION  
2.80 3.50 4.50 5.10 6.00 9.00

\*\*\*\*\*

\*\*\*\*\*  
\* \* \* \* \*  
27 KK \* SITELA \* NORTHWESTERLY SITE DEV. ROAD AND PARK. LOT RUNOFF TOWARD PT.1  
\* \* \* \* \*  
\*\*\*\*\*

\*\*\*\*\*  
\* DRAINAGE AREA = 0.37 AC = 0.0006 SQ. MI. CN=95 \*  
\* TIME OF CONCENTRATION = 5 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 \*  
\*\*\*\*\*

36 IN TIME DATA FOR INPUT TIME SERIES  
JXMIN 6 TIME INTERVAL IN MINUTES  
JXDATE 1 0 STARTING DATE  
JXTIME 0 STARTING TIME

SUBBASIN RUNOFF DATA

34 BA SUBBASIN CHARACTERISTICS  
TAREA 0.00 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00



0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.01	0.00	0.01	0.00	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.02	0.03	0.05
0.08	0.08	0.05	0.03	0.02	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.00	0.01	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

61 LS SCS LOSS RATE  
 STRTL 1.00 INITIAL ABSTRACTION  
 CRVNR 95.00 CURVE NUMBER  
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

62 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 0.05 LAG

\*\*\*

UNIT HYDROGRAPH  
 5 END-OF-PERIOD ORDINATES

3.	1.	0.	0.	0.		
TOTAL RAINFALL = 1.00, TOTAL LOSS = 1.00, TOTAL EXCESS = 0.00						
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
+	0.	0.10				
		(CFS)				
		0.	0.	0.	0.	
		(INCHES)	0.000	0.000	0.000	0.000
		(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA = 0.00 SQ MI						

\*\*\*

HYDROGRAPH AT STATION SITELA  
 FOR PLAN 1, RATIO = 2.80

TOTAL RAINFALL = 2.80, TOTAL LOSS = 1.41, TOTAL EXCESS = 1.39						
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
+	1.	12.20				
		(CFS)				
		0.	0.	0.	0.	
		(INCHES)	1.196	1.393	1.393	1.393
		(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA = 0.00 SQ MI						

\*\*\*

HYDROGRAPH AT STATION SITELA  
 FOR PLAN 1, RATIO = 3.50

TOTAL RAINFALL = 3.50, TOTAL LOSS = 1.43, TOTAL EXCESS = 2.07						
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
+	1.	12.20				
		(CFS)				
		0.	0.	0.	0.	
		(INCHES)	1.796	2.065	2.065	2.065
		(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA = 0.00 SQ MI						

\*\*\*

HYDROGRAPH AT STATION SITELA  
 FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL = 4.50, TOTAL LOSS = 1.46, TOTAL EXCESS = 3.04						
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
+	1.	12.20				
		(CFS)				
		0.	0.	0.	0.	
		(INCHES)	2.638	3.042	3.042	3.042
		(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA = 0.00 SQ MI						

\*\*\*  
 HYDROGRAPH AT STATION SITE1A  
 FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL = 5.10, TOTAL LOSS = 1.47, TOTAL EXCESS = 3.63

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
2.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	3.133	3.634	3.634	3.634
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SITE1A  
 FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 1.48, TOTAL EXCESS = 4.52

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
2.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	3.847	4.524	4.524	4.524
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SITE1A  
 FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 1.49, TOTAL EXCESS = 7.51

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
3.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	6.110	7.506	7.506	7.506
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

\*\*\*\*\*  
 \* ROUT1A \* ROUTING IN UNDERGROUND STORAGE SYSTEM FOR SITE-1A  
 \*\*\*\*\*

OUTLET STRUCTURE DATA: 14 STORMTECH MC-4500 UNITS  
 \*\*\*\*\*  
 \* WEIR LENGTH = 3.93' WEIR OVERFLOW AT EL.: 366.0 \*  
 \* 3.0-INCH DIAMETER CPV ORIFICE AT EL. 365.3 \*  
 \*\*\*\*\*

HYDROGRAPH ROUTING DATA

STATION	ROUTING DATA	1	2	3	4	5	6	7	8	9	10
71 RS	STORAGE ROUTING										
	NSTPS	1									
	ITYP	ELEV	TYPE OF INITIAL CONDITION								
	RSVRIC	361.25	INITIAL CONDITION								
	X	0.00	WORKING R AND D COEFFICIENT								
72 SV	STORAGE	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	
73 SE	ELEVATION	361.25	362.00	363.00	364.00	365.00	366.00	367.00	368.00	369.20	
74 SQ	DISCHARGE	0.	0.	0.	1.	2.	4.	7.	10.	14.	18.
75 SE	ELEVATION	365.30	365.70	365.90	366.10	366.30	366.50	366.70	366.90	367.10	367.30

\*\*\*  
 COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	0.00	0.02	0.03	0.04	0.04	0.04	0.04	0.05	0.05
OUTFLOW	0.00	0.00	0.00	0.00	0.00	0.00	0.13	0.17	0.37	0.57
ELEVATION	361.25	362.00	363.00	364.00	365.00	365.30	365.70	365.90	366.00	366.10
STORAGE	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.06	0.06	
OUTFLOW	2.16	4.42	7.18	10.36	12.14	13.91	17.80	31.42	54.76	
ELEVATION	366.30	366.50	366.70	366.90	367.00	367.10	367.30	368.00	369.20	

\*\*\* WARNING \*\*\* MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 0. TO 31.  
 THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.  
 THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION ROUT1A  
 FOR PLAN 1, RATIO = 2.80

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(CFS)			
+	0. 19.40	0.	0.	0.	0.
		(INCHES)	0.172	0.174	0.174
		(AC-FT)	0.	0.	0.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT)				
+	0. 18.30	0.	0.	0.	0.
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+	(FEET)				
+	365.34 19.60	365.33	364.04	363.49	363.49
CUMULATIVE AREA =		0.00 SQ MI			

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION ROUT1A  
 FOR PLAN 1, RATIO = 3.50

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(CFS)			
+	0. 13.90	0.	0.	0.	0.
		(INCHES)	0.643	0.846	0.846
		(AC-FT)	0.	0.	0.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT)				
+	0. 13.30	0.	0.	0.	0.
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+	(FEET)				
+	365.51 13.90	365.43	364.27	363.67	363.67
CUMULATIVE AREA =		0.00 SQ MI			

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION ROUT1A  
 FOR PLAN 1, RATIO = 4.50

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(CFS)			
+	1. 12.50	0.	0.	0.	0.
		(INCHES)	1.495	1.824	1.824
		(AC-FT)	0.	0.	0.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT)				
+	0. 12.40	0.	0.	0.	0.
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+	(FEET)				
+	366.09 12.50	365.58	364.36	363.75	363.75
CUMULATIVE AREA =		0.00 SQ MI			

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION ROUT1A  
 FOR PLAN 1, RATIO = 5.10

PEAK FLOW + (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
1.	12.30	(CFS)	0.	0.	0.	0.
		(INCHES)	2.035	2.415	2.415	2.415
		(AC-FT)	0.	0.	0.	0.
PEAK STORAGE		TIME	MAXIMUM AVERAGE STORAGE			
+	(AC-FT)	(HR)	6-HR	24-HR	72-HR	29.90-HR
	0.	12.30	0.	0.	0.	0.
PEAK STAGE		TIME	MAXIMUM AVERAGE STAGE			
+	(FEET)	(HR)	6-HR	24-HR	72-HR	29.90-HR
	366.16	12.30	365.62	364.40	363.78	363.78

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION ROUT1A  
FOR PLAN 1, RATIO = 6.00

PEAK FLOW + (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
2.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	2.847	3.305	3.305	3.305
		(AC-FT)	0.	0.	0.	0.
PEAK STORAGE		TIME	MAXIMUM AVERAGE STORAGE			
+	(AC-FT)	(HR)	6-HR	24-HR	72-HR	29.90-HR
	0.	12.20	0.	0.	0.	0.
PEAK STAGE		TIME	MAXIMUM AVERAGE STAGE			
+	(FEET)	(HR)	6-HR	24-HR	72-HR	29.90-HR
	366.24	12.20	365.67	364.47	363.83	363.83

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION ROUT1A  
FOR PLAN 1, RATIO = 9.00

PEAK FLOW + (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
3.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	5.525	6.287	6.287	6.287
		(AC-FT)	0.	0.	0.	0.
PEAK STORAGE		TIME	MAXIMUM AVERAGE STORAGE			
+	(AC-FT)	(HR)	6-HR	24-HR	72-HR	29.90-HR
	0.	12.10	0.	0.	0.	0.
PEAK STAGE		TIME	MAXIMUM AVERAGE STAGE			
+	(FEET)	(HR)	6-HR	24-HR	72-HR	29.90-HR
	366.36	12.20	365.83	364.72	364.03	364.03

CUMULATIVE AREA = 0.00 SQ MI

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\*                    \*  
76 KK           \*    SITE-1    \*    NORTHWESTERLY SITE DEV. ROAD AND TRAIL RUNOFF TOWARD PT.1  
\*                    \*  
\*\*\*\*\*

\*\*\*\*\*  
\* DRAINAGE AREA = 1.46 AC = 0.0023 SQ. MI.                    CN=79                    \*  
\* TIME OF CONCENTRATION = 5 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050                    \*  
\*\*\*\*\*

SUBBASIN RUNOFF DATA

83 BA                    SUBBASIN CHARACTERISTICS  
TAREA                    0.00                    SUBBASIN AREA



HYDROGRAPH AT STATION SITE-1  
FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL = 4.50, TOTAL LOSS = 2.51, TOTAL EXCESS = 1.99

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
3.	12.20	0.	0.	0.	0.
		(INCHES) 1.676	1.989	1.989	1.989
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.00 SQ MI			

\*\*\*

HYDROGRAPH AT STATION SITE-1  
FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL = 5.10, TOTAL LOSS = 2.61, TOTAL EXCESS = 2.49

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
4.	12.20	1.	0.	0.	0.
		(INCHES) 2.092	2.487	2.487	2.487
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.00 SQ MI			

\*\*\*

HYDROGRAPH AT STATION SITE-1  
FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 2.74, TOTAL EXCESS = 3.26

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
5.	12.20	1.	0.	0.	0.
		(INCHES) 2.739	3.264	3.264	3.264
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.00 SQ MI			

\*\*\*

HYDROGRAPH AT STATION SITE-1  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 3.00, TOTAL EXCESS = 6.00

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
9.	12.20	1.	0.	0.	0.
		(INCHES) 4.944	6.005	6.005	6.005
		(AC-FT) 1.	1.	1.	1.
CUMULATIVE AREA =		0.00 SQ MI			

\*\*\*

\*\*\*\*\*  
\*  
86 KK \* PT.1 \* ADD SITE-1A AND SITE-1 HYDROGRAPHS  
\*  
\*\*\*\*\*

87 HC HYDROGRAPH COMBINATION  
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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\*\*\*

HYDROGRAPH AT STATION PT.1  
FOR PLAN 1, RATIO = 2.80

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR

(CFS)  
 + 1. 12.20 0. 0. 0. 0.  
 (INCHES) 0.473 0.612 0.612 0.612  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION PT.1  
 FOR PLAN 1, RATIO = 3.50

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+ 2.	12.20	0.	0.	0.	0.
		(INCHES) 0.923	1.136	1.136	1.136
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA = 0.00 SQ MI					

\*\*\* \*\*

HYDROGRAPH AT STATION PT.1  
 FOR PLAN 1, RATIO = 4.50

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+ 3.	12.20	1.	0.	0.	0.
		(INCHES) 1.626	1.955	1.955	1.955
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA = 0.00 SQ MI					

\*\*\* \*\*

HYDROGRAPH AT STATION PT.1  
 FOR PLAN 1, RATIO = 5.10

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+ 4.	12.30	1.	0.	0.	0.
		(INCHES) 2.064	2.472	2.472	2.472
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA = 0.00 SQ MI					

\*\*\* \*\*

HYDROGRAPH AT STATION PT.1  
 FOR PLAN 1, RATIO = 6.00

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+ 7.	12.20	1.	0.	0.	0.
		(INCHES) 2.734	3.273	3.273	3.273
		(AC-FT) 0.	1.	1.	1.
CUMULATIVE AREA = 0.00 SQ MI					

\*\*\* \*\*

HYDROGRAPH AT STATION PT.1  
 FOR PLAN 1, RATIO = 9.00

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+ 12.	12.20	2.	0.	0.	0.
		(INCHES) 5.027	6.063	6.063	6.063
		(AC-FT) 1.	1.	1.	1.
CUMULATIVE AREA = 0.00 SQ MI					

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88 KK \* SITE-2 \* SOUTHWESTERLY SITE RUNOFF TOWARD PT.1  
 \* \* \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DRAINAGE AREA = 0.22 AC = 0.0003 SQ. MI. CN=90 \*  
 \* TIME OF CONCENTRATION = 5 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 \*  
 \*\*\*\*\*

SUBBASIN RUNOFF DATA

95 BA SUBBASIN CHARACTERISTICS  
 TAREA 0.00 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.01	0.00	0.01	0.00	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.02	0.03
0.08	0.08	0.05	0.03	0.02	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.00	0.01	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

96 LS SCS LOSS RATE  
 STRL 1.00 INITIAL ABSTRACTION  
 CRVNR 90.00 CURVE NUMBER  
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

97 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 0.05 LAG

\*\*\*

UNIT HYDROGRAPH  
 5 END-OF-PERIOD ORDINATES

1.	0.	0.	0.	0.	0.
TOTAL RAINFALL = 1.00, TOTAL LOSS = 1.00, TOTAL EXCESS = 0.00					
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	0.	0.	0.	0.	0.
	0.10	0.000	0.000	0.000	0.000
		(INCHES)	(INCHES)	(INCHES)	(INCHES)
		(AC-FT)	(AC-FT)	(AC-FT)	(AC-FT)
		0.	0.	0.	0.
CUMULATIVE AREA = 0.00 SQ MI					
***	***	***	***	***	***

HYDROGRAPH AT STATION SITE-2  
 FOR PLAN 1, RATIO = 2.80

TOTAL RAINFALL = 2.80, TOTAL LOSS = 1.69, TOTAL EXCESS = 1.11					
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+	0.	0.	0.	0.	0.
	12.20	0.937	1.113	1.113	1.113
		(INCHES)	(INCHES)	(INCHES)	(INCHES)
		(AC-FT)	(AC-FT)	(AC-FT)	(AC-FT)
		0.	0.	0.	0.
CUMULATIVE AREA = 0.00 SQ MI					
***	***	***	***	***	***

HYDROGRAPH AT STATION SITE-2  
 FOR PLAN 1, RATIO = 3.50



TOTAL RAINFALL = 3.50, TOTAL LOSS = 1.77, TOTAL EXCESS = 1.73

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
0.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	1.484	1.731	1.731	1.731
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-2  
FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL = 4.50, TOTAL LOSS = 1.84, TOTAL EXCESS = 2.66

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
1.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	2.277	2.657	2.657	2.657
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-2  
FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL = 5.10, TOTAL LOSS = 1.87, TOTAL EXCESS = 3.23

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
1.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	2.759	3.226	3.226	3.226
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-2  
FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 1.91, TOTAL EXCESS = 4.09

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
1.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	3.469	4.091	4.091	4.091
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-2  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 1.98, TOTAL EXCESS = 7.02

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
1.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	5.769	7.024	7.024	7.024
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*\*\*

98 KK

\*\*\*\*\*  
\* SITE3A \*  
\* \*  
\*\*\*\*\*

SOUTHEASTERLY DEVELOPED SITE RUNOFF TOWARD PT.3

\*\*\*\*\*  
\* DRAINAGE AREA = 2.28 AC = 0.0036 SQ. MI. CN=93 \*  
\* TIME OF CONCENTRATION = 5 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 \*  
\*\*\*\*\*

SUBBASIN RUNOFF DATA

105 BA SUBBASIN CHARACTERISTICS  
TAREA 0.00 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

106 LS SCS LOSS RATE  
STREL 1.00 INITIAL ABSTRACTION  
CRVNB 93.00 CURVE NUMBER  
RTIMP 0.00 PERCENT IMPERVIOUS AREA

107 UD SCS DIMENSIONLESS UNITGRAPH  
TLAG 0.05 LAG

\*\*\*

UNIT HYDROGRAPH  
5 END-OF-PERIOD ORDINATES

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	29.90-HR	
0.	0.10	0.	0.	0.	0.	
		(INCHES)	0.000	0.000	0.000	0.000
		(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA =		0.00 SQ MI				

\*\*\*

HYDROGRAPH AT STATION SITE3A  
FOR PLAN 1, RATIO = 2.80

TOTAL RAINFALL =		TOTAL LOSS =		TOTAL EXCESS =	
PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
3.	12.20	0.	0.	0.	0.
		(INCHES)	1.080	1.269	1.269
		(AC-FT)	0.	0.	0.
CUMULATIVE AREA =		0.00 SQ MI			

\*\*\*

HYDROGRAPH AT STATION SITE3A  
FOR PLAN 1, RATIO = 3.50

TOTAL RAINFALL =		TOTAL LOSS =		TOTAL EXCESS =	
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
3.50	12.20	0.	0.	0.	0.

			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	5.	12.20	(CFS)	1.	0.	0.
			(INCHES)	1.661	1.921	1.921
			(AC-FT)	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITE3A  
FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL = 4.50, TOTAL LOSS = 1.62, TOTAL EXCESS = 2.88

			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	7.	12.20	(CFS)	1.	0.	0.
			(INCHES)	2.485	2.881	2.881
			(AC-FT)	0.	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITE3A  
FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL = 5.10, TOTAL LOSS = 1.64, TOTAL EXCESS = 3.46

			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	9.	12.20	(CFS)	1.	0.	0.
			(INCHES)	2.977	3.464	3.464
			(AC-FT)	1.	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITE3A  
FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 1.65, TOTAL EXCESS = 4.35

			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	11.	12.20	(CFS)	1.	0.	0.
			(INCHES)	3.691	4.346	4.346
			(AC-FT)	1.	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITE3A  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 1.69, TOTAL EXCESS = 7.31

			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	17.	12.20	(CFS)	2.	1.	1.
			(INCHES)	5.980	7.312	7.312
			(AC-FT)	1.	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*\*\*

108 KK \*\*\*\*\*  
\* SITE-4 \* SOUTHEASTERLY SITE RUNOFF (DETENTION AREA) TOWARD PT.3  
\* \*\*\*\*\*

\*\*\*\*\*  
\* DRAINAGE AREA = 1.90 AC = 0.0030 SQ. MI. CN=75 \*

\* TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 \*  
 \*\*\*\*\*

SUBBASIN RUNOFF DATA

115 BA SUBBASIN CHARACTERISTICS  
 TAREA 0.00 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.01	0.00	0.01	0.00	0.01	0.00	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.02	0.03
0.08	0.08	0.05	0.03	0.02	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.00	0.01	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

116 LS SCS LOSS RATE  
 STRL 1.00 INITIAL ABSTRACTION  
 CRVNR 75.00 CURVE NUMBER  
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

117 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 0.10 LAG

\*\*\*

UNIT HYDROGRAPH  
 7 END-OF-PERIOD ORDINATES

	7.	8.	3.	1.	0.	0.	0.
TOTAL RAINFALL =	1.00,	TOTAL LOSS =	1.00,	TOTAL EXCESS =	0.00		
PEAK FLOW	TIME		6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	0.	0.10	0.	0.	0.	0.	0.
			(INCHES)	0.000	0.000	0.000	0.000
			(AC-FT)	0.	0.	0.	0.
			CUMULATIVE AREA =	0.00 SQ MI			

\*\*\*

HYDROGRAPH AT STATION SITE-4  
 FOR PLAN 1, RATIO = 2.80

TOTAL RAINFALL =	2.80,	TOTAL LOSS =	2.17,	TOTAL EXCESS =	0.63		
PEAK FLOW	TIME		6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	1.	12.30	0.	0.	0.	0.	0.
			(INCHES)	0.514	0.631	0.631	0.631
			(AC-FT)	0.	0.	0.	0.
			CUMULATIVE AREA =	0.00 SQ MI			

\*\*\*

HYDROGRAPH AT STATION SITE-4  
 FOR PLAN 1, RATIO = 3.50

TOTAL RAINFALL =	3.50,	TOTAL LOSS =	2.43,	TOTAL EXCESS =	1.07		
PEAK FLOW	TIME		6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				

+	2.	12.30		0.	0.	0.	0.
			(INCHES)	0.892	1.071	1.071	1.071
			(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-4  
FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL = 4.50, TOTAL LOSS = 2.71, TOTAL EXCESS = 1.79

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+	3.	12.30	(CFS)	0.	0.	0.
			(INCHES)	1.502	1.793	1.793
			(AC-FT)	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-4  
FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL = 5.10, TOTAL LOSS = 2.84, TOTAL EXCESS = 2.26

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+	4.	12.30	(CFS)	1.	0.	0.
			(INCHES)	1.893	2.261	2.261
			(AC-FT)	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-4  
FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 3.00, TOTAL EXCESS = 3.00

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+	5.	12.20	(CFS)	1.	0.	0.
			(INCHES)	2.505	3.000	3.000
			(AC-FT)	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SITE-4  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 3.35, TOTAL EXCESS = 5.65

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+	10.	12.20	(CFS)	1.	0.	0.
			(INCHES)	4.647	5.647	5.647
			(AC-FT)	1.	1.	1.

CUMULATIVE AREA = 0.00 SQ MI

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118 KK \* SITE5A \* NORTHEASTERLY DEVELOPED SITE RUNOFF TOWARD PT.5  
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\* DRAINAGE AREA = 4.26 AC = 0.0067 SQ. MI. CN=93 \*  
\* TIME OF CONCENTRATION = 5 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 \*  
\*\*\*\*\*



CUMULATIVE AREA = 0.01 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITESA  
FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL = 4.50, TOTAL LOSS = 1.62, TOTAL EXCESS = 2.88

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
14.	12.20	(CFS)	2.	1.	0.	0.
		(INCHES)	2.485	2.881	2.881	2.881
		(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = 0.01 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITESA  
FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL = 5.10, TOTAL LOSS = 1.64, TOTAL EXCESS = 3.46

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
16.	12.20	(CFS)	2.	1.	1.	1.
		(INCHES)	2.977	3.464	3.464	3.464
		(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = 0.01 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITESA  
FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 1.65, TOTAL EXCESS = 4.35

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
20.	12.20	(CFS)	3.	1.	1.	1.
		(INCHES)	3.691	4.346	4.346	4.346
		(AC-FT)	1.	2.	2.	2.

CUMULATIVE AREA = 0.01 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITESA  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 1.69, TOTAL EXCESS = 7.31

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
31.	12.20	(CFS)	4.	1.	1.	1.
		(INCHES)	5.980	7.312	7.312	7.312
		(AC-FT)	2.	3.	3.	3.

CUMULATIVE AREA = 0.01 SQ MI

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\* \*  
128 KK \* SUB5A \*  
\* \*  
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DT	DIVERSION ISTAD	PERC5A	DIVERSION HYDROGRAPH IDENTIFICATION				
DI	INFLOW	5.91	9.48	13.86	16.30	19.84	31.08
DQ	DIVERTED FLOW	5.44	9.01	13.39	15.83	19.37	30.61

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DIVERSION HYDROGRAPH PERCSA  
FOR PLAN 1, RATIO = 2.80

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	12.00	0.	0.	0.	0.
		(INCHES) 0.520	0.709	0.709	0.709
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

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HYDROGRAPH AT STATION SUBSA  
FOR PLAN 1, RATIO = 2.80

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
5.	12.20	0.	0.	0.	0.
		(INCHES) 0.560	0.560	0.560	0.560
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

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DIVERSION HYDROGRAPH PERCSA  
FOR PLAN 1, RATIO = 3.50

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	11.80	0.	0.	0.	0.
		(INCHES) 0.591	0.851	0.851	0.851
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

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HYDROGRAPH AT STATION SUBSA  
FOR PLAN 1, RATIO = 3.50

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
9.	12.20	1.	0.	0.	0.
		(INCHES) 1.070	1.070	1.070	1.070
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

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DIVERSION HYDROGRAPH PERCSA  
FOR PLAN 1, RATIO = 4.50

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	11.30	0.	0.	0.	0.
		(INCHES) 0.638	1.034	1.034	1.034
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

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HYDROGRAPH AT STATION SUBSA  
FOR PLAN 1, RATIO = 4.50

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
13.	12.20	1.	0.	0.	0.
		(INCHES) 1.846	1.846	1.846	1.846
		(AC-FT) 1.	1.	1.	1.
CUMULATIVE AREA =		0.01 SQ MI			



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DIVERSION HYDROGRAPH    PERCSA  
FOR PLAN 1, RATIO = 5.10

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	10.90	0.	0.	0.	0.
		(INCHES) 0.652	1.138	1.138	1.138
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

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HYDROGRAPH AT STATION    SUBSA  
FOR PLAN 1, RATIO = 5.10

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
16.	12.20	2.	0.	0.	0.
		(INCHES) 2.325	2.326	2.326	2.326
		(AC-FT) 1.	1.	1.	1.
CUMULATIVE AREA =		0.01 SQ MI			

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DIVERSION HYDROGRAPH    PERCSA  
FOR PLAN 1, RATIO = 6.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	10.40	0.	0.	0.	0.
		(INCHES) 0.652	1.284	1.284	1.284
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

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HYDROGRAPH AT STATION    SUBSA  
FOR PLAN 1, RATIO = 6.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
19.	12.20	2.	1.	0.	0.
		(INCHES) 3.039	3.062	3.062	3.062
		(AC-FT) 1.	1.	1.	1.
CUMULATIVE AREA =		0.01 SQ MI			

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DIVERSION HYDROGRAPH    PERCSA  
FOR PLAN 1, RATIO = 9.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	8.70	0.	0.	0.	0.
		(INCHES) 0.652	1.631	1.631	1.631
		(AC-FT) 0.	1.	1.	1.
CUMULATIVE AREA =		0.01 SQ MI			

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HYDROGRAPH AT STATION    SUBSA  
FOR PLAN 1, RATIO = 9.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
31.	12.20	4.	1.	1.	1.
		(INCHES) 5.328	5.681	5.681	5.681
		(AC-FT) 2.	2.	2.	2.

CUMULATIVE AREA = 0.01 SQ MI

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 \* ROUT5A \* ROUTING IN UNDERGROUND STORAGE SYSTEM FOR SITE-5A  
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 \* WEIR LENGTH = 4.71' WEIR OVERFLOW AT EL.: 366.3 \*  
 \* 4.5-INCH DIAMETER CPV ORIFICE AT EL.: 364.2 \*  
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HYDROGRAPH ROUTING DATA

STATION	ROUTING DATA	1	2	3	4	5	6	7	8	9	10
140 RS	STORAGE ROUTING										
	NSTPS	1									
	ITYP	ELEV	TYPE OF INITIAL CONDITION								
	RSVRC	359.00	INITIAL CONDITION								
	X	0.00	WORKING R AND D COEFFICIENT								
141 SV	STORAGE	0.0	0.0	0.1	0.2	0.3	0.3	0.4	0.4	0.4	
142 SE	ELEVATION	359.00	359.75	360.75	361.75	362.75	363.75	364.75	365.75	368.50	
143 SQ	DISCHARGE	0.	0.	1.	1.	3.	6.	9.	13.	22.	38.
144 SE	ELEVATION	364.20	364.60	366.20	366.40	366.60	366.80	367.00	367.20	367.60	368.20

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COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

	0.00	0.03	0.12	0.20	0.28	0.35	0.37	0.39	0.40	0.44
STORAGE	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.25	0.29
OUTFLOW	359.00	359.75	360.75	361.75	362.75	363.75	364.20	364.60	364.75	365.75
ELEVATION										
STORAGE	0.44	0.44	0.44	0.44	0.44	0.44	0.44	0.44	0.44	0.44
OUTFLOW	0.73	1.21	3.13	5.84	9.15	12.97	21.91	38.06	46.13	
ELEVATION	366.20	366.40	366.60	366.80	367.00	367.20	367.60	368.20	368.50	

\*\*\* WARNING \*\*\* MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 1. TO 46.  
 THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.  
 THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

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HYDROGRAPH AT STATION ROUT5A  
 FOR PLAN 1, RATIO = 2.80

PEAK FLOW	TIME		6-HR	24-HR	72-HR	29.90-HR
(CFS)	(HR)	(CFS)				
0.	0.10	0.	0.	0.	0.	0.
		(INCHES)	0.000	0.000	0.000	0.000
		(AC-FT)	0.	0.	0.	0.
PEAK STORAGE	TIME		6-HR	24-HR	72-HR	29.90-HR
(AC-FT)	(HR)					
0.	16.00	0.	0.	0.	0.	0.
PEAK STAGE	TIME		6-HR	24-HR	72-HR	29.90-HR
(FEET)	(HR)					
361.74	16.10	361.74	361.00	360.61	360.61	

CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION ROUT5A  
 FOR PLAN 1, RATIO = 3.50

PEAK FLOW	TIME		6-HR	24-HR	72-HR	29.90-HR
(CFS)	(HR)	(CFS)				
0.	15.20	0.	0.	0.	0.	0.
		(INCHES)	0.033	0.033	0.033	0.033
		(AC-FT)	0.	0.	0.	0.
PEAK STORAGE	TIME		6-HR	24-HR	72-HR	29.90-HR

		6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT) (HR)				
	0. 14.80	0.	0.	0.	0.
	PEAK STAGE TIME	MAXIMUM AVERAGE STAGE			
+	(FEET) (HR)	6-HR	24-HR	72-HR	29.90-HR
	364.29 16.10	364.24	362.79	362.04	362.04

CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION ROUT5A  
FOR PLAN 1, RATIO = 4.50

		6-HR	24-HR	72-HR	29.90-HR
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
+	(CFS) (HR)				
	3. 12.50	0.	0.	0.	0.
	(CFS)				
	(INCHES)	0.585	0.585	0.585	0.585
	(AC-FT)	0.	0.	0.	0.
	PEAK STORAGE TIME	MAXIMUM AVERAGE STORAGE			
+	(AC-FT) (HR)	6-HR	24-HR	72-HR	29.90-HR
	0. 12.50	0.	0.	0.	0.
	PEAK STAGE TIME	MAXIMUM AVERAGE STAGE			
+	(FEET) (HR)	6-HR	24-HR	72-HR	29.90-HR
	366.85 12.50	366.63	364.62	363.51	363.51

CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION ROUT5A  
FOR PLAN 1, RATIO = 5.10

		6-HR	24-HR	72-HR	29.90-HR
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
+	(CFS) (HR)				
	12. 12.30	1.	0.	0.	0.
	(CFS)				
	(INCHES)	1.018	1.018	1.018	1.018
	(AC-FT)	0.	0.	0.	0.
	PEAK STORAGE TIME	MAXIMUM AVERAGE STORAGE			
+	(AC-FT) (HR)	6-HR	24-HR	72-HR	29.90-HR
	0. 12.50	0.	0.	0.	0.
	PEAK STAGE TIME	MAXIMUM AVERAGE STAGE			
+	(FEET) (HR)	6-HR	24-HR	72-HR	29.90-HR
	367.11 12.50	366.90	364.85	363.70	363.70

CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION ROUT5A  
FOR PLAN 1, RATIO = 6.00

		6-HR	24-HR	72-HR	29.90-HR
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
+	(CFS) (HR)				
	19. 12.20	1.	0.	0.	0.
	(CFS)				
	(INCHES)	1.760	1.760	1.760	1.760
	(AC-FT)	1.	1.	1.	1.
	PEAK STORAGE TIME	MAXIMUM AVERAGE STORAGE			
+	(AC-FT) (HR)	6-HR	24-HR	72-HR	29.90-HR
	0. 12.50	0.	0.	0.	0.
	PEAK STAGE TIME	MAXIMUM AVERAGE STAGE			
+	(FEET) (HR)	6-HR	24-HR	72-HR	29.90-HR
	367.13 12.50	366.89	364.88	363.72	363.72

CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION ROUT5A  
FOR PLAN 1, RATIO = 9.00

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)			
+ 31.	12.20	3.	1.	1.	1.
		(INCHES)	4.459	4.644	4.644
		(AC-FT)	2.	2.	2.
PEAK STORAGE					
		MAXIMUM AVERAGE STORAGE			
+ (AC-FT)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+ 0.	12.00	0.	0.	0.	0.
PEAK STAGE					
		MAXIMUM AVERAGE STAGE			
+ (FEET)	(HR)	6-HR	24-HR	72-HR	29.90-HR
+ 367.92	12.20	366.24	363.66	362.74	362.74
CUMULATIVE AREA =		0.01 SQ MI			

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 \* \* \* \* \*  
 145 KK \* PT.A \* ADD SITE-3A, SITE-4 AND SITE5A HYDROGRAPHS  
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146 HC HYDROGRAPH COMBINATION  
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION PT.A  
 FOR PLAN 1, RATIO = 2.80

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)			
+ 4.	12.20	1.	0.	0.	0.
		(INCHES)	0.408	0.486	0.486
		(AC-FT)	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

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HYDROGRAPH AT STATION PT.A  
 FOR PLAN 1, RATIO = 3.50

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)			
+ 7.	12.20	1.	0.	0.	0.
		(INCHES)	0.666	0.778	0.778
		(AC-FT)	0.	1.	1.
CUMULATIVE AREA =		0.01 SQ MI			

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HYDROGRAPH AT STATION PT.A  
 FOR PLAN 1, RATIO = 4.50

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)			
+ 10.	12.20	2.	1.	0.	0.
		(INCHES)	1.304	1.479	1.479
		(AC-FT)	1.	1.	1.
CUMULATIVE AREA =		0.01 SQ MI			

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HYDROGRAPH AT STATION PT.A  
 FOR PLAN 1, RATIO = 5.10

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)			
+ 23.	12.30	2.	1.	1.	1.

(INCHES) 1.743 1.961 1.961 1.961  
 (AC-FT) 1. 1. 1. 1.

CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION PT.A  
 FOR PLAN 1, RATIO = 6.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
35.	12.20	3.	1.	1.	1.	
		(INCHES) 2.445	2.739	2.739	2.739	
		(AC-FT) 2.	2.	2.	2.	

CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION PT.A  
 FOR PLAN 1, RATIO = 9.00

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
57.	12.20	7.	2.	2.	2.	
		(INCHES) 4.830	5.592	5.592	5.592	
		(AC-FT) 3.	4.	4.	4.	

CUMULATIVE AREA = 0.01 SQ MI

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\*\*\*\*\*  
 147 KK SUBA \*  
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DT	DIVERSION ISTAD	PERCA	DIVERSION HYDROGRAPH IDENTIFICATION			
DI	INFLOW	3.91	6.68	10.40	15.75	35.20
DQ	DIVERTED FLOW	3.54	6.31	10.03	15.38	34.83

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DIVERSION HYDROGRAPH PERCA  
 FOR PLAN 1, RATIO = 2.80

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
0.	12.00	0.	0.	0.	0.	
		(INCHES) 0.209	0.286	0.286	0.286	
		(AC-FT) 0.	0.	0.	0.	

CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION SUBA  
 FOR PLAN 1, RATIO = 2.80

PEAK FLOW + (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
4.	12.20	0.	0.	0.	0.	
		(INCHES) 0.199	0.199	0.199	0.199	
		(AC-FT) 0.	0.	0.	0.	

CUMULATIVE AREA = 0.01 SQ MI

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DIVERSION HYDROGRAPH PERCA  
 FOR PLAN 1, RATIO = 3.50

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	11.90	0.	0.	0.	0.
		(INCHES) 0.242	0.355	0.355	0.355
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

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HYDROGRAPH AT STATION SUBA  
FOR PLAN 1, RATIO = 3.50

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
6.	12.20	1.	0.	0.	0.
		(INCHES) 0.424	0.424	0.424	0.424
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

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DIVERSION HYDROGRAPH PERCA  
FOR PLAN 1, RATIO = 4.50

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	11.40	0.	0.	0.	0.
		(INCHES) 0.255	0.429	0.429	0.429
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

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HYDROGRAPH AT STATION SUBA  
FOR PLAN 1, RATIO = 4.50

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
10.	12.20	2.	0.	0.	0.
		(INCHES) 1.049	1.049	1.049	1.049
		(AC-FT) 1.	1.	1.	1.
CUMULATIVE AREA =		0.01 SQ MI			

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DIVERSION HYDROGRAPH PERCA  
FOR PLAN 1, RATIO = 5.10

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	11.00	0.	0.	0.	0.
		(INCHES) 0.258	0.475	0.475	0.475
		(AC-FT) 0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

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HYDROGRAPH AT STATION SUBA  
FOR PLAN 1, RATIO = 5.10

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
22.	12.30	2.	1.	0.	0.
		(INCHES) 1.485	1.485	1.485	1.485
		(AC-FT) 1.	1.	1.	1.
CUMULATIVE AREA =		0.01 SQ MI			

\*\*\*

DIVERSION HYDROGRAPH PERCA  
FOR PLAN 1, RATIO = 6.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	29.90-HR	
0.	10.50	0.	0.	0.	0.	
		(INCHES)	0.259	0.536	0.536	0.536
		(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI				

\*\*\* \*\*

HYDROGRAPH AT STATION SUBA  
FOR PLAN 1, RATIO = 6.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	29.90-HR	
35.	12.20	3.	1.	1.	1.	
		(INCHES)	2.187	2.203	2.203	2.203
		(AC-FT)	2.	2.	2.	2.
CUMULATIVE AREA =		0.01 SQ MI				

\*\*\* \*\*

DIVERSION HYDROGRAPH PERCA  
FOR PLAN 1, RATIO = 9.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	29.90-HR	
0.	9.00	0.	0.	0.	0.	
		(INCHES)	0.259	0.671	0.671	0.671
		(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI				

\*\*\* \*\*

HYDROGRAPH AT STATION SUBA  
FOR PLAN 1, RATIO = 9.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	29.90-HR	
57.	12.20	7.	2.	1.	1.	
		(INCHES)	4.572	4.922	4.922	4.922
		(AC-FT)	3.	3.	3.	3.
CUMULATIVE AREA =		0.01 SQ MI				

\*\*\*\*\*

\*\*\*\*\*  
\* ROUTA \* ROUTING IN ABOVE GROUND STORAGE SYSTEM FOR COMB-3  
\* \*\*\*\*\*

OUTLET STRUCTURE DATA:  
\*\*\*\*\*  
\* WEIR LENGTH = 3.0' WEIR OVERFLOW AT EL.: 356.0 \*  
\* 3.50-INCH DIAMETER CPV ORIFICE AT EL. 351.3 \*  
\* 8-INCH DIAMETER ORIFICE AT EL. 354.5 \*  
\*\*\*\*\*

HYDROGRAPH ROUTING DATA

STORAGE ROUTING	NSTPS	1	NUMBER OF SUBREACHES								
ITYP	ELEV		TYPE OF INITIAL CONDITION								
RSVRC	350.00		INITIAL CONDITION								
X	0.00		WORKING R AND D COEFFICIENT								
161 SV	STORAGE	0.0	0.1	0.2	0.5	0.8	1.4	1.5	1.5		
162 SE	ELEVATION	350.00	350.50	351.50	353.00	355.00	357.00	358.25	358.00		
163 SQ	DISCHARGE	0.	0.	1.	1.	3.	4.	30.	38.	50.	66.
164 SE	ELEVATION	351.90	351.80	354.80	355.00	356.00	356.20	358.00	358.20	358.40	358.60

\*\*\*

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	0.00	0.09	0.19	0.26	0.45	0.76	0.79	1.08	1.14	1.38
OUTFLOW	0.00	0.00	0.00	0.10	0.29	0.60	1.31	2.54	3.52	15.26
ELEVATION	350.00	350.50	351.50	351.90	353.00	354.80	355.00	356.00	356.20	357.00

STORAGE	1.50	1.53	1.54	1.54	1.54
OUTFLOW	29.93	37.92	41.05	50.45	65.63
ELEVATION	358.00	358.20	358.25	358.40	358.60

\*\*\* WARNING \*\*\* MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 30. TO 66.  
 THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.  
 THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

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HYDROGRAPH AT STATION    ROUTA  
 FOR PLAN 1, RATIO = 2.80

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(CFS)			
+	0.    0.10	0.	0.	0.	0.
		(INCHES)	0.000	0.000	0.000
		(AC-FT)	0.	0.	0.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT)	(AC-FT)			
+	0.    14.40	0.	0.	0.	0.
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+	(FEET)	(FEET)			
+	351.04    16.10	351.04	350.75	350.61	350.61
CUMULATIVE AREA =		0.01 SQ MI			

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION    ROUTA  
 FOR PLAN 1, RATIO = 3.50

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(CFS)			
+	0.    14.80	0.	0.	0.	0.
		(INCHES)	0.070	0.134	0.134
		(AC-FT)	0.	0.	0.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT)	(AC-FT)			
+	0.    14.80	0.	0.	0.	0.
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+	(FEET)	(FEET)			
+	351.97    15.30	351.92	351.30	351.05	351.05
CUMULATIVE AREA =		0.01 SQ MI			

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION    ROUTA  
 FOR PLAN 1, RATIO = 4.50

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(CFS)			
+	0.    14.80	0.	0.	0.	0.
		(INCHES)	0.292	0.612	0.612
		(AC-FT)	0.	0.	0.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
+	(AC-FT)	(AC-FT)			
+	1.    14.80	1.	0.	0.	0.
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+	(FEET)	(FEET)			
+	353.94    15.20	353.75	352.26	351.81	351.81
CUMULATIVE AREA =		0.01 SQ MI			



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HYDROGRAPH AT STATION    ROUTA  
FOR PLAN 1, RATIO = 5.10

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)			
+ 1.	13.90	1.	0.	0.	0.
		(INCHES)	0.535	0.977	0.977
		(AC-FT)	0.	1.	1.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)				
+ 1.	13.90	1.	0.	0.	0.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)				
+ 355.00	13.90	354.72	352.76	352.21	352.21

CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION    ROUTA  
FOR PLAN 1, RATIO = 6.00

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)			
+ 2.	13.40	2.	1.	0.	0.
		(INCHES)	1.177	1.670	1.670
		(AC-FT)	1.	1.	1.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)				
+ 1.	13.40	1.	0.	0.	0.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)				
+ 355.86	13.40	355.36	353.03	352.43	352.43

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION    ROUTA  
FOR PLAN 1, RATIO = 9.00

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)			
+ 36.	12.40	5.	2.	1.	1.
		(INCHES)	3.559	4.307	4.307
		(AC-FT)	3.	3.	3.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)				
+ 2.	12.40	1.	1.	0.	0.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)				
+ 358.16	12.40	356.07	353.55	352.85	352.85

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*\*\*

165 KK                    \*\*\*\*\*  
   \*                    \*  
   \*    SITE-3    \*                    SOUTHEASTERLY UNIMPROVED SITE RUNOFF TOWARD PT.3  
   \*                    \*  
   \*\*\*\*\*

\*\*\*\*\*  
\* DRAINAGE AREA = 0.16 AC = 0.0003 SQ. MI.                    CN=70                    \*  
\* TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100                    \*  
\*\*\*\*\*



CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITE-3  
FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL = 4.50, TOTAL LOSS = 2.93, TOTAL EXCESS = 1.57

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
0.	12.30	(CFS)	0.	0.	0.	0.
		(INCHES)	1.310	1.573	1.573	1.573
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITE-3  
FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL = 5.10, TOTAL LOSS = 3.10, TOTAL EXCESS = 2.00

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
0.	12.30	(CFS)	0.	0.	0.	0.
		(INCHES)	1.669	2.005	2.005	2.005
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITE-3  
FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 3.31, TOTAL EXCESS = 2.69

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
0.	12.30	(CFS)	0.	0.	0.	0.
		(INCHES)	2.236	2.692	2.692	2.692
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SITE-3  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 3.79, TOTAL EXCESS = 5.21

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
1.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	4.282	5.209	5.209	5.209
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

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*           *
175 KK *   PT.B *   ADD ROUTE3 AND SITE-3 HYDROGRAPHS
*           *
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176 HC   HYDROGRAPH COMBINATION
        ICOMP      2  NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION PT.B

FOR PLAN 1, RATIO = 2.80

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	12.30	0.	0.	0.	0.
		(CFS)			
		(INCHES)	0.010	0.012	0.012
		(AC-FT)	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

\*\*\*

HYDROGRAPH AT STATION PT.B  
FOR PLAN 1, RATIO = 3.50

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	12.30	0.	0.	0.	0.
		(CFS)			
		(INCHES)	0.079	0.151	0.151
		(AC-FT)	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

\*\*\*

HYDROGRAPH AT STATION PT.B  
FOR PLAN 1, RATIO = 4.50

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	14.70	0.	0.	0.	0.
		(CFS)			
		(INCHES)	0.299	0.634	0.634
		(AC-FT)	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI			

\*\*\*

HYDROGRAPH AT STATION PT.B  
FOR PLAN 1, RATIO = 5.10

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
1.	13.90	1.	0.	0.	0.
		(CFS)			
		(INCHES)	0.544	0.999	0.999
		(AC-FT)	0.	1.	1.
CUMULATIVE AREA =		0.01 SQ MI			

\*\*\*

HYDROGRAPH AT STATION PT.B  
FOR PLAN 1, RATIO = 6.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
2.	13.40	2.	1.	0.	0.
		(CFS)			
		(INCHES)	1.189	1.692	1.692
		(AC-FT)	1.	1.	1.
CUMULATIVE AREA =		0.01 SQ MI			

\*\*\*

HYDROGRAPH AT STATION PT.B  
FOR PLAN 1, RATIO = 9.00

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
37.	12.40	5.	2.	1.	1.
		(CFS)			
		(INCHES)	3.560	4.327	4.327
		(AC-FT)	3.	3.	3.
CUMULATIVE AREA =		0.01 SQ MI			

\*\*\*\*\*

177 KK \*\*\*\*\*  
\* OFF-1 \* OFFSITE SOUTHEASTERLY RUNOFF TOWARD PT.3  
\*\*\*\*\*

\*\*\*\*\*  
\* DRAINAGE AREA = 7.85 AC = 0.0123 SQ. MI. CN=93 \*  
\* TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 \*  
\*\*\*\*\*

SUBBASIN RUNOFF DATA

184 BA SUBBASIN CHARACTERISTICS  
TAREA 0.01 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN  
Table with 11 columns of precipitation values ranging from 0.00 to 0.05.

185 LS SCS LOSS RATE  
STRTL 1.00 INITIAL ABSTRACTION  
CRVNR 93.00 CURVE NUMBER  
RTIMP 0.00 PERCENT IMPERVIOUS AREA

186 UD SCS DIMENSIONLESS UNITGRAPH  
TLAG 0.10 LAG

UNIT HYDROGRAPH  
7 END-OF-PERIOD ORDINATES

Table showing rainfall and loss data for a 30-hour period. Includes columns for rainfall, loss, and excess.

\*\*\*

HYDROGRAPH AT STATION OFF-1  
FOR PLAN 1, RATIO = 2.80

Table showing rainfall and loss data for a 10-hour period at station OFF-1. Includes columns for rainfall, loss, and excess.

\*\*\*  
 HYDROGRAPH AT STATION OFF-1  
 FOR PLAN 1, RATIO = 3.50

TOTAL RAINFALL = 3.50, TOTAL LOSS = 1.58, TOTAL EXCESS = 1.92

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
15.	12.30	2.	1.	1.	1.
		(INCHES) 1.659	1.921	1.921	1.921
		(AC-FT) 1.	1.	1.	1.

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION OFF-1  
 FOR PLAN 1, RATIO = 4.50

TOTAL RAINFALL = 4.50, TOTAL LOSS = 1.62, TOTAL EXCESS = 2.88

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
23.	12.20	3.	1.	1.	1.
		(INCHES) 2.484	2.881	2.881	2.881
		(AC-FT) 2.	2.	2.	2.

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION OFF-1  
 FOR PLAN 1, RATIO = 5.10

TOTAL RAINFALL = 5.10, TOTAL LOSS = 1.64, TOTAL EXCESS = 3.46

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
27.	12.20	4.	1.	1.	1.
		(INCHES) 2.976	3.464	3.464	3.464
		(AC-FT) 2.	2.	2.	2.

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION OFF-1  
 FOR PLAN 1, RATIO = 6.00

TOTAL RAINFALL = 6.00, TOTAL LOSS = 1.65, TOTAL EXCESS = 4.35

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
33.	12.20	5.	1.	1.	1.
		(INCHES) 3.691	4.346	4.346	4.346
		(AC-FT) 2.	3.	3.	3.

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION OFF-1  
 FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 1.69, TOTAL EXCESS = 7.31

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
52.	12.20	8.	2.	2.	2.
		(INCHES) 5.979	7.312	7.312	7.312
		(AC-FT) 4.	5.	5.	5.

CUMULATIVE AREA = 0.01 SQ MI

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 \* \* \* \* \*  
 187 KK \* PT.3 \* ADD PT.B AND OFF-1 HYDROGRAPHS  
 \* \* \* \* \*  
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188 HC HYDROGRAPH COMBINATION  
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION PT.3  
 FOR PLAN 1, RATIO = 2.80

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
10.	12.30	1.	0.	0.	0.
		(INCHES) 0.517	0.609	0.609	0.609
		(AC-FT) 1.	1.	1.	1.

CUMULATIVE AREA = 0.03 SQ MI

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HYDROGRAPH AT STATION PT.3  
 FOR PLAN 1, RATIO = 3.50

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
15.	12.30	2.	1.	1.	1.
		(INCHES) 0.828	0.992	0.992	0.992
		(AC-FT) 1.	1.	1.	1.

CUMULATIVE AREA = 0.03 SQ MI

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HYDROGRAPH AT STATION PT.3  
 FOR PLAN 1, RATIO = 4.50

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
23.	12.20	4.	1.	1.	1.
		(INCHES) 1.316	1.701	1.701	1.701
		(AC-FT) 2.	2.	2.	2.

CUMULATIVE AREA = 0.03 SQ MI

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HYDROGRAPH AT STATION PT.3  
 FOR PLAN 1, RATIO = 5.10

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
27.	12.20	5.	2.	1.	1.
		(INCHES) 1.663	2.170	2.170	2.170
		(AC-FT) 2.	3.	3.	3.

CUMULATIVE AREA = 0.03 SQ MI

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HYDROGRAPH AT STATION PT.3  
 FOR PLAN 1, RATIO = 6.00

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
34.	12.20	6.	2.	2.	2.
		(INCHES) 2.322	2.952	2.952	2.952
		(AC-FT) 3.	4.	4.	4.

CUMULATIVE AREA = 0.03 SQ MI

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HYDROGRAPH AT STATION PT.3  
 FOR PLAN 1, RATIO = 9.00

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
76.	12.30	13.	4.	3.	3.
		(INCHES) 4.546	5.744	5.744	5.744
		(AC-FT) 6.	8.	8.	8.
CUMULATIVE AREA =		0.03 SQ MI			

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 \* \* \* \* \*  
 189 KK \* LAG-3 \* LAG PT.2 COMBINED HYDROGRAPH TO PT.4  
 \* \* \* \* \*  
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HYDROGRAPH ROUTING DATA

190 RT TATUM OR STRADDLE-STAGGER ROUTING  
 NSTPS 0 NUMBER OF TATUM STEPS  
 NSTDL 0 NUMBER OF ORDINATES TO BE AVERAGED  
 LAG 1 NUMBER OF INTERVALS TO LAG HYDROGRAPH

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HYDROGRAPH AT STATION LAG-3  
 FOR PLAN 1, RATIO = 2.80

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
10.	12.40	1.	0.	0.	0.
		(INCHES) 0.517	0.609	0.609	0.609
		(AC-FT) 1.	1.	1.	1.
CUMULATIVE AREA =		0.03 SQ MI			

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HYDROGRAPH AT STATION LAG-3  
 FOR PLAN 1, RATIO = 3.50

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
15.	12.40	2.	1.	1.	1.
		(INCHES) 0.828	0.992	0.992	0.992
		(AC-FT) 1.	1.	1.	1.
CUMULATIVE AREA =		0.03 SQ MI			

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HYDROGRAPH AT STATION LAG-3  
 FOR PLAN 1, RATIO = 4.50

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
23.	12.30	4.	1.	1.	1.
		(INCHES) 1.316	1.700	1.700	1.700
		(AC-FT) 2.	2.	2.	2.
CUMULATIVE AREA =		0.03 SQ MI			

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HYDROGRAPH AT STATION LAG-3  
 FOR PLAN 1, RATIO = 5.10

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
27.	12.30	5.	2.	1.	1.
		(INCHES) 1.663	2.169	2.169	2.169
		(AC-FT) 2.	3.	3.	3.
CUMULATIVE AREA =		0.03 SQ MI			



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HYDROGRAPH AT STATION LAG-3  
FOR PLAN 1, RATIO = 6.00

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
34.	12.30	(CFS)	6.	2.	2.	2.
		(INCHES)	2.322	2.951	2.951	2.951
		(AC-FT)	3.	4.	4.	4.
CUMULATIVE AREA =			0.03 SQ MI			

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HYDROGRAPH AT STATION LAG-3  
FOR PLAN 1, RATIO = 9.00

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
76.	12.40	(CFS)	13.	4.	3.	3.
		(INCHES)	4.546	5.743	5.743	5.743
		(AC-FT)	6.	8.	8.	8.
CUMULATIVE AREA =			0.03 SQ MI			

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*****
* SITE-5 * NORTHEASTERLY UNDEVELOPED SITE RUNOFF TOWARD PT.4
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\*\*\*\*\*  
 \* DRAINAGE AREA = 3.78 AC = 0.0059 SQ. MI. CN=73 \*  
 \* TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 \*  
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SUBBASIN RUNOFF DATA

198 BA SUBBASIN CHARACTERISTICS  
TAREA 0.01 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

199 LS SCS LOSS RATE  
 STRL 1.00 INITIAL ABSTRACTION  
 CRVNR 73.00 CURVE NUMBER  
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

200 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 0.10 LAG

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UNIT HYDROGRAPH  
7 END-OF-PERIOD ORDINATES

	14.	16.	5.	2.	1.	0.	0.
TOTAL RAINFALL =	1.00,	TOTAL LOSS =	1.00,	TOTAL EXCESS =	0.00		
PEAK FLOW	TIME						
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	0.	0.10	0.	0.	0.	0.	0.
			(INCHES)	0.000	0.000	0.000	0.000
			(AC-FT)	0.	0.	0.	0.
			CUMULATIVE AREA =	0.01 SQ MI			

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HYDROGRAPH AT STATION    SITE-5  
FOR PLAN 1, RATIO = 2.80

	2.80,	TOTAL LOSS =	2.21,	TOTAL EXCESS =	0.59		
PEAK FLOW	TIME						
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	2.	12.30	0.	0.	0.	0.	0.
			(INCHES)	0.478	0.589	0.589	0.589
			(AC-FT)	0.	0.	0.	0.
			CUMULATIVE AREA =	0.01 SQ MI			

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HYDROGRAPH AT STATION    SITE-5  
FOR PLAN 1, RATIO = 3.50

	3.50,	TOTAL LOSS =	2.49,	TOTAL EXCESS =	1.01		
PEAK FLOW	TIME						
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	3.	12.30	1.	0.	0.	0.	0.
			(INCHES)	0.837	1.008	1.008	1.008
			(AC-FT)	0.	0.	0.	0.
			CUMULATIVE AREA =	0.01 SQ MI			

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HYDROGRAPH AT STATION    SITE-5  
FOR PLAN 1, RATIO = 4.50

	4.50,	TOTAL LOSS =	2.80,	TOTAL EXCESS =	1.70		
PEAK FLOW	TIME						
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	6.	12.30	1.	0.	0.	0.	0.
			(INCHES)	1.422	1.702	1.702	1.702
			(AC-FT)	0.	1.	1.	1.
			CUMULATIVE AREA =	0.01 SQ MI			

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HYDROGRAPH AT STATION    SITE-5  
FOR PLAN 1, RATIO = 5.10

	5.10,	TOTAL LOSS =	2.94,	TOTAL EXCESS =	2.16		
PEAK FLOW	TIME						
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	7.	12.30	1.	0.	0.	0.	0.
			(INCHES)	1.800	2.156	2.156	2.156
			(AC-FT)	1.	1.	1.	1.
			CUMULATIVE AREA =	0.01 SQ MI			

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HYDROGRAPH AT STATION    SITE-5  
FOR PLAN 1, RATIO = 6.00

	6.00,	TOTAL LOSS =	3.13,	TOTAL EXCESS =	2.87		
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PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
			(CFS)				
+	10.	12.30	2.	0.	0.	0.	
			(INCHES)	2.395	2.874	2.874	2.874
			(AC-FT)	1.	1.	1.	1.
			CUMULATIVE AREA = 0.01 SQ MI				

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HYDROGRAPH AT STATION SITE-5  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 3.53, TOTAL EXCESS = 5.47

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
+	(CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
			(CFS)				
+	19.	12.20	3.	1.	1.	1.	
			(INCHES)	4.501	5.471	5.471	5.471
			(AC-FT)	1.	2.	2.	2.
			CUMULATIVE AREA = 0.01 SQ MI				

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*              *
201 KK      * OFF-2 *      OFFSITE EASTERLY RUNOFF TOWARD PT.4
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*****
* DRAINAGE AREA = 3.32 AC = 0.0052 SQ. MI.          CN=78          *
* TIME OF CONCENTRATION = 10 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.100 *
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SUBBASIN RUNOFF DATA

208 BA SUBBASIN CHARACTERISTICS  
TAREA 0.01 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

209 LS SCS LOSS RATE  
STRTL 1.00 INITIAL ABSTRACTION  
CRVNR 78.00 CURVE NUMBER  
RTIMP 0.00 PERCENT IMPERVIOUS AREA

210 UD SCS DIMENSIONLESS UNITGRAPH  
TLAG 0.10 LAG

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UNIT HYDROGRAPH  
7 END-OF-PERIOD ORDINATES

13.	14.	5.	2.	1.	0.	0.
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TOTAL RAINFALL =		1.00,	TOTAL LOSS =	1.00,	TOTAL EXCESS =	0.00
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
+ (CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
+ 0.	0.10	(CFS)	0.	0.	0.	0.
		(INCHES)	0.000	0.000	0.000	0.000
		(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI				
***	***	***	***	***	***	***
HYDROGRAPH AT STATION OFF-2						
FOR PLAN 1, RATIO = 2.80						
TOTAL RAINFALL =		2.80,	TOTAL LOSS =	2.10,	TOTAL EXCESS =	0.70
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
+ (CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
+ 2.	12.30	(CFS)	0.	0.	0.	0.
		(INCHES)	0.574	0.701	0.701	0.701
		(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI				
***	***	***	***	***	***	***
HYDROGRAPH AT STATION OFF-2						
FOR PLAN 1, RATIO = 3.50						
TOTAL RAINFALL =		3.50,	TOTAL LOSS =	2.33,	TOTAL EXCESS =	1.17
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
+ (CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
+ 3.	12.30	(CFS)	1.	0.	0.	0.
		(INCHES)	0.982	1.175	1.175	1.175
		(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA =		0.01 SQ MI				
***	***	***	***	***	***	***
HYDROGRAPH AT STATION OFF-2						
FOR PLAN 1, RATIO = 4.50						
TOTAL RAINFALL =		4.50,	TOTAL LOSS =	2.56,	TOTAL EXCESS =	1.94
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
+ (CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
+ 6.	12.30	(CFS)	1.	0.	0.	0.
		(INCHES)	1.630	1.938	1.938	1.938
		(AC-FT)	0.	1.	1.	1.
CUMULATIVE AREA =		0.01 SQ MI				
***	***	***	***	***	***	***
HYDROGRAPH AT STATION OFF-2						
FOR PLAN 1, RATIO = 5.10						
TOTAL RAINFALL =		5.10,	TOTAL LOSS =	2.67,	TOTAL EXCESS =	2.43
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
+ (CFS)	(HR)	6-HR	24-HR	72-HR	29.90-HR	
+ 7.	12.30	(CFS)	1.	0.	0.	0.
		(INCHES)	2.040	2.429	2.429	2.429
		(AC-FT)	1.	1.	1.	1.
CUMULATIVE AREA =		0.01 SQ MI				
***	***	***	***	***	***	***
HYDROGRAPH AT STATION OFF-2						
FOR PLAN 1, RATIO = 6.00						
TOTAL RAINFALL =		6.00,	TOTAL LOSS =	2.80,	TOTAL EXCESS =	3.20
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
		6-HR	24-HR	72-HR	29.90-HR	

+	(CFS)	(HR)	(CFS)				
+	10.	12.20	1.	0.	0.	0.	0.
			(INCHES)	2.678	3.197	3.197	3.197
			(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION    OFF-2  
FOR PLAN 1, RATIO = 9.00

TOTAL RAINFALL = 9.00, TOTAL LOSS = 3.09, TOTAL EXCESS = 5.91

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	18.	12.20	3.	1.	1.	1.	
			(INCHES)	4.869	5.915	5.915	5.915
			(AC-FT)	1.	2.	2.	2.

CUMULATIVE AREA = 0.01 SQ MI

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\*                    \*  
211 KK           \*    PT.4   \*           ADD LAG-3, SITE-5 AND OFF-2 HYDROGRAPHS  
\*                    \*  
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212 HC                    HYDROGRAPH COMBINATION  
                              ICOMP                    3    NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION    PT.4  
FOR PLAN 1, RATIO = 2.80

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	13.	12.40	2.	1.	0.	0.	
			(INCHES)	0.519	0.619	0.619	0.619
			(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = 0.04 SQ MI

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION    PT.4  
FOR PLAN 1, RATIO = 3.50

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	22.	12.30	3.	1.	1.	1.	
			(INCHES)	0.851	1.020	1.020	1.020
			(AC-FT)	2.	2.	2.	2.

CUMULATIVE AREA = 0.04 SQ MI

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION    PT.4  
FOR PLAN 1, RATIO = 4.50

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	29.90-HR	
+	(CFS)	(HR)	(CFS)				
+	34.	12.30	5.	2.	1.	1.	
			(INCHES)	1.377	1.734	1.734	1.734
			(AC-FT)	3.	3.	3.	3.

CUMULATIVE AREA = 0.04 SQ MI

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HYDROGRAPH AT STATION    PT.4  
FOR PLAN 1, RATIO = 5.10

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
42.	12.30	7.	2.	2.	2.
		(INCHES) 1.738	2.203	2.203	2.203
		(AC-FT) 3.	4.	4.	4.
CUMULATIVE AREA =		0.04 SQ MI			

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HYDROGRAPH AT STATION PT.4  
FOR PLAN 1, RATIO = 6.00

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
53.	12.30	9.	3.	2.	2.
		(INCHES) 2.383	2.973	2.973	2.973
		(AC-FT) 5.	6.	6.	6.
CUMULATIVE AREA =		0.04 SQ MI			

\*\*\*

HYDROGRAPH AT STATION PT.4  
FOR PLAN 1, RATIO = 9.00

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
103.	12.40	18.	6.	5.	5.
		(INCHES) 4.582	5.724	5.724	5.724
		(AC-FT) 9.	11.	11.	11.
CUMULATIVE AREA =		0.04 SQ MI			

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PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
VOLUME IN ACRE-FEET, TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION						
				RATIO 1 2.80	RATIO 2 3.50	RATIO 3 4.50	RATIO 4 5.10	RATIO 5 6.00	RATIO 6 9.00	
HYDROGRAPH AT										
+	SITE1A	0.001	1	FLOW	0.62	0.93	1.31	1.53	1.83	2.82
				TIME	12.20	12.20	12.20	12.20	12.20	12.20
				VOLUME	0.04	0.07	0.10	0.12	0.14	0.24
ROUTED TO										
+	ROUT1A	0.001	1	FLOW	0.01	0.07	0.54	1.03	1.65	2.89
				TIME	19.40	13.90	12.50	12.30	12.20	12.20
				VOLUME	0.01	0.03	0.06	0.08	0.11	0.20
				** PEAK STAGES IN FEET **						
			1	STAGE	365.34	365.51	366.09	366.16	366.24	366.36
				TIME	19.60	13.90	12.50	12.30	12.20	12.20
HYDROGRAPH AT										
+	SITE-1	0.002	1	FLOW	0.91	1.76	3.04	3.83	5.03	9.03
				TIME	12.20	12.20	12.20	12.20	12.20	12.20
				VOLUME	0.09	0.15	0.24	0.31	0.40	0.74
2 COMBINED AT										
+	PT.1	0.003	1	FLOW	0.91	1.76	3.04	4.12	6.68	11.92
				TIME	12.20	12.20	12.20	12.30	12.20	12.20
				VOLUME	0.09	0.18	0.30	0.38	0.51	0.94
HYDROGRAPH AT										
+	SITE-2	0.000	1	FLOW	0.22	0.37	0.57	0.68	0.84	1.36
				TIME	12.20	12.20	12.20	12.20	12.20	12.20
				VOLUME	0.02	0.03	0.04	0.05	0.07	0.11
HYDROGRAPH AT										
+	SITE3A	0.004	1	FLOW	3.18	5.09	7.45	8.76	10.66	16.70
				TIME	12.20	12.20	12.20	12.20	12.20	12.20
				VOLUME	0.24	0.37	0.55	0.67	0.83	1.40
HYDROGRAPH AT										
+	SITE-4	0.003	1	FLOW	0.93	1.76	3.07	3.90	5.18	9.85
				TIME	12.30	12.30	12.30	12.30	12.20	12.20
				VOLUME	0.10	0.17	0.29	0.36	0.48	0.90
HYDROGRAPH AT										
+	SITE5A	0.007	1	FLOW	5.91	9.48	13.86	16.30	19.84	31.08

				TIME	12.20	12.20	12.20	12.20	12.20	12.20
				VOLUME	0.45	0.69	1.03	1.24	1.55	2.61
DIVERSION TO										
+	PERCSA	0.007	1	FLOW	0.47	0.47	0.47	0.47	0.47	0.47
				TIME	12.00	11.80	11.30	10.90	10.40	8.70
				VOLUME	0.25	0.30	0.37	0.41	0.46	0.58
HYDROGRAPH AT										
+	SUB5A	0.007	1	FLOW	5.44	9.01	13.39	15.83	19.37	30.61
				TIME	12.20	12.20	12.20	12.20	12.20	12.20
				VOLUME	0.20	0.38	0.66	0.83	1.09	2.03
ROUTED TO										
+	ROUT5A	0.007	1	FLOW	0.00	0.06	3.49	12.01	19.37	30.61
				TIME	0.10	15.20	12.50	12.30	12.20	12.20
				VOLUME	0.00	0.01	0.21	0.36	0.63	1.66
				** PEAK STAGES IN FEET **						
			1	STAGE	361.74	364.29	366.85	367.11	367.13	367.92
				TIME	16.10	16.10	12.50	12.50	12.50	12.20
3 COMBINED AT										
+	PT.A	0.013	1	FLOW	3.91	6.68	10.40	22.61	35.20	57.16
				TIME	12.20	12.20	12.20	12.30	12.20	12.20
				VOLUME	0.34	0.55	1.05	1.39	1.94	3.97
DIVERSION TO										
+	PERCA	0.013	1	FLOW	0.37	0.37	0.37	0.37	0.37	0.37
				TIME	12.00	11.90	11.40	11.00	10.50	9.00
				VOLUME	0.20	0.25	0.30	0.34	0.38	0.48
HYDROGRAPH AT										
+	SUBA	0.013	1	FLOW	3.54	6.31	10.03	22.24	34.83	56.79
				TIME	12.20	12.20	12.20	12.30	12.20	12.20
				VOLUME	0.14	0.30	0.74	1.05	1.56	3.49
ROUTED TO										
+	ROUTA	0.013	1	FLOW	0.00	0.11	0.45	1.30	2.37	36.35
				TIME	0.10	14.80	14.80	13.90	13.40	12.40
				VOLUME	0.00	0.09	0.43	0.69	1.18	3.05
				** PEAK STAGES IN FEET **						
			1	STAGE	351.04	351.97	353.94	355.00	355.86	358.16
				TIME	16.10	15.30	15.20	13.90	13.40	12.40
HYDROGRAPH AT										
+	SITE-3	0.000	1	FLOW	0.08	0.15	0.26	0.34	0.46	0.90
				TIME	12.30	12.30	12.30	12.30	12.30	12.20
				VOLUME	0.01	0.01	0.03	0.03	0.04	0.08
2 COMBINED AT										
+	PT.B	0.014	1	FLOW	0.08	0.15	0.47	1.33	2.43	37.03
				TIME	12.30	12.30	14.70	13.90	13.40	12.40
				VOLUME	0.01	0.11	0.46	0.72	1.23	3.14
HYDROGRAPH AT										
+	OFF-1	0.012	1	FLOW	9.62	15.04	22.65	26.90	32.99	52.19
				TIME	12.30	12.30	12.20	12.20	12.20	12.20
				VOLUME	0.83	1.26	1.89	2.27	2.85	4.80
2 COMBINED AT										
+	PT.3	0.026	1	FLOW	9.69	15.19	22.90	27.30	33.70	75.67
				TIME	12.30	12.30	12.20	12.20	12.20	12.30
				VOLUME	0.84	1.37	2.35	3.00	4.08	7.93
ROUTED TO										
+	LAG-3	0.026	1	FLOW	9.69	15.19	22.90	27.30	33.70	75.67
				TIME	12.40	12.40	12.30	12.30	12.30	12.40
				VOLUME	0.84	1.37	2.35	3.00	4.08	7.93
HYDROGRAPH AT										
+	SITE-5	0.006	1	FLOW	1.67	3.22	5.69	7.26	9.69	18.68
				TIME	12.30	12.30	12.30	12.30	12.30	12.20
				VOLUME	0.19	0.32	0.54	0.68	0.90	1.72
HYDROGRAPH AT										
+	OFF-2	0.005	1	FLOW	1.82	3.41	5.84	7.34	9.71	17.98
				TIME	12.30	12.30	12.30	12.30	12.20	12.20
				VOLUME	0.19	0.33	0.54	0.67	0.89	1.64
3 COMBINED AT										
+	PT.4	0.037	1	FLOW	12.85	21.67	34.43	41.90	53.01	102.91
				TIME	12.40	12.30	12.30	12.30	12.30	12.40
				VOLUME	1.22	2.01	3.42	4.35	5.87	11.29

\*\*\* NORMAL END OF HEC-1 \*\*\*